

### Problem sheet 3

1. **Overland flow** Overland flow on a hill slope is described by the equation

$$\frac{\partial h}{\partial t} + ch^m \frac{\partial h}{\partial x} = E,$$

where  $E = P - I$  is the excess rainfall rate, being the difference between precipitation and infiltration rates. The equation is to be solved in  $x > 0$ , and the initial and boundary condition are

$$h = 0 \quad \text{at} \quad t = 0, x > 0 \quad \text{and} \quad x = 0, t > 0.$$

First consider the case of constant  $E > 0$ . Solve the equation and sketch the solution at various times.

Next, consider the case where  $E(t)$  is time dependent, such that  $E \geq 0$  for  $0 \leq t \leq t_*$ , and  $E < 0$  for  $t > t_*$ . Find an implicit expression for the solution in terms of integrals of  $E$  for  $t \leq t_*$ .

For  $t > t_*$ , a drying front moves down the slope (behind which  $h = 0$ ). Determine the position of the front  $x_d(t)$  as a function of time and hence find the complete solution for all  $t > 0$ .

2. **St Venant equations** Derive the St Venant equations from first principles in the form

$$\frac{\partial A}{\partial t} + \frac{\partial}{\partial x}(Au) = 0,$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = gS - \frac{\tau \ell}{\rho A} - g \frac{\partial \bar{h}}{\partial x},$$

indicating the meaning of the various terms.

Manning's law corresponds to taking  $\tau = \rho g n^2 u^2 / R^{1/3}$ , where  $R = A/\ell$  is the hydraulic radius. Assuming a triangular cross-section with transverse bed angle  $\beta$ , find appropriate expressions for  $\tau$  and  $\bar{h}$  in terms of  $u$  and  $A$ .

Non-dimensionalise the resulting equations using a length scale  $L$  and discharge scale  $Q$  to obtain

$$\frac{\partial A}{\partial t} + \frac{\partial}{\partial x}(Au) = 0,$$

$$\varepsilon F^2 \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} \right) = 1 - \frac{u^2}{A^{2/3}} - \varepsilon \frac{\partial}{\partial x}(A^{1/2}),$$

and define the parameters  $\varepsilon$  and  $F$ . Assuming that  $\varepsilon \ll 1$  and  $F \ll 1$ , show that  $A$  satisfies the approximate equation

$$\frac{\partial A}{\partial t} + \frac{4}{3} A^{1/3} \frac{\partial A}{\partial x} = \frac{1}{4} \varepsilon \frac{\partial}{\partial x} \left( A^{5/6} \frac{\partial A}{\partial x} \right).$$

A sluice gate on the river is suddenly opened so that the cross-sectional area there increases from  $A_-$  to  $A_+$ . The hydrograph is measured a distance  $L$  downstream. Sketch the hydrograph for the cases (i)  $\varepsilon = 0$  and (ii)  $0 < \varepsilon \ll 1$  (no detailed calculation is required).

3. **Surface waves** Show that with a suitable choice of non-dimensionalisation, the St Venant equations for a triangular-shaped cross section with Manning's roughness law, can be written in the form

$$\frac{\partial A}{\partial t} + \frac{\partial}{\partial x}(Au) = 0,$$

$$F^2 \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} \right) = 1 - \frac{u^2}{A^{2/3}} - \frac{1}{2A^{1/2}} \frac{\partial A}{\partial x},$$

giving the definition of  $F$ . Write down the uniform steady state with dimensionless discharge 1.

Show that small perturbations to the steady state can propagate up and downstream if  $F < F_1$ , but can only propagate downstream if  $F > F_1$ ; and that they are unstable if  $F > F_2$ . Give the values of  $F_1$  and  $F_2$ .

4. **Anti-dunes** A simple model of bed erosion based on the St Venant equations can be written in dimensionless form as

$$\varepsilon h_t + (hu)_x = 0,$$

$$F^2(\varepsilon u_t + uu_x) = -\eta_x + \delta \left( 1 - \frac{u^2}{h} \right),$$

$$h(\varepsilon c_t + uc_x) = E(u) - c = -s_t,$$

where  $h = \eta - s$ , and  $E(1) = 1$ . Briefly explain the meaning of the terms in this model, and the physical significance of the dimensionless parameters  $\varepsilon$ ,  $\delta$  and  $F$ .

By considering the stability of the steady state  $u = h = c = 1$ , and assuming that  $\varepsilon \ll 1$  while  $\delta$  and  $F$  are  $\mathcal{O}(1)$ , show that instability can occur depending on the sign of  $E'(1)$  and the size of  $F$ .

Find the phase difference between surface and bed profiles in the limit of small and large wavenumbers ( $k \rightarrow 0$  and  $k \rightarrow \infty$ ).

5. **Eddy-viscosity model** Derive the Exner equation relating bed elevation  $s$  and bedload transport  $q$ .

Supposing the bedload is a function of the shear stress  $q = q(\tau)$ , show that the equation can be written in dimensionless form as,

$$\frac{\partial s}{\partial t} + q'(\tau) \frac{\partial \tau}{\partial x} = 0.$$

An eddy-viscosity model for turbulent flow over linearised topography leads to the following approximate expression for the dimensionless shear stress,

$$\tau = \left[ 1 - s + \int_0^\infty K(\xi) \frac{\partial s}{\partial x}(x - \xi, t) \, d\xi \right],$$

where the kernel is  $K(x) = \mu/x^{1/3}$ , and  $\mu > 0$  is constant.

Making use of this expression, examine whether linear perturbations to the steady state  $s = 0$  are unstable. Which direction do the perturbations travel?

[Hint: in your calculation you will need to evaluate the integral  $\int_0^\infty \xi^{-1/3} e^{-ik\xi} \, d\xi$ , for which you can use contour integration to find the value  $e^{-i\pi/3} \Gamma(\frac{2}{3}) k^{-2/3}$ , where  $\Gamma(\nu) = \int_0^\infty t^{\nu-1} e^{-t} \, dt$  is the gamma function.]