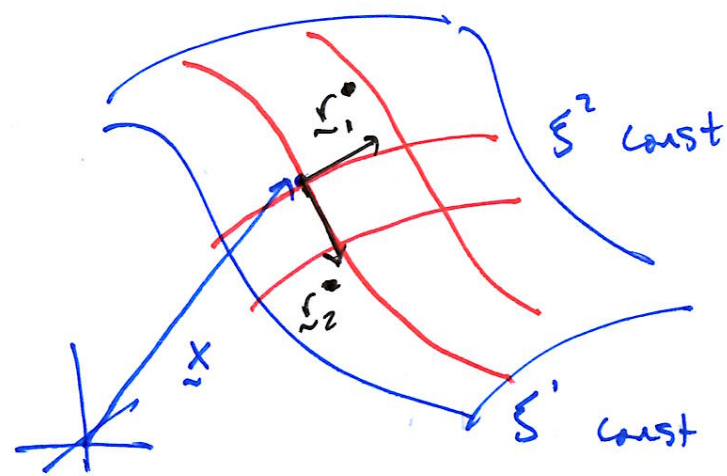
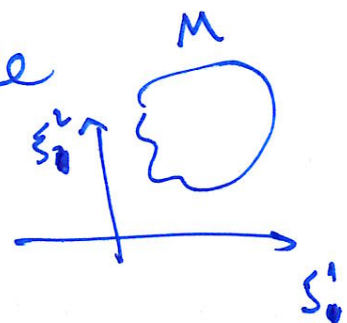


# Geometry of Surfaces

Let  $\Sigma$  be an orientable surface

w/ parameterisation  $\underline{x}(\xi^1, \xi^2) \in \mathbb{R}^3$ ,  
 $(\xi^1, \xi^2) \in M \subset \mathbb{R}^2$



- We assume  $\underline{x}$  is at least  $C^2$  & such that  $\underline{r}_i := \frac{\partial \underline{x}}{\partial \xi^i}$  are

lin. indep.  $\forall (\xi^1, \xi^2) \in M$ . Can define a unit normal  $\underline{n} = \frac{\underline{r}_1 \wedge \underline{r}_2}{\|\underline{r}_1 \wedge \underline{r}_2\|}$

and  $\{\underline{r}_1, \underline{r}_2, \underline{n}\}$  forms a basis.

Surface area  $A = \int_{\Sigma} dS$

Recall (1<sup>st</sup> yr):  $d\underline{S} = \underline{r}_1 \wedge \underline{r}_2 d\xi^1 d\xi^2$ ,  $dS = |d\underline{S}|$

Using identity  $(\underline{r}_1 \wedge \underline{r}_2)^2 = \underline{r}_1^2 \underline{r}_2^2 - (\underline{r}_1 \cdot \underline{r}_2)^2$ , we have  $dS = \sqrt{\underline{r}_1^2 \underline{r}_2^2 - (\underline{r}_1 \cdot \underline{r}_2)^2} d\xi^1 d\xi^2$

Defn Let  $g_{ij} := \underline{r}_i \cdot \underline{r}_j = \frac{\partial \underline{x}}{\partial \xi^i} \cdot \frac{\partial \underline{x}}{\partial \xi^j}$ . This is metric tensor. Also define  $G = (g_{ij})$  - the matrix of metric tensor

Then  $dS = \sqrt{g_{11}g_{22} - g_{12}^2} d\xi^1 d\xi^2 = \sqrt{\det G} d\xi^1 d\xi^2$

and  $A = \int_M \sqrt{\det G} d\xi^1 d\xi^2$

# Biomembranes Overview

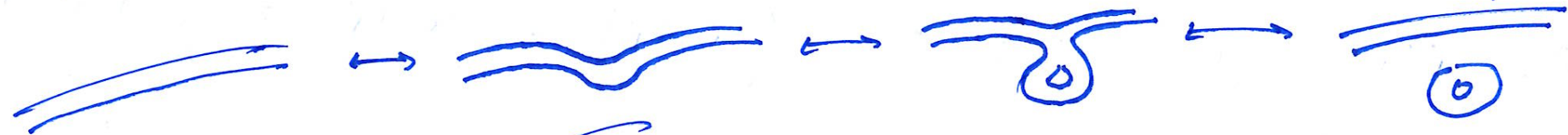
• Membrane - structure w/ one small dimension



Motivation □ Micro: the diverse and fascinating behaviour of cells highly linked to mechanics of cell membrane

Exs • Permeability

• Exo. endocytosis



• Cell migration



★ Large shape changes ★

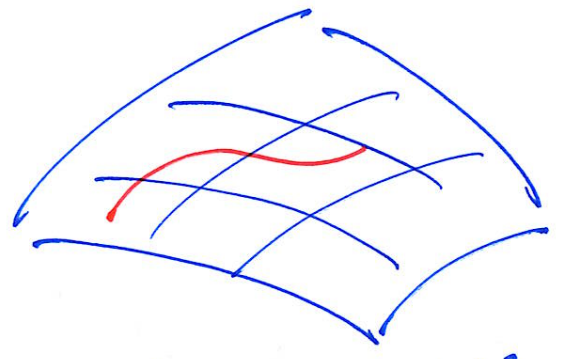
□ Macro - a sheet of cells → tissue mechanics, eg skin  
- in plants: leaves, petals Q: How do get shape?  
- Venus fly trap, rapid seed dispersal - rapid motion triggered by release of elastic energy

Plan: • Geometry of surfaces → Membrane energy → Energy minimisation

• Alt: force, moment balance (for axisymmetric)

Surface  $\underline{x}(\xi^1, \xi^2)$ ,  $\underline{r}_i = \frac{\partial \underline{x}}{\partial \xi^i}$ ,  $\underline{n} = \frac{|\underline{r}_1 \wedge \underline{r}_2|}{\|\underline{r}_1 \wedge \underline{r}_2\|}$ ,  $g_{ij} = \underline{r}_i \cdot \underline{r}_j$  metric tensor

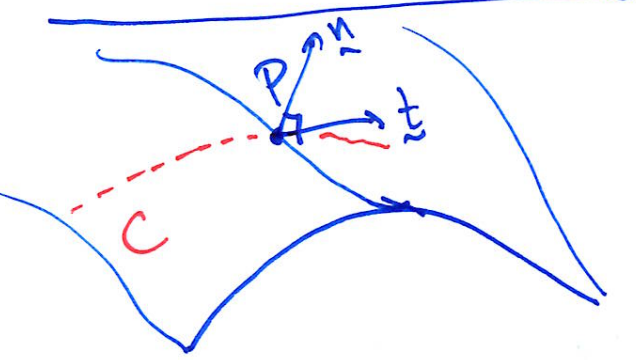
Arclength



given a path on  $\Sigma$ , the infinitesimal length is  $ds^2 = |\underline{x}(\xi^1 + d\xi^1, \xi^2 + d\xi^2) - \underline{x}(\xi^1, \xi^2)|^2$

(expand)  $= |\underline{r}_1 d\xi^1 + \underline{r}_2 d\xi^2|^2 = \underline{r}_1^2 (d\xi^1)^2 + \underline{r}_2^2 (d\xi^2)^2 + 2 \underline{r}_1 \cdot \underline{r}_2 d\xi^1 d\xi^2 = \boxed{g_{ij} d\xi^i d\xi^j}$   
 (summation notation)

So arclength  $L = \int_a^b \sqrt{g_{ij} \frac{d\xi^i}{dt} \frac{d\xi^j}{dt}} dt$  is first fundamental form  
 arclength of curve  $\underline{x}(\xi^1(t), \xi^2(t))$  for  $t \in [a, b]$



Consider curve  $C$  on  $\Sigma$  passing through pt  $P$  and parameterised by arclength  $s$ .  $\underline{t}(s) := \frac{d\underline{x}}{ds}$  is unit tangent.

Let  $\underline{k} := \frac{d\underline{t}}{ds}$ . We know  $|\frac{d\underline{t}}{ds}| = |K|$  curvature of  $C$

Let  $\underline{k} = -k_n \underline{n} + \underline{k}_g$  w/  $\underline{k}_g \cdot \underline{n} = 0$

Normal curvature  
 [sign so that sphere w/ outward normal has  $k_n > 0$ ]

$|\underline{k}_g| = k_g$  geodesic curvature  
 curve is curved relative to surface

Due to fact that surface is curved

$$\dot{\underline{x}} = \frac{d\underline{x}}{ds} = \frac{\partial \underline{x}}{\partial \xi^i} \frac{d\xi^i}{ds} = \underline{r}_i \frac{d\xi^i}{ds}$$

$$\Rightarrow \underline{\kappa} = \frac{d\underline{\dot{x}}}{ds} = \frac{d}{ds} \left( \underline{r}_i \frac{d\xi^i}{ds} \right) = \frac{\partial \underline{r}_i}{\partial \xi^j} \frac{d\xi^j}{ds} \frac{d\xi^i}{ds} + \underline{r}_i \frac{d^2 \xi^i}{ds^2}$$

$$\text{So } \kappa_n = -\underline{n} \cdot \underline{\kappa} = -\underline{n} \cdot \frac{\partial \underline{r}_i}{\partial \xi^j} \frac{d\xi^j}{ds} \frac{d\xi^i}{ds}$$

$$\underline{r}_i \cdot \underline{n} = 0$$

Define  $K_{ij}^{\parallel}$  - symmetric

$$\frac{\partial \underline{r}_i}{\partial \xi^j} = \frac{\partial^2 \underline{x}}{\partial \xi^i \partial \xi^j} = \frac{\partial \underline{r}_j}{\partial \xi^i}$$

$$\text{so } K_{ij} = K_{ji}$$

$$\text{Then } \kappa_n = K_{ij} \frac{d\xi^j}{ds} \frac{d\xi^i}{ds}$$

$K_{ij}$  is called extrinsic curvature tensor.

$K_{ij} d\xi^j d\xi^i$  is 2<sup>nd</sup> fundamental form

$g_{ij} = \underline{r}_i \cdot \underline{r}_j$  metric tensor

$K_{ij} = -\underline{n} \cdot \frac{\partial \underline{r}_i}{\partial \xi_j}$  curv. tensor

$k_n = K_{ij} \frac{d\xi^i}{ds} \frac{d\xi^j}{ds}$  normal curvature

Extremal values of  $k_n$

$K_{ij} d\xi^i d\xi^j = k_n ds^2 = k_n g_{ij} d\xi^i d\xi^j$

$\Rightarrow \left( (K_{ij} - k_n g_{ij}) \frac{d\xi^i}{ds} \frac{d\xi^j}{ds} = 0 \right)$

$g_{ij}, K_{ij}$  depend on surface only (& not on curve  $C$ ), while  $k_n$  depends on  $C$ , such that  $dk_n = 0$  at an extremal of varying

the paths of curves through  $P$ .



$\therefore$  Differentiate w.r.t.  $\frac{d\xi^i}{ds}$ :

$0 = (K_{ij} - g_{ij} k_n) \left( \delta_{ij}^p \frac{d\xi^j}{ds} + \frac{d\xi^i}{ds} \delta_{ij}^p \right) = \underbrace{(K_{pj} - g_{pj} k_n)}_{\text{same by symmetry}} \frac{d\xi^j}{ds} + \underbrace{(K_{ip} - g_{ip} k_n)}_{\text{same by symmetry}} \frac{d\xi^i}{ds}$

$= 2 (K_{pj} - g_{pj} k_n) \frac{d\xi^j}{ds}$

$\therefore 2 (g^{jp} K_{pj} - k_n g^{jp} g_{pj}) \frac{d\xi^j}{ds} = 0$

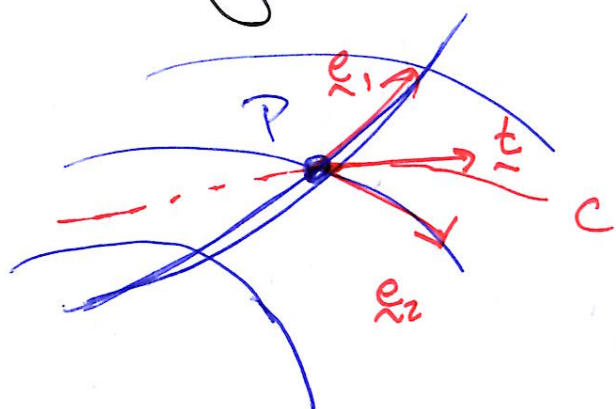
Same by symmetry of  $K_{ij}, g_{ij}$  where  $g^{jp} g_{pj} = \delta_j^j$

$(G^{-1} K - k_n \mathbb{1}) \frac{d\xi}{ds} = 0$

In matrix notation:

$\therefore$  Extremal values of  $k_n$  eigenvalues of  $L = G^{-1} K$

Let  $\underline{e}_1, \underline{e}_2$  denote the orthonormal eig' vectors of  $L$   
 w/ associated eig' values  $\underline{k_1, k_2}$



↑ principal curvatures

• can write  $\underline{t} = \cos\theta \underline{e}_1 + \sin\theta \underline{e}_2$  and (Euler 1760)  
 $K_n = k_1 \cos^2\theta + k_2 \sin^2\theta$

Def'n  $H = \frac{\text{Tr}(L)}{2} = \frac{k_1 + k_2}{2}$  mean curvature

$K_G = \det L = k_1 k_2$  Gaussian curvature - intrinsic to surface

•  $|H|$  is indep. of parameterisation, but  $H$  changes sign w/ dir. of normal vec.

Classification  $K_G > 0$  Elliptic,  $K_G < 0$  Hyperbolic,  $K_G = 0$  Parabolic

Gauss-Bonnet Thm Let  $\Sigma$  be compact surface w/ bdy  $\partial\Sigma$ . Then

$$\int_{\Sigma} K_G dS + \int_{\partial\Sigma} k_g d\ell = 2\pi \chi(\Sigma)$$

Euler-characteristic for surface of genus  $P$   
 $= 2 - 2P$   
 sphere - genus 0  
 torus - genus 1

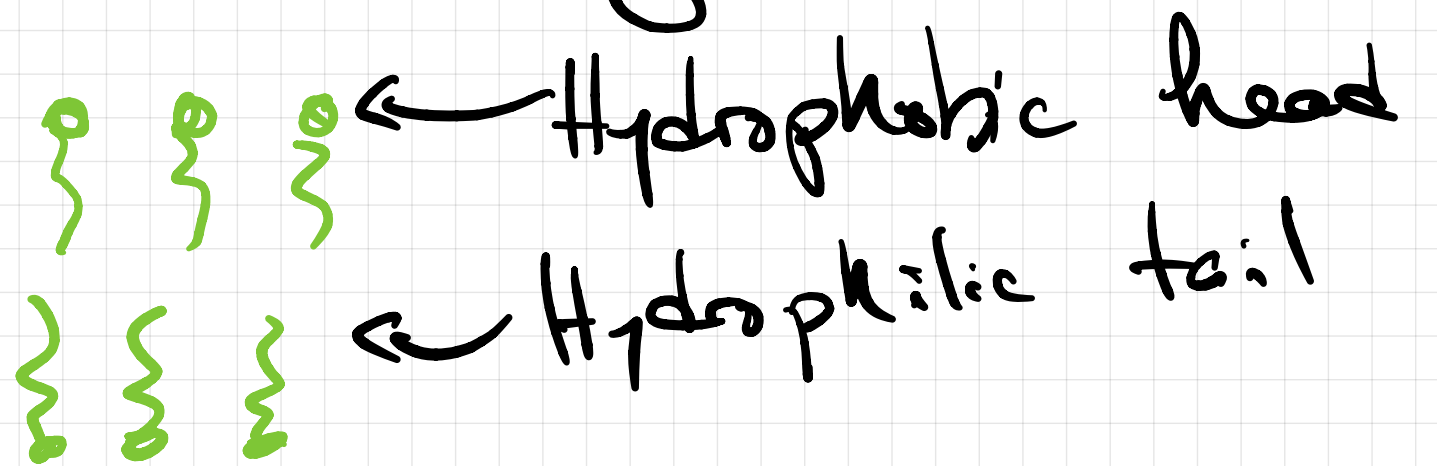
∴ For closed surface,  
 $\int_{\Sigma} K_G dS = 4\pi(1-P)$   
const.

# Fluid biomembranes

Assumptions: - sufficiently thin so that  
can be treated as surface  $\Sigma$

- No resistance to shear, but resists bending & stretching

eg, lipid bilayer



- Free energy given by (Helfrich 1973):

$$E = \int dS \left( \gamma + 2\kappa (H - H_0)^2 + \bar{\kappa} K_G \right)$$

saddle  
-splay  
modulus

Bending  
modulus

intrinsic  
mean  
curv.

Surface tension

Note  $2\kappa H^2 = \frac{\kappa}{2} (k_1 + k_2)^2 \Rightarrow$  if flat in one-dir.,

then  $k_2 = 0 \Rightarrow K_G = 0 \rightarrow$  recovers "beam energy"

Goal find shape that minimizes  $E$ , given ref. shape

- if extra constraints, add Lagrange multiplier

- eg, if fixed Volume -  $V = V_0$ , minimise  $E - P(V - V_0)$

Lagrange  
multiplier  
(pressure)



For closed surface, Gauss-Bonnet  $\Rightarrow$  can ignore  $K_G$

Estimates  $[H] = \frac{1}{\text{length}} \Rightarrow [K] = \text{Energy}$

$[Y] = \frac{\text{Energy}}{\text{length}^2} \Rightarrow \left(\frac{K}{Y}\right)^{\frac{1}{2}} =: \lambda$  characteristic length at which both bending & tension matter

If  $L$  is lengthscale of variation in membrane:  $L \gg \lambda \Rightarrow$  surface tension dominant

eg lipid bilayer:  $L \ll \lambda \Rightarrow$  bending dominant

$K \approx 10^{-19} \text{ J}, Y \approx 10^{-3} \frac{\text{N}}{\text{m}} = 10^{-3} \frac{\text{J}}{\text{m}^2} \Rightarrow \lambda \approx 10^{-8} \text{ m}$

$\therefore$  For  $L \gg 10 \text{ nm} \Rightarrow$  surface tension dominates  $\rightarrow$  will form approx. sphere

[Recipe: - parameterisation  $\rightarrow G, K \rightarrow L = G^{-1}K$

$\rightarrow K_1, K_2 \rightarrow H, K_G \rightarrow \Sigma \rightarrow$  Euler-Lagrange

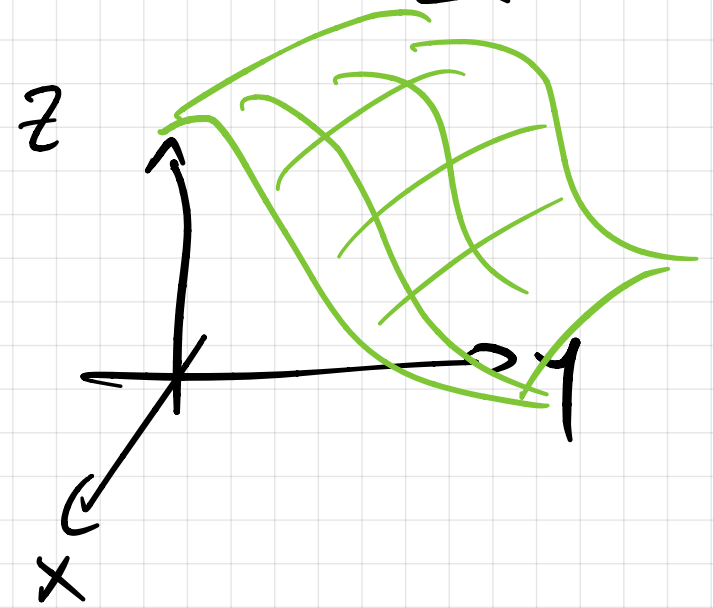
↓  
Shape

Monge Representation - consider surface  $\Sigma$  as

function

$$z = h(x, y) \in C^2,$$

$$(x, y) \in U \subset \mathbb{R}^2$$



$$\vec{r} = (x, y, h(x, y))$$

$$\rightarrow \vec{r}_1 = \frac{\partial \vec{r}}{\partial x} = (1, 0, h_x) \Rightarrow$$

$$\vec{r}_2 = (0, 1, h_y)$$

$$\vec{n} = \frac{\vec{r}_1 \wedge \vec{r}_2}{\|\vec{r}_1 \wedge \vec{r}_2\|} = \frac{(h_x, h_y, -1)}{\sqrt{1+h_x^2+h_y^2}}$$

Metric tensor  
matrix

$$G = \begin{pmatrix} r_1^2 & r_1 \cdot r_2 \\ r_1 \cdot r_2 & r_2^2 \end{pmatrix} = \begin{pmatrix} 1+h_x^2 & h_x h_y \\ h_x h_y & 1+h_y^2 \end{pmatrix}$$

$$\Rightarrow G^{-1} = \frac{1}{\det G} \begin{pmatrix} 1+h_y^2 & -h_x h_y \\ -h_x h_y & 1+h_x^2 \end{pmatrix}$$

$$\det G = 1+h_x^2+h_y^2$$

// call

$$g = \frac{\partial r_i}{\partial x_j}$$

Now compute

$$K = (K_{ij})$$

$$\rightarrow K = \sqrt{g} \begin{pmatrix} h_{xx} & h_{xy} \\ h_{xy} & h_{yy} \end{pmatrix}$$

Can now compute  $L = G^{-1}K$ , from which

we get  $\chi_G = \det L = \det G^{-1} \det K = \frac{h_{xx}h_{yy} - h_{xy}^2}{g^2}$

$\&$   $H = \frac{\text{tr}(L)}{2} = \frac{1}{2g^{3/2}} (h_{xx}(1+h_y^2) + h_{yy}(1+h_x^2) - 2h_{xy}h_xh_y)$

Simple case - Surface tension only - set  $\kappa = \kappa_G = 0$

$\gamma$  const  $\rightarrow \mathcal{E} = \gamma \int dS$  (wants to minimize surface area)

$$\mathcal{E} = \gamma \int_M \sqrt{\det G} d\xi^1 d\xi^2 = \gamma \int \underbrace{\sqrt{1 + h_x^2 + h_y^2}}_{\text{call } \mathcal{L}(h, h_x, h_y)} dx dy$$

Calc. of variations - Euler Lagrange eqn:

$$\frac{\partial}{\partial x} \left( \frac{\partial \mathcal{L}}{\partial h_x} \right) + \frac{\partial}{\partial y} \left( \frac{\partial \mathcal{L}}{\partial h_y} \right) - \frac{\partial \mathcal{L}}{\partial h} = 0$$

$$\rightarrow \frac{\partial}{\partial x} \left( \frac{h_x}{\sqrt{1+h_x^2+h_y^2}} \right) + \frac{\partial}{\partial y} \left( \frac{h_y}{\sqrt{1+h_x^2+h_y^2}} \right) = 0$$

Note: Same as  $\nabla \cdot \left( \frac{\nabla h}{\sqrt{g}} \right) = 0$   $\left( \nabla \equiv e_x \frac{\partial}{\partial x} + e_y \frac{\partial}{\partial y} \right)$

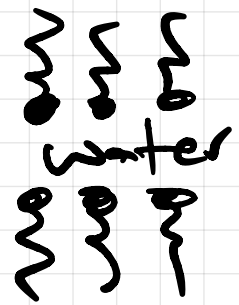
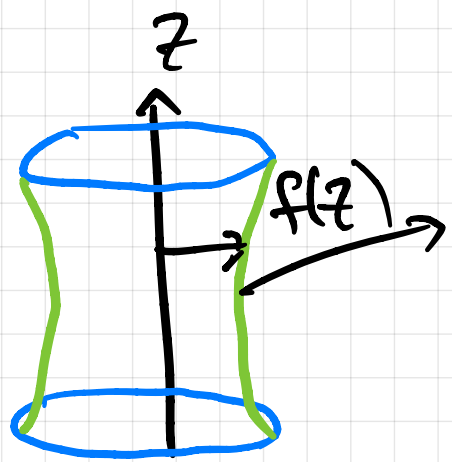
Same as  $H = 0$  or equiv.  $\nabla \cdot \underline{n} = 0$

Surface w/ zero mean curvature  
 - called a minimal surface  $\rightarrow$  locally minimizes surface at every pt.

Note:  $H=0 \Rightarrow k_1 = -k_2 \Rightarrow K_G \leq 0$  (w/ equality only if  $k_1 = k_2 = 0$  i.e. flat!)

$\Rightarrow$  minimal surfaces are saddle shaped

Ex. Soap film spanning any boundary  
 - consider soap film b/t two rings  
 - surface of revolution



Bilayer  
 w/  
 $L \gg \lambda$

$$x = \begin{pmatrix} f(z) \cos \theta \\ f(z) \sin \theta \\ z \end{pmatrix}$$

Then  $\vec{r}_1 = \frac{\partial \vec{x}}{\partial z} = \begin{pmatrix} f' \cos \theta \\ f' \sin \theta \\ 1 \end{pmatrix}$ ,  $\vec{r}_2 = \frac{\partial \vec{x}}{\partial \theta} = \begin{pmatrix} -f \sin \theta \\ f \cos \theta \\ 0 \end{pmatrix}$

$\rightarrow G = \begin{pmatrix} 1+f'^2 & 0 \\ 0 & f^2 \end{pmatrix} \Rightarrow \Sigma = \int_a^b \int_0^{2\pi} \sqrt{\det G} \, d\theta \, dz$

w/  $\sqrt{\det G} = f(z) \sqrt{1+f'^2} \stackrel{||G||}{=} F(f, f')$

Euler-Lagrange  $\rightarrow \frac{1+f'^2 - f f''}{(1+f'^2)^{3/2}} = 0$

[same as  $H=0$ ]



Better: Beltrami identity -  $\frac{\partial F}{\partial z} = 0$

$$\rightarrow F - f' \frac{\partial F}{\partial f'} = c \text{ (const)} \rightarrow \text{1st integral}$$

$$\rightarrow \frac{f}{\sqrt{1+f'^2}} = c$$

(can solve for  $f'$ ,  
separate and integrate  
...  $f = A \cosh(Bz)$ )

Catenoid

# Small Gradient Approx.

Keep  $\bar{x} = H_0 = 0$  but w/  $\kappa \neq 0$  and

Suppose  $|h_x|, |h_y| \ll 1$

Then  $\sqrt{g} = (1 + h_x^2 + h_y^2)^{\frac{1}{2}} \approx 1 + \frac{1}{2}(h_x^2 + h_y^2) + O(\nabla h^3)$

$\Rightarrow (2H)^2 = \frac{1}{g^3} (h_{xx} + h_{yy} + O(\nabla h^3))^2 = \underbrace{(h_{xx} + h_{yy})^2}_{\text{red underline}} (1 + O(\nabla h)^2)$

$\therefore \mathcal{E} = \int dS (\gamma + 2\kappa H^2) = \int dx dy \sqrt{g} (\gamma + 2\kappa H^2) = \int dx dy \left(1 + \frac{1}{2}(\nabla h)^2\right) \left(\gamma + 2\kappa(\nabla^2 h)^2\right) + \dots$

$= \int dx dy \left( \gamma + \frac{1}{2} \gamma (\nabla h)^2 + \frac{1}{2} \kappa (\nabla^2 h)^2 \right) + \dots$

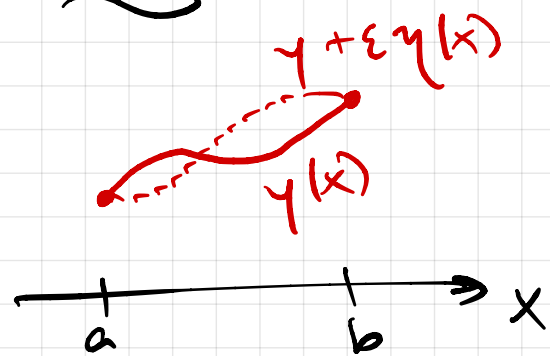
$\gamma$  const - so want impact minimisation

Recall Calc. of variations

$\mathcal{E}[y(x)] = \int_a^b F(x, y(x), y'(x), \dots) dx$

$y(x)$  is an extremum of  $\mathcal{E}$  if

$\frac{d}{d\epsilon} \mathcal{E}[y(x) + \epsilon \eta(x)] \Big|_{\epsilon=0} = 0 \quad \forall \eta(x)$



Expand in  $\epsilon$ , int. by parts  $\rightarrow$

$\int \left( \dots \right) \eta(x) dx + \text{BT} = 0$   
 Euler-Lagrange

Variation:  $\left. \frac{d}{d\varepsilon} \mathcal{E} [h(x,y) + \varepsilon \eta(x,y)] \right|_{\varepsilon=0} = \int_{\mathcal{U}} dx dy \left( \underbrace{\gamma \nabla h \cdot \nabla \eta}_{\substack{= \\ \nabla \cdot (\eta \nabla h) - \eta \nabla^2 h}} + \kappa \underbrace{\nabla^2 h \nabla^2 \eta}_{\substack{= \\ \nabla \cdot (\eta \nabla^2 h) - \eta \nabla^4 h}} \right)$

$= \int_{\partial \mathcal{U}} \left( \gamma \nabla h \cdot \underline{\tilde{N}} + \kappa (\nabla \eta \nabla^2 h) \cdot \underline{\tilde{N}} \right) ds - \int_{\mathcal{U}} dx dy \left( \gamma \nabla^2 h \eta + \kappa \nabla \nabla^2 h \nabla \eta \right)$

$= \int_{\partial \mathcal{U}} \left[ \eta \left( \underbrace{\gamma \nabla h - \kappa \nabla \nabla^2 h}_{\text{(A)}} + \underbrace{\kappa \nabla \eta \nabla^2 h}_{\text{(B)}} \right) \cdot \underline{\tilde{N}} ds - \int_{\mathcal{U}} dx dy \left( \gamma \nabla^2 h - \kappa \nabla^4 h \right) \eta \right] = 0$

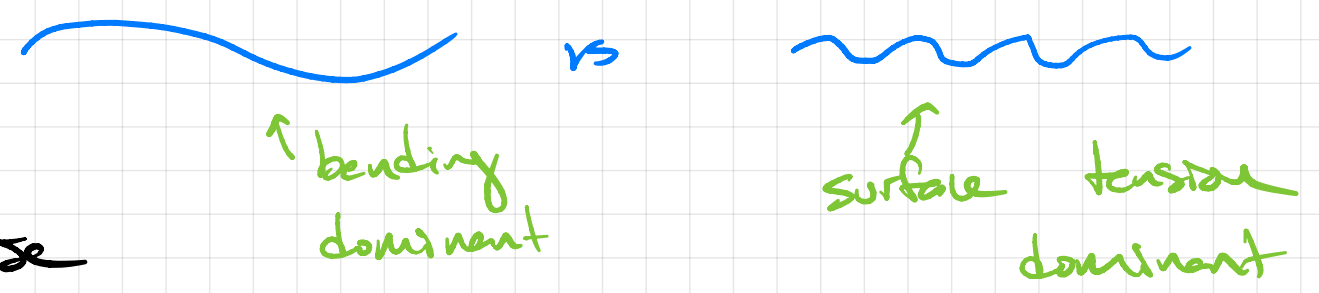
For extremum, we require  $\boxed{\nabla^4 h - \frac{1}{\lambda^2} \nabla^2 h = 0}$ ,  $\lambda := \sqrt{\frac{\kappa}{\gamma}}$   
 (Note;  $\lambda \ll 1 \Rightarrow$  singular pert. problems!)

Bdy cond: Need (A) and (B) to vanish.

- If impose  $h$  at bdy  $\Rightarrow$  must impose  $\eta = 0$  at bdy then (A) already 0,  $\therefore$  require  $\nabla^2 h = 0$  on bdy
- If impose  $\nabla h \cdot \underline{\tilde{N}}$  on bdy  $\Rightarrow$  must impose  $\nabla \eta \cdot \underline{\tilde{N}} = 0$  on bdy so (B) already 0, require  $\left( \nabla h - \frac{1}{\lambda^2} \nabla (\nabla^2 h) \right) \cdot \underline{\tilde{N}} = 0$  on bdy

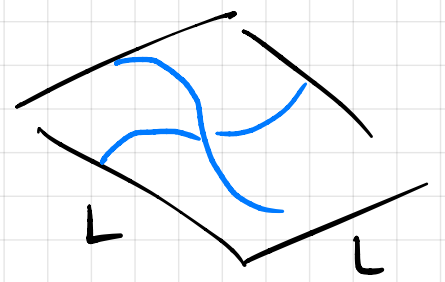
Flicker spectroscopy - Study biomembrane mechanics by measuring spectrum of

thermal undulations via light microscopy



- Small gradients - linear eqns, so can use Fourier methods

- Square membrane



seek  $h(x,y) = h(\underline{r}) = \sum_{\underline{g}} h_{\underline{g}} e^{i\underline{g} \cdot \underline{r}}$   
 $\underline{g} = \frac{2\pi}{L} (n_x, n_y), n_x, n_y \in \mathbb{Z}$  Fourier modes

$h_{\underline{g}} \in \mathbb{C}$  Fourier coeffs,  $h$  real  $\rightarrow h_{-\underline{g}} = \overline{h_{\underline{g}}}$

Then  $\nabla h = \sum_{\underline{g}} i\underline{g} h_{\underline{g}} e^{i\underline{g} \cdot \underline{r}} \Rightarrow (\nabla h)^2 = \sum_{\underline{g}, \underline{g}'} -\underline{g} \cdot \underline{g}' h_{\underline{g}} h_{\underline{g}'} e^{i\underline{r} \cdot (\underline{g} + \underline{g}')}$

And  $\nabla^2 h = \sum_{\underline{g}} -g^2 h_{\underline{g}} e^{i\underline{g} \cdot \underline{r}} \Rightarrow (\nabla^2 h)^2 = \sum_{\underline{g}, \underline{g}'} g^2 g'^2 h_{\underline{g}} h_{\underline{g}'} e^{i\underline{r} \cdot (\underline{g} + \underline{g}')}$

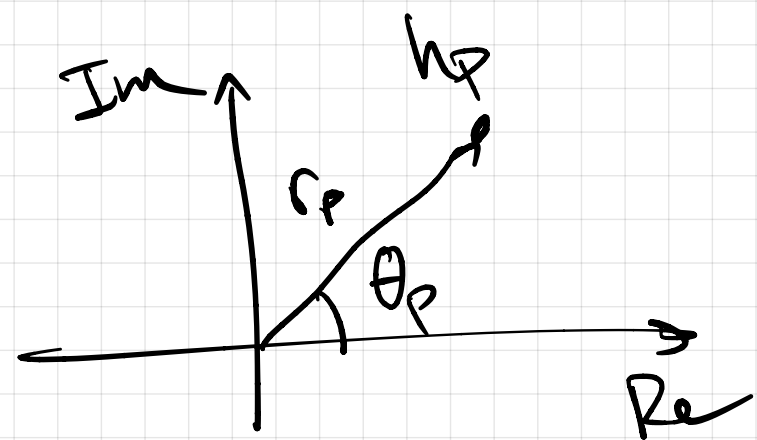
$\therefore E = \frac{1}{2} \int_0^L dx dy \sum_{\underline{g}, \underline{g}'} h_{\underline{g}} h_{\underline{g}'} e^{i\underline{r} \cdot (\underline{g} + \underline{g}')} (k g^2 g'^2 - \gamma \underline{g} \cdot \underline{g}')$

Orthogonality:  $\int_0^L dx dy e^{i\mathbf{r} \cdot (\mathbf{g} + \mathbf{g}')} = L^2 \delta_{\mathbf{0}, \mathbf{g} + \mathbf{g}'}$

$\Rightarrow \mathcal{E} = \frac{L^2}{2} \sum_{\mathbf{g}} h_{\mathbf{g}} h_{-\mathbf{g}} (\kappa_{\mathbf{g}}^4 - \gamma_{\mathbf{g}}^2) = \boxed{\frac{L^2}{2} \sum_{\mathbf{g}} |h_{\mathbf{g}}|^2 (\kappa_{\mathbf{g}}^4 - \gamma_{\mathbf{g}}^2)}$

Goal compute  $\langle |h_p|^2 \rangle$  for a given mode  $\mathbf{p} = \frac{2\pi}{L} (p_x, p_y)$

state:  $\{h_1, h_2, \dots\}$   $\hookrightarrow \int D[h] |h_p|^2 P(\{h_1, h_2, \dots\})$



$h_p \in \mathbb{C}$ , so can write  $h_p = r_p e^{i\theta_p}$

$= \frac{e^{-\beta \mathcal{E}(\{h_1, h_2, \dots\})}}{Z}$ ,  $\beta = \frac{1}{k_B T}$

$-\frac{\beta L^2}{2} \sum_{\mathbf{g}} r_{\mathbf{g}}^2 f(\mathbf{g}) \rightarrow f(\mathbf{g}) := \kappa_{\mathbf{g}}^4 - \gamma_{\mathbf{g}}^2$

Then  $Z = \int \prod_m dr_m r_m d\theta_m e$

$$\langle |h_p|^2 \rangle = \frac{1}{Z} \int \prod_m dr_m d\theta_m r_m \underbrace{r_p^2}_{\text{circled}} e^{-\frac{\beta L^2}{2} \sum_{i,j} r_i^2 r_j^2 f(i,j)}$$

Key: has all same integrals as  $Z$ , except at  $m=p$

$\therefore$  everything cancels w/ matching term in  $Z$  except:

$$\langle |h_p|^2 \rangle = \frac{\int_0^\infty dr_p r_p^3 e^{-\frac{\beta L^2}{2} r_p^2 f(p)} \int N_p}{\int_0^\infty dr_p r_p e^{-\frac{\beta L^2}{2} r_p^2 f(p)}} \quad \text{We observe}$$

$$\frac{\partial}{\partial \beta} \ln(I_p) = \frac{-1}{\frac{\beta L^2}{2} f(p)} \cdot N_p$$

$$\therefore \langle |h_p|^2 \rangle = \frac{-1}{\frac{\beta L^2}{2} f(p)} \underbrace{\frac{\frac{\partial}{\partial \beta} \ln(I_p)}{I_p}}_{\text{call } I_p} \Rightarrow \frac{\partial}{\partial \beta} \ln I_p = -\frac{1}{\beta}$$

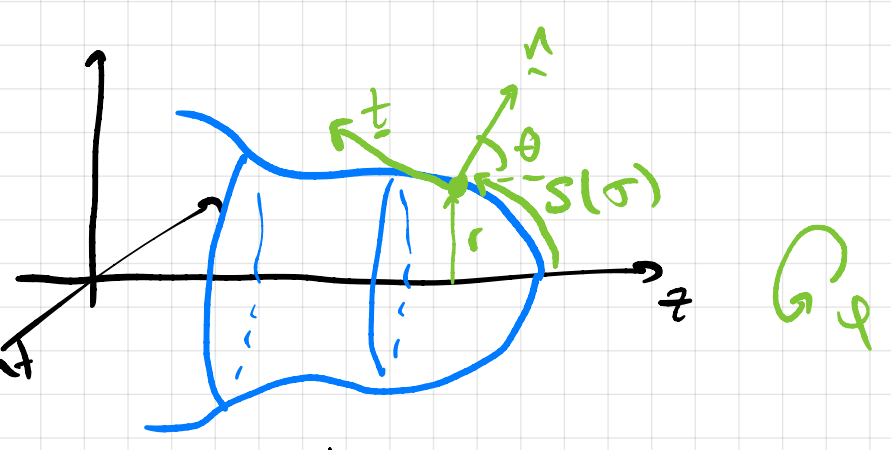
$$\therefore \langle |h_p|^2 \rangle = \frac{2k_B T}{L^2 (\chi_p^4 - \gamma_p^2)}$$

# Axisymmetric Membranes & Shells

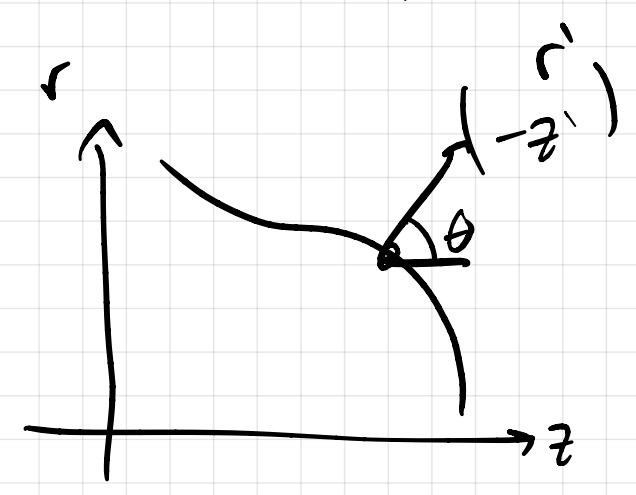
1. Kinematics - we take the membrane to be a surface of revolution

w/:

- $\vec{n}$  unit normal
- $\vec{t} = \vec{e}_s$  unit tangent



- in dir. of increasing arc length  $s$
- $\sigma$  arc length before deformation - material parameter
- $r$  radius, distance from  $z$ -axis

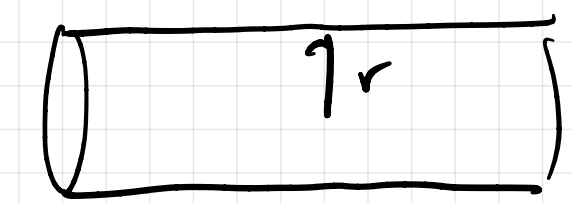


Trigonometry gives:

$$\frac{dr}{ds} = \cos\theta, \quad \frac{dz}{ds} = -\sin\theta$$

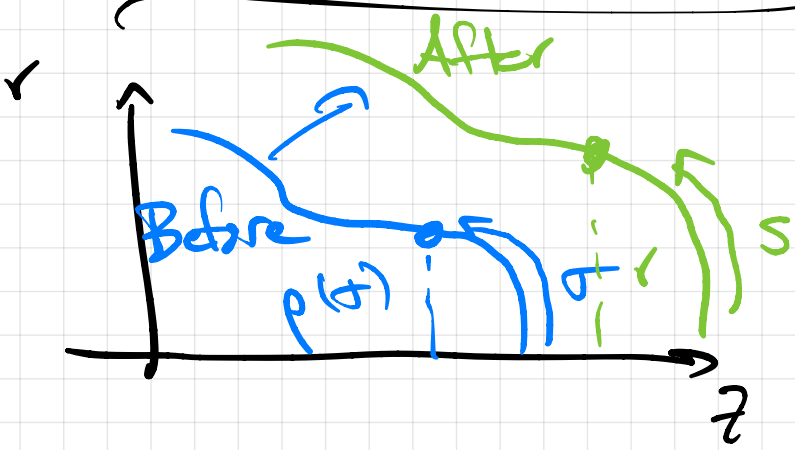
Principal curvatures:

$$k_s = \frac{d\theta}{ds}, \quad k_\varphi = \frac{\sin\theta}{r}$$



$$k_\varphi = \frac{1}{r}$$

Stretch variables



- stretch is  $s$ -direction
- radial stretch

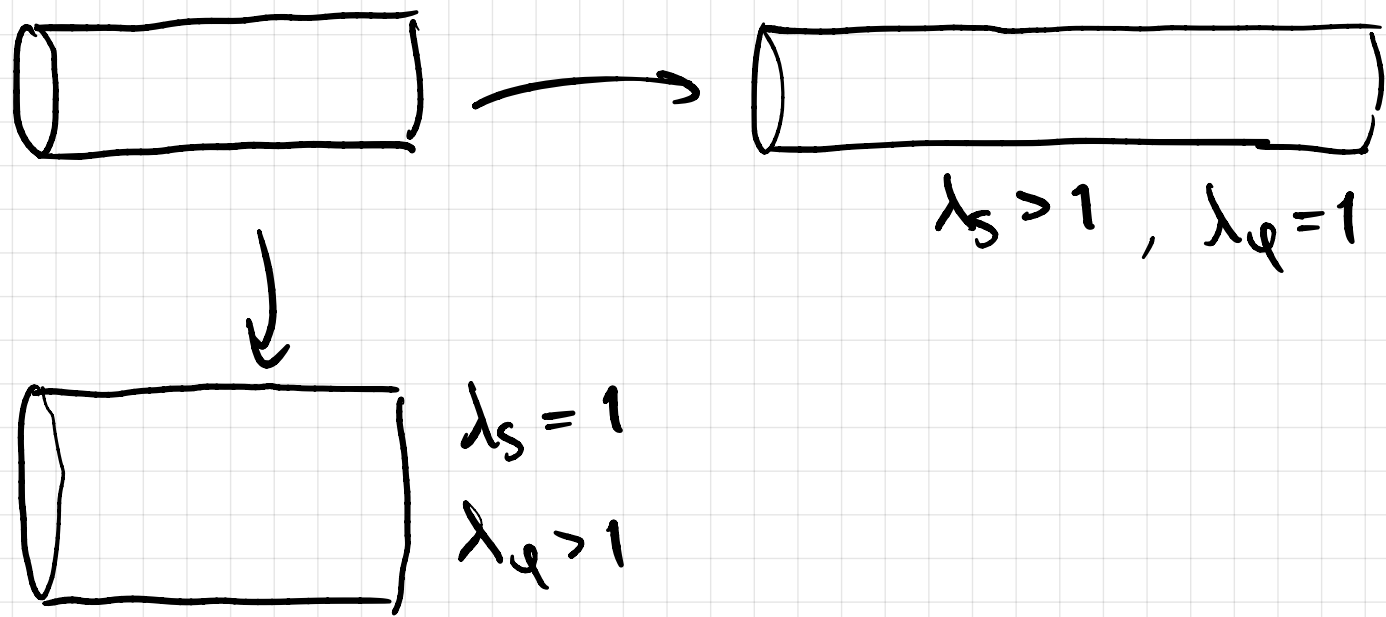
$$\lambda_s = \frac{\partial s}{\partial \sigma}$$

$$\lambda_\varphi = \frac{r}{\rho}$$

$\theta \approx 0$



$$k_\varphi \approx 0$$



Mechanics - Consider an element of membrane associated

w/ section  $[s, s + \Delta s]$ ,  $[\phi, \phi + \Delta \phi]$  subject to:

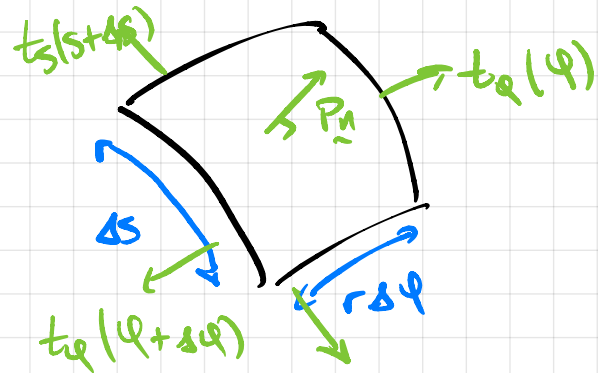
i) Pressure,  $P_{int}$ , eq due to pressurized internal fluid

ii) Tension on surface  $\underline{T} = t_s \underline{e}_s + t_\phi \underline{e}_\phi$    
 unit vector in direction of increasing azimuthal angle  $\phi$

iii) A force per unit area  $\underline{F} = f \underline{e}_s$    
 due to external fluid movement   
 to maintain axisymmetry



Zoom in on surface element:



Force balance (ignore inertia)

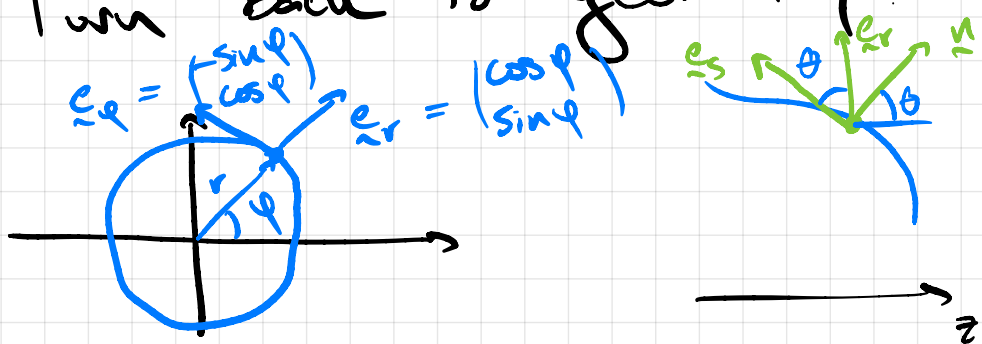
$$\Delta s \Delta \phi \left[ \frac{\partial}{\partial s} (r t_s \underline{e}_s) + \frac{\partial}{\partial \phi} (t_\phi \underline{e}_\phi) + r P \underline{n} + r f \underline{e}_s \right] = \underline{0}$$

(neglecting higher order terms)

(Goal: express ito  $\underline{e}_s, \underline{n}$  components)

you'd have  $r(s+\Delta s) t_s(s+\Delta s) \underline{e}_s(s+\Delta s) \Delta \phi - r(s) t_s(s) \underline{e}_s(s) \Delta \phi$

Turn back to geometry:



$$\underline{e}_r = \cos \theta \underline{e}_s + \sin \theta \underline{n}$$

$$\Rightarrow \frac{\partial \underline{e}_\phi}{\partial \phi} = -\underline{e}_r = -\cos \theta \underline{e}_s - \sin \theta \underline{n}$$

Also require  $\frac{\partial t_\phi}{\partial \phi} = 0$

for axisymm.

Also, recall  $\underline{e}_s = \underline{t}$ , and so

$$\frac{\partial \underline{e}_s}{\partial s} = \frac{\partial \underline{t}}{\partial s} = -\kappa_s \underline{n} \text{ by defn of curvature}$$

Observe: if  $t_s = t_\phi = t$

$$P = 2tH$$

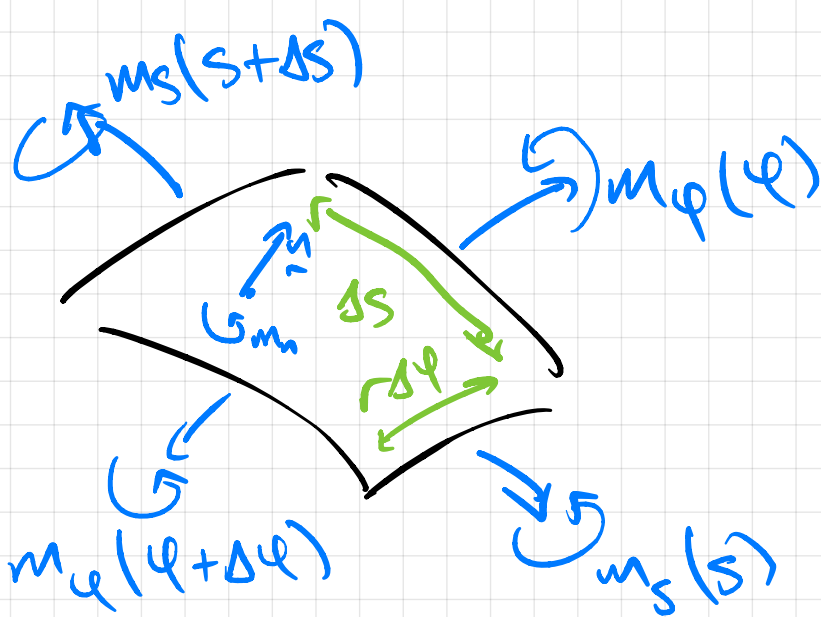
∴ Force balance becomes:

$$\underline{0} = \underline{e}_s \left[ \frac{\partial}{\partial s} (r t_s) - t_\phi \cos \theta + r f \right] + \underline{n} \left[ -r t_s \kappa_s - t_\phi \sin \theta + r P \right]$$

$$P = t_s \kappa_s + t_\phi \frac{\sin \theta}{r} = t_s \kappa_s + t_\phi \kappa_\phi$$

$$\frac{\partial}{\partial s} (r t_s) = t_\phi \cos \theta - r f = t_\phi \frac{\partial r}{\partial s} - r f$$

# Moment balance



Balancing moments in section gives:

$$\delta s \delta \phi \left[ \frac{\partial}{\partial s} (r m_s \underline{e}_s) + \frac{\partial}{\partial \phi} (m_\phi \underline{e}_\phi) + m_n \underline{e}_n \right] = 0$$

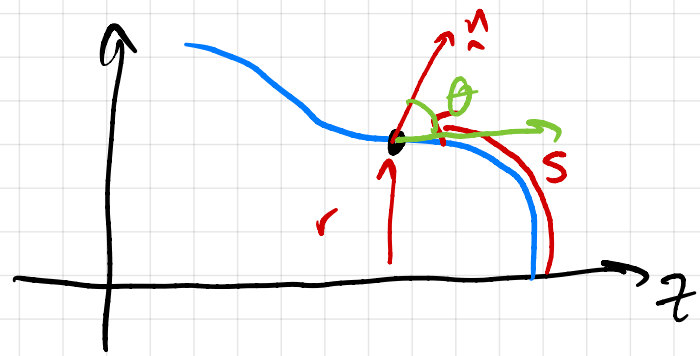
Again, use  $\frac{\partial}{\partial \phi} \underline{e}_\phi = -\cos\theta \underline{e}_s - \sin\theta \underline{e}_n$

$$\rightarrow \left[ \frac{\partial}{\partial s} (r m_s) - m_\phi \cos\theta = 0 \right] \underline{e}_s \text{ comp.}$$

$\underline{e}_n$  component gives  $m_n$  in terms of  $m_s, m_\phi$ ,  
but not needed, because  $m_n$  not imposed.

# Constant Pressure Case ( $f=0$ )

Claim  $P = \text{const} \Rightarrow r^2 (2t_s \kappa_\varphi - P) = \text{const}$



Force balance: (i)  $P = t_s \kappa_s + t_\varphi \kappa_\varphi$   
 $= t_s \theta' + t_\varphi \frac{\sin \theta}{r}$

(ii)  $(r t_s)' = t_\varphi r'$ ,  $(r' = \cos \theta)$

Pf  $(r^2 P)' = 2 r r' P = 2 r r' t_s \kappa_s + 2 \underbrace{r r' t_\varphi \kappa_\varphi}_{\substack{\text{sin } \theta \\ \text{|| (ii)} \\ (r t_s)'}} = (2 r t_s \sin \theta)'$   
 $= 2 (r^2 \kappa_\varphi t_s)'$

$\therefore r^2 P - 2 r^2 \kappa_\varphi t_s = \text{const} \quad \checkmark$

Observe: if surface crosses  $z$ -axis, so  $r=0$  at a point,

then  $\text{const} = 0 \Rightarrow \boxed{P = 2 \kappa_\varphi t_s}$  (Young-Laplace law)

Constitutive laws. We need to relate  $t_s$  and  $t_\varphi$  to the deformation of the membrane, defined by the stretch ratios  $\lambda_s = \frac{ds}{ds}$ ,  $\lambda_\varphi = \frac{r}{r}$

[there is a 3<sup>rd</sup> stretch, in normal direction,  $\lambda_3$   
 for incompressible material (volume doesn't change),

$$\lambda_3 = \frac{1}{\lambda_s \lambda_\varphi}$$

General form:  $t_s = A f_s(\lambda_s, \lambda_\varphi)$ ,  $t_\varphi = A f_\varphi(\lambda_s, \lambda_\varphi)$  such that  $f_s(1,1) = 0$   
 $f_\varphi(1,1) = 0$

Standard moment constit relation

$$m_s = m_\varphi = B (k_s + k_\varphi - k_0)$$

↑ isotropic
sum of curvatures in stress-free config.

Recall: moment balance:  $\frac{d}{ds}(r m_s) - m_\varphi \cos\theta = 0$

"  $m_s$ 
"  $\frac{dr}{ds}$

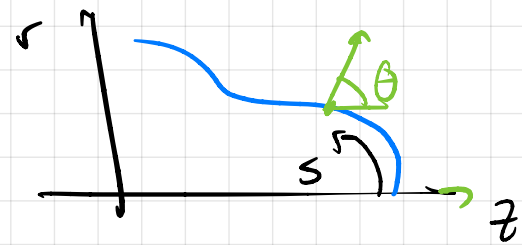
$$\Rightarrow \frac{dm_s}{ds} = 0 \Rightarrow \frac{d}{ds} k_s + \frac{d}{ds} k_\varphi = 0 \quad (\text{if } k_0 = \text{const})$$

$$\Rightarrow k_s + k_\varphi = k_1 \quad \text{const}$$

$$\text{ie } \boxed{k_s = k_1 - \frac{\sin\theta}{r}}$$

# Workspace

• Geometry



$$r' = \cos\theta$$

$$z' = -\sin\theta$$

$$r = \frac{d}{ds}$$

$$k_s = \theta', \quad k_\varphi = \frac{\sin\theta}{r}$$

• MB  
(isotropic)

$$\frac{dm_s}{ds} = 0$$

• CL  $m_s = B(k_s + k_\varphi - k_0)$

• FB  $P = t_s k_s + t_\varphi k_\varphi$  • CL :  $t_s = A f_s(k_s, \frac{r}{\rho})$

$$(r t_s)' = r' t_\varphi$$

$$t_s' = \frac{r'}{r} (t_\varphi - t_s)$$

$$t_\varphi = A f_\varphi(k_s, \frac{r}{\rho})$$

# Closed System

$$\frac{ds}{d\sigma} = \lambda_s$$

$$\frac{dr}{d\sigma} = \lambda_s \cos\theta$$

$$\frac{dz}{d\sigma} = -\lambda_s \sin\theta$$

$$\frac{dm_s}{d\sigma} = 0$$

$$\frac{d\theta}{d\sigma} = \lambda_s k_s$$

$$\frac{dt_s}{d\sigma} = \frac{A \cos\theta}{r} (f_\varphi(k_s, \frac{r}{\rho}) - f_s(k_s, \frac{r}{\rho}))$$

$$P = t_s k_s + A f_\varphi(k_s, \frac{r}{\rho}) \frac{\sin\theta}{r}$$

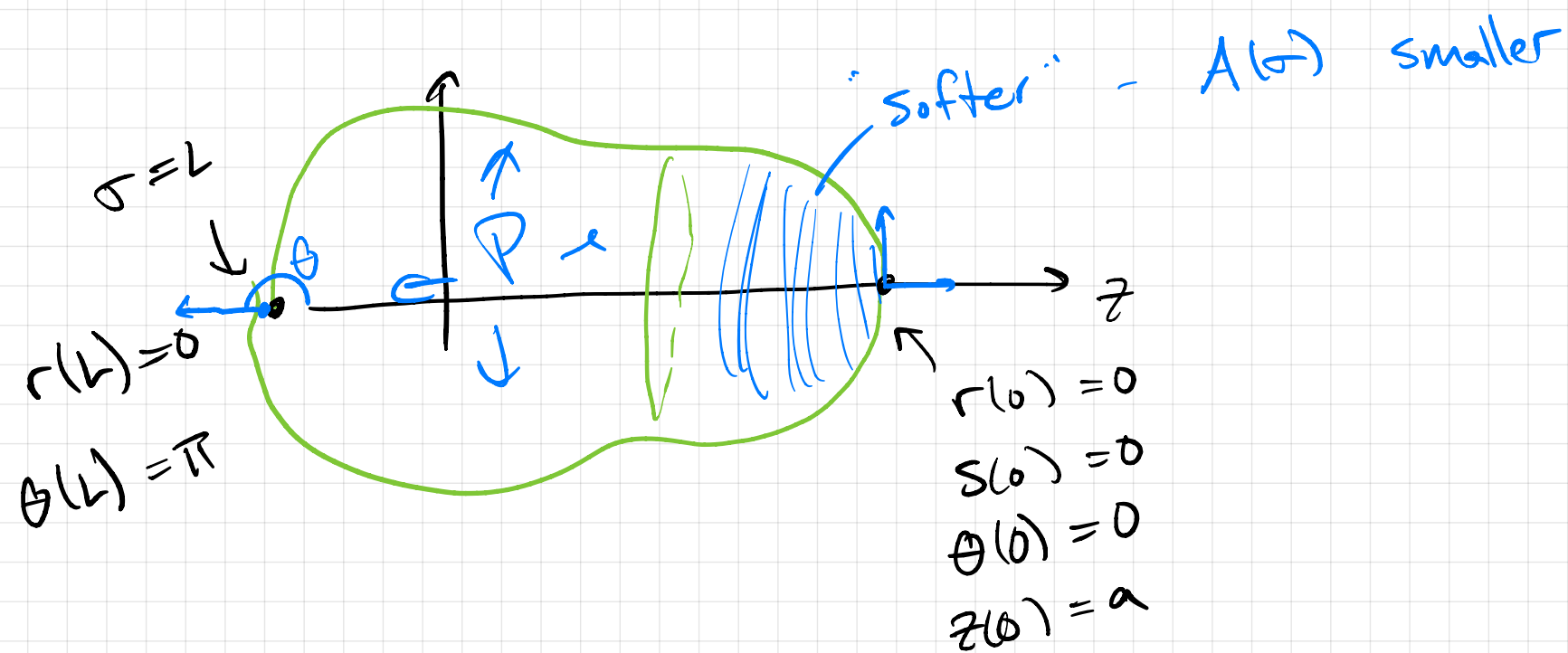
$$m_s = B(k_s + \frac{\sin\theta}{r} - k_0)$$

6 ODEs + 2 Algebraic for

$\{s, r, z, m_s, \theta, t_s, \lambda_s, k_s\}$  functions of  $\sigma$

- Notes:
  - $f_s, f_p$  known  $f_{ns}$
  - $B, A, K_0$  all material properties,
    - $K_0$  assumed known
    - $= K_{s_0} + K_{p_0}$  could be worked out from  $\{p(\sigma), z_0(\sigma)\}$
  - Typical problem: impose  $P$  (plus BC), determine deformed shape

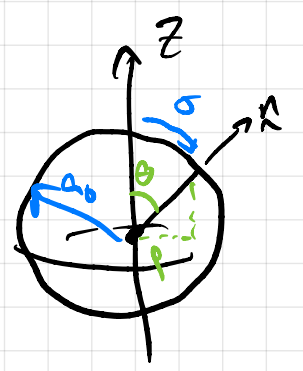
Ex. Pressurised cell w/ variable stiffness -  $A = A(\sigma)$



Ex. - Inflation of a Sphere - Consider a sphere of radius  $a_0$  in

undeformed state. Suppose the pressure is increased to  $P^*$ . Find the deformed radius  $a$ .

Initial  
( $\lambda_s = \lambda_\varphi = 1$ )

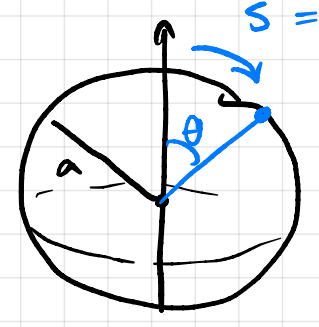


$\sigma = a_0 \theta$       Geometry: ( $r' = \frac{d}{d\sigma}$ )

$$\left. \begin{aligned} z_0' &= -\sin\theta = -\sin\left(\frac{\sigma}{a_0}\right) \\ r' &= \cos\theta \end{aligned} \right\} \Rightarrow \begin{aligned} z_0 &= a_0 \cos\left(\frac{\sigma}{a_0}\right) \\ r &= a_0 \sin\left(\frac{\sigma}{a_0}\right) \end{aligned}$$

$z_0(0) = a_0$   
 $r(0) = 0$

Deformed



$s = a\theta = \frac{a}{a_0} \sigma \Rightarrow \lambda_s = \frac{ds}{d\sigma} = \frac{a}{a_0}$

$$\left. \begin{aligned} z' &= -\lambda_s \sin\theta \\ r' &= \lambda_s \cos\theta \end{aligned} \right\} \rightarrow \begin{aligned} z(\sigma) &= a \cos\left(\frac{\sigma}{a_0}\right) \\ r(\sigma) &= a \sin\left(\frac{\sigma}{a_0}\right) \end{aligned}$$

$z(0) = a$   
 $r(0) = 0$

$\theta = \frac{\sigma}{a_0} \Rightarrow \frac{d\theta}{d\sigma} = \frac{1}{a_0} = \lambda_s \kappa_s = \frac{a}{a_0} \cdot \frac{1}{a} \quad \checkmark$

Suppose  $f_s = f_\varphi = A \left( \lambda_s^2 + \lambda_\varphi^2 - 2 \right)$   
Symmetry  $\left(\frac{a}{a_0}\right)^2 \quad \left(\frac{a}{a_0}\right)^2$

$\Rightarrow t_s = t_\varphi = 2A \left( \frac{a^2}{a_0^2} - 1 \right)$

$P^* = t_s \kappa_s + t_\varphi \kappa_\varphi = 4A \left( \frac{a^2}{a_0^2} - 1 \right) \cdot \frac{1}{a} \Rightarrow a = \frac{a_0}{2} \left( \beta + \sqrt{\beta^2 + 4} \right)$

$\checkmark \beta = \frac{P^* a_0}{4A}$

Mechanics

$m_s = B (\kappa_s + \kappa_\varphi - \kappa_0)$   
 $\kappa_{s_0} = \frac{1}{a_0} = \kappa_{\varphi_0} \Rightarrow \kappa_0 = \frac{2}{a_0}$   
 $\kappa_s = \kappa_\varphi = \frac{1}{a}$   
 $\Rightarrow m_s = 2B \left( \frac{1}{a} - \frac{1}{a_0} \right)$   
satisfies  $m_s' = 0$