

C

Topics in fluids sheet 4 Answers

$$1. \quad p = \frac{\rho R T}{M_a}$$

$$\frac{\partial p}{\partial z} = -\rho g$$

$$\rho c_p \frac{\partial T}{\partial z} - \frac{\partial p}{\partial z} = 0 \Rightarrow \rho c_p \frac{\partial T}{\partial z} = \frac{\partial p}{\partial z} = -\rho g$$

$$\Rightarrow \frac{\partial T}{\partial z} = -\frac{g}{c_p}$$

$$\Rightarrow T = T_0 - \frac{gz}{c_p}, \quad \rho = \bar{\rho} = \rho_0 \rho^* (z)$$

$$\text{where } \rho_0 \rho^* = \frac{\partial p}{\partial z} = -\rho g = -\frac{M_a \rho g}{R T} = \frac{-M_a \rho_0 \rho^* g}{R (T_0 - \frac{gz}{c_p})}$$

$$\text{so } \frac{\rho^*}{\rho^*} = -\frac{M_a g}{R T_0 (1 - \frac{gz}{c_p T_0})}, \quad \rho^*(0) = 1$$

$$\Rightarrow \ln \rho^* = +\frac{M_a g}{R T_0} \cdot \frac{c_p T_0}{g} \ln \left[1 - \frac{gz}{c_p T_0} \right]$$

$$\Rightarrow \rho^* = \left(1 - \frac{gz}{c_p T_0} \right)^{\frac{M_a c_p}{R}}$$

$$\text{Define } H = \frac{R T_0}{M_a g}, \quad \rho^* = \left(1 - \frac{z}{H} \frac{R T_0}{M_a g} \cdot \frac{g}{c_p T_0} \right)^{\frac{M_a c_p}{R}}$$

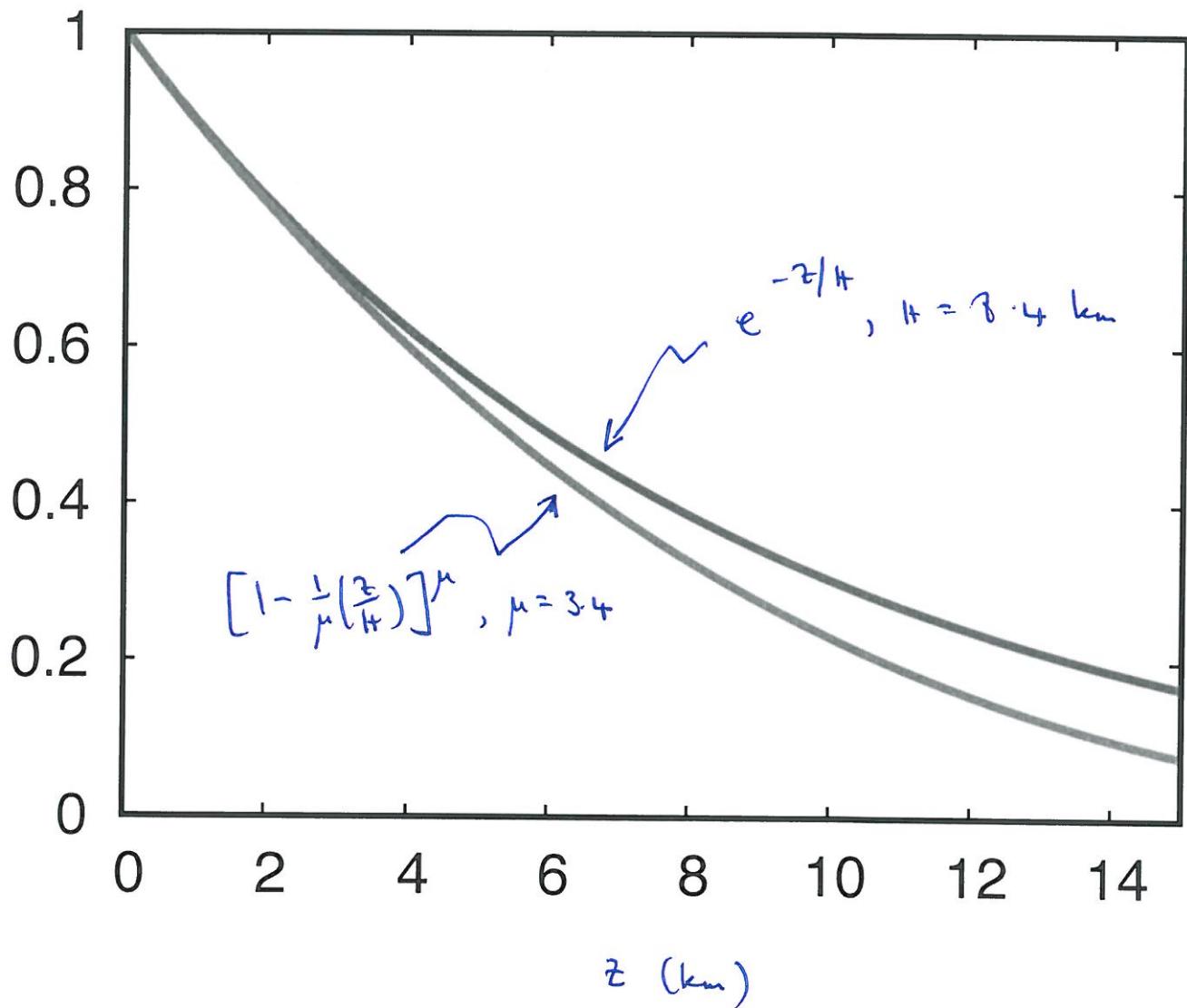
$$= \left[1 - \frac{z}{\mu(H)} \right]^\mu, \quad \mu = \frac{M_a c_p}{R} = 3.4$$

$$\text{So for } z \sim H \text{ & since } \mu \gg 1, \quad \rho^* = \exp \left(-\frac{z}{H} \right)$$

(2)

The approximation is not valid for $z \gtrsim H$

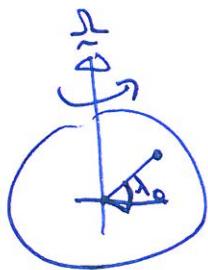
(and is anyway inappropriate above the tropopause).



3

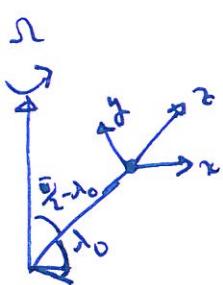
$$\rho_f + \nabla \cdot (\rho \underline{u}) = 0$$

$$\rho \left[\frac{du}{dt} + 2\Omega \times \underline{u} \right] = -\nabla p - \rho g \hat{k}$$



The magnitude of Ω is

$$2\pi d^{-1} = \frac{2\pi}{24 \times 3600} s^{-1} \approx 0.73 \times 10^{-4} s^{-1}$$



$$\text{Note } \underline{\Omega} = (0, \Omega \cos \lambda_0, \Omega \sin \lambda_0)$$

$$\text{so } \underline{\Omega} \times \underline{u} = \begin{pmatrix} i & j & k \\ 0 & \Omega \cos \lambda_0 & \Omega \sin \lambda_0 \\ u & v & w \end{pmatrix} \approx (-\Omega v \sin \lambda_0, \Omega v \sin \lambda_0, -\Omega u \sin \lambda_0)$$

Since $w \ll u, v$

Scaling the variables as prescribed in the question, we get

$$\rho_f + \nabla \cdot (\rho \underline{u}) = 0$$

$$\rho_0 \rho \left[\frac{U^2}{l} \frac{du}{dt} + -2\Omega U \sin \lambda_0 f v \right] = -2\rho_0 \Omega U \sin \lambda_0 P_n$$

$$\text{& thus } \left(\frac{\rho}{\rho_0}, \frac{U}{U_0}, \frac{\lambda}{\lambda_0} \right) \frac{U^2}{l} \frac{du}{dt} - f v = -\frac{1}{\rho} P_n, \quad f = \frac{\sin \lambda}{\sin \lambda_0}$$

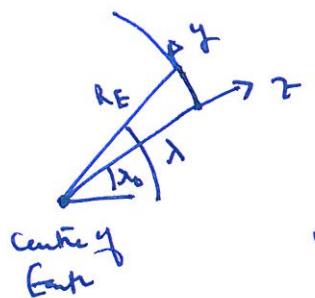
$$\text{i.e. } \underbrace{\varepsilon \frac{du}{dt} - f v}_{=0} = -\frac{1}{\rho} P_n$$

$$\varepsilon = \frac{U}{2\Omega l \sin \lambda_0} \quad \text{Froude number}$$

(4)

Similarly (the scales of the two are the same)

$$\varepsilon \frac{du}{dt} + fu = -\frac{1}{\rho} p_y$$



$$\text{we have } y = R_E \sin(\lambda - \lambda_0)$$

and for $y \ll R_E$, $\lambda \approx \lambda_0$ & $y \approx R_E(\lambda - \lambda_0)$

$$\text{thus } \lambda = \lambda_0 + \frac{y}{R_E}$$

$$\begin{aligned} f &= \frac{\sin(\lambda_0 + \frac{y}{R_E})}{\sin \lambda_0} \approx \frac{\sin \lambda_0 \cos \frac{y}{R_E} + \cos \lambda_0 \sin \frac{y}{R_E}}{\sin \lambda_0} \\ &= \text{retaining } 1 - \frac{y^2}{2R_E^2} \dots + \cot \lambda_0 \frac{y}{R_E} \dots \end{aligned}$$

$$\text{Now dimensionally } f = 1 + \frac{\lambda \cot \lambda_0}{R_E} y$$

$$= 1 + \varepsilon \beta y ,$$

$$\underline{\beta = \frac{\lambda \cot \lambda_0}{\varepsilon R_E}}$$

$$\rho = \frac{\Pi}{\theta}, \quad \Pi = \theta \Pi^2, \quad -\frac{\partial \Pi}{\partial z} = \bar{p}$$

$$\Pi = \bar{p} + \epsilon^2 \rho \quad \theta = \bar{\theta} + \epsilon^2 \Theta$$

$$\rho = \frac{\Pi^{1-\alpha}}{\theta} = \bar{\rho} + O(\epsilon^2), \quad \bar{\rho} = \frac{\bar{p}^{1-\alpha}}{\bar{\theta}}$$

Now $\rho_t + (\rho u)_x + (\rho v)_y + (\rho w)_z = 0$
 (momentum)

$$\text{Thus } \bar{\rho}(u_x + v_y) + (\bar{\rho}w)_z = O(\epsilon^2)$$

But also $\begin{aligned} -\bar{\rho}v &= -\rho_x + O(\epsilon) \\ \bar{\rho}u &= -\rho_y + O(\epsilon) \end{aligned}$ from momentum eqns

$$\text{so } \bar{\rho}(u_x + v_y) = O(\epsilon)$$

$$\Rightarrow w = O(\epsilon) \quad (\text{from mass continuity})$$

Now we take $\rho = \rho_0 \Pi = \rho_0 \bar{\rho} + \epsilon^2 \frac{\rho_0}{\bar{\rho}} \bar{P}$
 but also $\rho = \rho_0 \bar{\rho} + 2\rho_0 \sqrt{l} U \sin \lambda_0 \bar{P}$

and thus $\epsilon^2 \frac{\rho_0}{\bar{\rho}} \bar{P} = 2\rho_0 \sqrt{l} U \sin \lambda_0$

$$\text{i.e. } \frac{\rho_0 g h U^2}{(2 \sqrt{l} \sin \lambda_0)^2} = \rho_0 U (2 \sqrt{l} \sin \lambda_0)$$

$$\text{so } U = \frac{g (2 \sqrt{l} \sin \lambda_0)}{g h}$$

(earlier we had
 $\rho_0 = \rho_0 g h$)

(b) (iii)

$$\lambda_0 = 45^\circ \Rightarrow \sin \lambda_0 = 0.7$$

$$U = g \frac{\left[0.73 \times 10^{-4} \cdot 10^6 \text{ m} \cdot 0.7 \text{ s}^{-1} \right]^3}{9.8 \cdot 8 \cdot 10^3 \text{ m s}^{-2}}$$

$$= g \frac{0.73^3 (0.7 \times 0.73)^3 \cdot 10^6}{9.8 \cdot 8 \cdot 10^3} \text{ m s}^{-1}$$

$$\approx 12 \text{ m s}^{-1}$$

Note that

$$\Sigma = \frac{12}{2 \cdot 0.73 \cdot 10^{-4} \cdot 0.7 \cdot 8 \cdot 10^6} \approx 0.12$$

Now we have

$$-\frac{\partial \Pi}{\partial z} = \rho = \frac{\Pi^{1-\alpha}}{\Theta}, \quad \Pi = \bar{p} + \epsilon^2 p$$

$$\Theta = \bar{\Theta} + \epsilon^2 \Theta$$

$$\therefore -\frac{\partial \bar{p}}{\partial z} - \epsilon^2 \frac{\partial p}{\partial z} = \frac{(\bar{p} + \epsilon^2 p)^{1-\alpha}}{\bar{\Theta} + \epsilon^2 \Theta} = \frac{\bar{p}^{1-\alpha}}{\bar{\Theta}} \left[1 + \epsilon^2 (1-\alpha) \frac{p}{\bar{p}} \right] \left[1 - \epsilon^2 \frac{\Theta}{\bar{\Theta}} \right]$$

$$= \frac{\bar{p}^{1-\alpha}}{\bar{\Theta}} + \epsilon^2 \left\{ \frac{(1-\alpha)p}{\bar{\Theta} \bar{p}^\alpha} - \frac{\bar{p}^{1-\alpha} \Theta}{\bar{\Theta}^2} \right\} \dots$$

thus equating to terms of $O(\epsilon^2)$

$$\frac{\bar{p}^{1-\alpha}}{\bar{\Theta}^2} \Theta = \frac{(1-\alpha)p}{\bar{\Theta} \bar{p}^\alpha} + \frac{\partial p}{\partial z} \quad (\text{as well as } \frac{\partial \bar{p}}{\partial z} = -\frac{\bar{p}^{1-\alpha}}{\bar{\Theta}})$$

$$\therefore \Theta = \bar{\Theta}^2 \left[\frac{(1-\alpha)p}{\bar{\Theta} \bar{p}^\alpha} + \frac{1}{\bar{p}^{1-\alpha}} \frac{\partial p}{\partial z} \right]$$

$$\text{Now note } \frac{\partial}{\partial z} \frac{1}{\bar{p}^{1-\alpha}} = -\frac{(1-\alpha)}{\bar{p}^{2-\alpha}} \frac{\partial \bar{p}}{\partial z} = \frac{(1-\alpha)}{\bar{p}^{2-\alpha}} \frac{\bar{p}^{1-\alpha}}{\bar{\Theta}} = \frac{(1-\alpha)}{\bar{\Theta} \bar{p}^\alpha}$$

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$$\text{Therefore } \Theta = \bar{\theta}^2 \left[\rho \frac{\partial}{\partial z} \frac{1}{\bar{p}^{1-\alpha}} + \frac{1}{\bar{p}^{1-\alpha}} \frac{\partial \rho}{\partial z} \right]$$

$$= \bar{\theta}^2 \frac{\partial}{\partial z} \left[\frac{\rho}{\bar{p}^{1-\alpha}} \right]$$

Define $\rho = \bar{p} \Psi$ and assume $\bar{\theta} \approx 1$

Then (geostrophy) $v \approx \frac{1}{\bar{p}} \rho_n$, $u \approx -\frac{1}{\bar{p}} \rho_y$
use p3

so $u \approx -\Psi_y$, $v \approx \Psi_n$

and $\Theta = \bar{\theta}^2 \frac{\partial}{\partial z} \left[\frac{\bar{p} \Psi}{\bar{p}^{1-\alpha}} \right] = \bar{\theta}^2 \frac{\partial}{\partial z} \left[\frac{\Psi}{\bar{\theta}} \right]$ $(\bar{p} \approx \frac{\bar{p}^{1-\alpha}}{\bar{\theta}})$

$\Rightarrow \Theta \approx \Psi_z$

thus $\frac{\partial u}{\partial z} \approx -\frac{\partial \Theta}{\partial y}$, $\frac{\partial v}{\partial z} \approx \frac{\partial \Theta}{\partial n}$

(8)

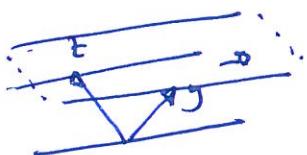
3/ with $\bar{\rho}$ LS constant, $\beta = 1 + \delta = 0$,

$$\left[\frac{\partial}{\partial t} - \Psi_y \frac{\partial}{\partial x} + \Psi_x \frac{\partial}{\partial y} \right] \left[\nabla^2 \Psi + \frac{1}{S} \Psi_{zz} \right] = 0 \quad (\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2})$$

$\nabla \cdot (\partial_t - \Psi_y \partial_x + \Psi_x \partial_y) \Psi_z = 0 \quad \text{at } z=0,1$

$\Psi_z = 0 \quad \text{at } y=0,1$

(flow in an unconfined channel)



$\Psi = -yz$ is a particular solution satisfying the b.c's + eq.

with $\Theta = \Psi_z = -y$

$$\nabla \cdot \frac{\partial u}{\partial z} = -\Theta_y = 1, \frac{\partial v}{\partial z} = \Theta_x = 0 \quad (\text{or just } u = -\Psi_y = -z, v = \Psi_x = 0)$$

this corresponds to ^{unifind} total ~~free~~ shear flow.

Put $\Psi = -yz + \bar{\Psi}$, $\Psi_y = -z + \bar{\Psi}_y$, $\Psi_x = \bar{\Psi}_x$, $\Psi_z = -y + \bar{\Psi}_z$

$$\nabla^2 \Psi + \frac{1}{S} \Psi_{zz} = \nabla^2 \bar{\Psi} + \frac{1}{S} \bar{\Psi}_{zz} \ll 1$$

so linearized QGPVE is

$$\left(\frac{\partial}{\partial t} + z \frac{\partial}{\partial x} \right) \left(\nabla^2 \bar{\Psi} + \frac{1}{S} \bar{\Psi}_{zz} \right)$$

& the linearized b.c's are $\bar{\Psi}_x = 0$ at $y=0,1$

$$-\bar{\Psi}_z + \left(\frac{\partial}{\partial t} + z \frac{\partial}{\partial x} \right) \bar{\Psi}_z = 0 \quad \text{at } z=0,1$$

(from $\frac{\partial}{\partial t} + (-z + \bar{\Psi}_y) \frac{\partial}{\partial x} + \bar{\Psi}_x \frac{\partial}{\partial y} \right] [-y + \bar{\Psi}_z]$)

(9)

there are normal mode solutions

$$\Psi = A(z) e^{ik(z+ct)} \text{ since } \text{ which satisfy they } z=0, 1 \text{ b.c.s}$$

[Note $\operatorname{Re}[-ikc] = \operatorname{Re}[-ik(c_{\text{at}} + i\epsilon)] = c_{\text{at}}$ so instability if $\operatorname{Im} c > 0$
 The wave speed is $-\frac{\operatorname{Im}[-ik(c_{\text{at}} + i\epsilon)]}{k} = c_{\text{R}} = \operatorname{Re} c$]

and then

$$(-ikc + ikt)(-(k^2 + \mu^2)A + \frac{1}{S}A'') = 0$$

$$\text{where } (z-c)(A'' - \mu^2 A) = 0 \quad \mu^2 = (k^2 + \mu^2)S \quad (>0)$$

& the b.c. is

$$-ikA + ik(z-c)A' = 0$$

~~At $z=0$ & $z=1$, A' is not zero~~

where

~~$A=0 \text{ at } z=0, 1$~~

(we exclude the trivial case $k=0$)

~~$-A + (z-c)A' = 0 \text{ on } z=0, 1$~~

If $\epsilon \ll 0 < c \ll 1$ then ~~the b.c.~~

~~$\text{for } z=0, \text{ we have } A'' - \mu^2 A = 0 + A' - c - 0$
 $\Rightarrow A = \dots \text{ right} + \text{left} \text{ values.}$~~

However there are solutions

$$A'' - \mu^2 A = \delta(z-c)$$

which gives gives the Green's function $G(z, c)$ for the o.d.e. + homogeneous b.c.

Since c ^{then} spread, these solutions are not unstable.

(10)

~~Solve for c to obtain c ,~~

The general solution is

$$A = a \cosh \mu z + b \sinh \mu z$$

$$\Rightarrow A' = \mu [a \sinh \mu z + b \cosh \mu z]$$

$$\text{at } z=0, cA' + A = 0$$

$$\Rightarrow \mu cb + a = 0$$

$$\text{at } z=1, \text{ write } c_h = \cosh \mu, s_h = \sinh \mu, (1-c)A' = A$$

$$\text{then } (1-c)\mu [as_h + bs_h] = ac_h + bs_h$$

Since $a = -\mu cb$,

$$\Rightarrow (1-c)\mu [-\mu cs_h + c_h] = -\mu cc_h + bs_h$$

$$\Rightarrow \mu^2 s_h(c^2 - c) + \mu c_h(1-c) + \mu c_h c - s_h = 0$$

$$\Rightarrow c^2 - c = \frac{s_h - \mu c_h}{\mu^2 s_h}$$

$$\text{so } c = \frac{1}{2} \pm \left[\frac{1}{4} + \frac{s_h - \mu c_h}{\mu^2 s_h} \right]^{\frac{1}{2}}.$$

Comparing this with answer, we write

$$c = \frac{1}{2} \pm \frac{1}{\mu} \left[\frac{1}{4}\mu^2 + 1 + \frac{s_h - \mu c_h}{s_h} - 1 \right]^{\frac{1}{2}}$$

$$= \frac{1}{2} \pm \frac{1}{\mu} \left[\frac{1}{4}\mu^2 + 1 - \mu \coth \mu \right]^{\frac{1}{2}}$$

(4)

Now note that

$$\begin{aligned} & \frac{1}{2}(\coth \mu_2 + \tanh \mu_2) \\ &= \frac{1}{2} \left[\frac{\cosh \mu_2}{\sinh \mu_2} + \frac{\sinh \mu_2}{\cosh \mu_2} \right] \\ &= \frac{\cosh^2 \mu_2 + \sinh^2 \mu_2}{2 \sinh \mu_2 \cosh \mu_2} \\ &= \frac{\cosh \mu_2}{\sinh \mu_2} = \coth \mu_2 \end{aligned}$$

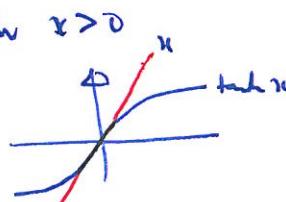
thus $c = \frac{1}{2} \pm \frac{1}{\mu} \left[\frac{1}{4} \mu^2 + 1 - \frac{1}{2} (\coth \mu_2 + \tanh \mu_2) \right]^{\frac{1}{2}}$

$$= \frac{1}{2} \pm \frac{1}{\mu} \left[(\mu - \coth \mu_2)(\mu + \tanh \mu_2) \right]^{\frac{1}{2}}$$

The local flow is unstable if $\overset{\text{Im}}{\star} c > 0$

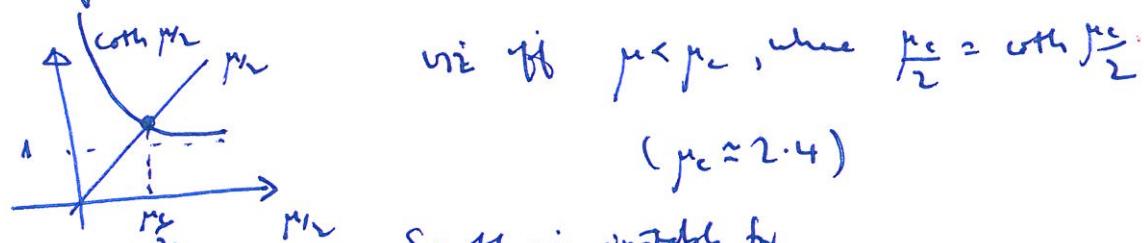
& since there are two conjugate roots, the sufficient condition is that $[] < 0$ in above.

Now μ is real and positive w.l.o.g. Also $\tanh x < x$ for $x > 0$



$\Rightarrow \mu - \tanh \mu_2 > 0$.

Therefore the flow is unstable iff $\mu < \coth \mu_2$



So flow is unstable for
 $\mu = (k^2 + n^2 \pi^2)^{\frac{1}{2}} S^{\frac{1}{n}} < \mu_c$
 $\text{or } S < \frac{\mu_c}{(k^2 + n^2 \pi^2)^{\frac{1}{2}}} \text{. Excluding }_{(\text{trivial})} n=0 \Rightarrow S < S_c = \frac{\mu_c}{\pi^2} \text{ for } n=1$
 $\text{and } k \rightarrow 0$
 (long wavelength)

4/

$$(\alpha \rho_s)_t + (\alpha \rho_s v)_z = \Gamma$$

$$[\rho_e(1-\alpha)]_t + [\rho_e(1-\alpha)v]_z = -\Gamma$$

$$\rho_s(v_t + vv_z) = -v_z - M$$

$$\rho_e(v_t + \alpha D_e v v_z) = -v_z + M$$

If $\underline{\psi}$ is in the form $A\underline{\psi}_t + B\underline{\psi}_z = \underline{c}$

but if $\underline{\psi}$ was scalar, the characteristics would be $\dot{z} = \frac{B}{A} = A^{-1}B$

↳ this generalizes to systems:

$$\text{Suppose } A \text{ invertible } A^{-1}B \underline{w} = \lambda \underline{w}$$

$$\text{so } \det(A^{-1}B - \lambda I) = 0$$

↳ suppose $A^{-1}B$ is diagonalizable,

$$A^{-1}B = PDP^{-1}, D = \text{diag}(\lambda_i)$$

$$\text{Put } \underline{\psi} = P \underline{u}$$

$$\text{then } A(P\underline{u}_t + P_t \underline{u}) + B P \underline{u}_z = \underline{c}$$

$$\Rightarrow \underline{u}_t + P^{-1}A^{-1}BP \underline{u}_z = P^{-1}A^{-1}\underline{c} - P^{-1}A^{-1}AP_t \underline{u}$$

$$\text{i.e. } \underline{u}_t + D \underline{u}_z = P^{-1}A^{-1}\underline{c} - P^{-1}P_t \underline{u}$$

↳ the characteristics are $\dot{z} = \lambda_i$

$$\text{and which } \dot{u}_i = [P^{-1}A^{-1}\underline{c} - P^{-1}P_t \underline{u}]_i$$

More generally, $\det(\lambda A - B) = 0$.

(13)

(i) ρ_g, ρ_e const., $\frac{\rho_g}{\rho_e} = \gamma \ll 1$

$$\text{Thus } \dot{\alpha}_T + v \alpha_Z + \alpha v_Z = \frac{r}{\rho_g}$$

$$-\dot{\alpha}_T - u \alpha_Z + (1-\alpha) v_Z = -\frac{r}{\rho_e}$$

$$\rho_g v_T + \rho_g v_Z v_Z + p_Z = -M$$

$$\rho_e \dot{\alpha}_T + D_e \rho_e u v_Z + p_Z = M$$

with $\underline{\Psi} = \begin{pmatrix} \alpha \\ u \\ v \\ p \end{pmatrix}$

$$\underbrace{\begin{pmatrix} 1 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & \rho_g & 0 \\ 0 & \rho_e & 0 & 0 \end{pmatrix}}_A \underline{\Psi}_T + \underbrace{\begin{pmatrix} v & 0 & \alpha & 0 \\ -u & (1-\alpha) & 0 & 0 \\ 0 & 0 & \rho_g v & 1 \\ 0 & D_e \rho_e u & 0 & 1 \end{pmatrix}}_B \underline{\Psi}_{-Z} = \begin{pmatrix} r/\rho_g \\ -r/\rho_e \\ -M \\ M \end{pmatrix}$$

$$\det(\Delta A - B)$$

$$= \begin{vmatrix} \lambda - v & 0 & -\alpha & 0 \\ -(\lambda - u) & -(1-\alpha) & 0 & 0 \\ 0 & 0 & \rho_g(\lambda - v) & -1 \\ 0 & \rho_e(\lambda - D_e u) & 0 & -1 \end{vmatrix} = 0$$

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This gives

$$(\lambda - v) \left[- (1-\alpha) \rho_g (\lambda - v) \cdot -1 \right] \\ - \alpha \left[- (\lambda - u) \rho_e (\lambda - D_\ell u) \right] = 0$$

$$u \approx \rho_g (1-\alpha) (\lambda - v)^2 + \rho_e \alpha (\lambda - u) (\lambda - D_\ell u) = 0$$

with $\delta = \frac{\rho_g}{\rho_e} \ll 1$

$$\delta (1-\alpha) (\lambda - v)^2 + \alpha (\lambda - u) (\lambda - D_\ell u) = 0$$

$$(\lambda - u) (\lambda - D_\ell u) = - \frac{\delta (1-\alpha)}{\alpha} (\lambda - v)^2$$

Approximately $\lambda = u$ & $\lambda = D_\ell u$ are the (real) roots

A "connection" to "

$$\lambda - u = - \frac{\delta (1-\alpha)}{\alpha} \frac{(\lambda - v)^2}{\lambda - D_\ell u}$$

$$\Rightarrow \lambda \approx u + \frac{\delta (1-\alpha)}{\alpha} \frac{(u-v)^2}{(D_\ell - 1) u} \quad \text{etc.}$$

This only goes away if $D_\ell \sim \delta$.

(15)

$$\text{(ii) Now suppose } \frac{dp_g}{dp} = \frac{1}{c_g^2}, \quad , \quad \frac{dp_e}{dp} = \frac{1}{c_e^2}$$

(c^2 are sound speeds)

then equations are

$$p_g \alpha_f + \frac{\alpha}{c_g^2} p_f + p_g v \alpha_z + r_g \alpha v_z + \frac{\alpha v}{c_g^2} p_z = \Gamma$$

$$-p_e \alpha_f + \frac{(1-\alpha)}{c_e^2} p_f - r_e u \alpha_z + r_e (1-\alpha) u_z + \frac{(1-\alpha) u}{c_e^2} p_z = -\Gamma$$

or (define $\Pi_h = p_h c_h^{-2}$)

$$\alpha_f + \frac{\alpha}{\Pi_g} p_f + v \alpha_z + \alpha v_z + \frac{\alpha v}{\Pi_g} p_z = \frac{\Gamma}{p_g}$$

$$-\alpha_f + \frac{1-\alpha}{\Pi_e} p_f - u \alpha_z + (1-\alpha) u_z + \frac{(1-\alpha) u}{\Pi_e} p_z = -\frac{\Gamma}{p_e}$$

$$\text{And } p_g r_f + p_g v v_z + p_z = -M$$

$$p_e r_f + p_e D_e u u_z + p_z = M$$

The red terms are the additives, thus

$$A = \begin{pmatrix} 1 & 0 & 0 & \frac{\alpha}{\Pi_g} \\ -1 & 0 & 0 & \frac{1-\alpha}{\Pi_e} \\ 0 & 0 & r_g & 0 \\ 0 & p_e & 0 & 0 \end{pmatrix}, \quad B = \begin{pmatrix} v & 0 & \alpha & \frac{\alpha v}{\Pi_g} \\ -u & (1-\alpha) & 0 & \frac{(1-\alpha) u}{\Pi_e} \\ 0 & 0 & p_g v & 1 \\ 0 & D_e p_e u & 0 & 1 \end{pmatrix}$$

(16)

and thus

$$\det(\lambda A - B)$$

$$= \begin{vmatrix} \lambda - v & 0 & -\alpha & \frac{\alpha}{\pi_g} (\lambda - v) \\ -(\lambda - u) & -(1-\alpha) & 0 & \frac{(1-\alpha)}{\pi_e} (\lambda - u) \\ 0 & 0 & p_g(\lambda - v) & -1 \\ 0 & p_e(\lambda - D_e u) & 0 & -1 \end{vmatrix} = 0$$

$$\text{If } (\lambda - v) \left[(1-\alpha) p_g(\lambda - v) - \frac{(1-\alpha)}{\pi_e} (\lambda - u) r_g r_e (\lambda - v)(\lambda - D_e u) \right]$$

$$- \alpha \left[-(\lambda - u) r_e (\lambda - D_e u) \right]$$

$$- \frac{\alpha}{\pi_g} (\lambda - v) \left[-(\lambda - u) \cdot -r_g r_e (\lambda - v)(\lambda - D_e u) \right] = 0$$

$$\text{i.e. } p_g(1-\alpha)(\lambda - v)^2 + p_e \alpha (\lambda - u)(\lambda - D_e u)$$

$$- p_g p_e \left[\frac{1-\alpha}{\pi_e} + \frac{\alpha}{\pi_g} \right] (\lambda - v)^2 (\lambda - u)(\lambda - D_e u) = 0$$

(17)

Previously, we had $\lambda \approx u$

Let's suppose $v \approx u$ and $c_g \approx c_d$

If $\lambda \approx u$ then the new term is $\sim \left[\frac{p_g}{c_d^2}, \frac{p_d}{c_g^2} \right] u^4 \ll p_d u^2$

So two approximate roots are $\lambda = u, D_d u$ as before.

As the new term is singular, the other two roots are large

$$\text{Approximately } p_d \propto (\lambda - u)(\lambda - D_d u) - \frac{\alpha p_d}{c_g^2} (\lambda - v)^2 (\lambda - u)(\lambda - D_d u) \approx 0$$

so the other two roots are

$$\lambda = v \pm c_g \quad \text{for sound waves}$$

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5)

Energy equation:

$$\Gamma_L + \frac{\rho_g}{\rho_s} (\dot{m}_s (T_f + v T_2) + (1-\alpha) \rho_e c_{pe} (T_f + u T_2)) - \{(\alpha \dot{m}_g)_f + (\alpha \dot{m}_g v)_2\} - [\{(1-\alpha) \rho_e\}_f + \{(1-\alpha) \rho_e u\}_2] = Q$$

$$\text{where } \Gamma = (\alpha \dot{m}_g)_f + (\alpha \dot{m}_g v)_2 = -[\{(1-\alpha) \rho_e\}_f + \{(1-\alpha) \rho_e u\}_2]$$

Energy is thus

$$\Gamma_L + \alpha \rho_g (\dot{m}_s f + v \dot{m}_g z) + (1-\alpha) \rho_e (\dot{m}_e f + u \dot{m}_e z) - \{(\alpha \dot{m}_g)_f + (\alpha \dot{m}_g v)_2\} - [\{(1-\alpha) \rho_e\}_f + \{(1-\alpha) \rho_e u\}_2] = Q$$

Now consider ~~$(\dot{m}_g f + \dot{m}_g v)_2$~~ viz $\Gamma (\dot{m}_g - \dot{m}_e) + \dots$

$$\begin{aligned} \text{viz } & \dot{m}_g [(\alpha \dot{m}_g)_f + (\alpha \dot{m}_g v)_2] + \alpha \dot{m}_g (\dot{m}_s f + v \dot{m}_g z) \\ & + \dot{m}_e [\{(1-\alpha) \rho_e\}_f + \{(1-\alpha) \rho_e u\}_2] + (1-\alpha) \rho_e (\dot{m}_e f + u \dot{m}_e z) \\ & - \dots = Q \end{aligned}$$

$$\begin{aligned} \text{viz } & (\alpha \dot{m}_g \dot{m}_g)_f + (\alpha \dot{m}_g v \dot{m}_g)_2 - \{(\alpha \dot{m}_g)_f - (\alpha \dot{m}_g v)_2 \\ & + \{(1-\alpha) \rho_e \dot{m}_e\}_f + \{(1-\alpha) \rho_e \dot{m}_e u\}_2 - \{(1-\alpha) \rho_e\}_f - \{(1-\alpha) \rho_e u\}_2\} = Q \end{aligned}$$

$$\begin{aligned} \text{viz } & \{ \alpha (\rho_g \dot{m}_g - \dot{m}_g) \}_f + \{ \alpha v (\rho_g \dot{m}_g - \dot{m}_g) \}_2 \\ & + \{(1-\alpha) (\rho_e \dot{m}_e - \dot{m}_e)\}_f + \{(1-\alpha) (\rho_e \dot{m}_e - \dot{m}_e) u\}_2 = Q \end{aligned}$$

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$$u \dot{e} = (\alpha \rho_g e_g)_F + (\alpha \rho_g e_g v)_Z$$

$$+ \{(1-\alpha) \rho_e e_e\}_F + \{(1-\alpha) \rho_e e_e u\}_Z = Q$$

D

$$\rho = e_e(1-\alpha) + \rho_g \alpha$$

$$F = (1-\alpha) p_e + \alpha p_g$$

$$\rho e = \alpha \rho_g e_g + (1-\alpha) \rho_e e_e$$

$$h = e + \frac{p}{\rho}$$

$$\Rightarrow \rho h = \rho e + p = \alpha \rho_g e_g + (1-\alpha) \rho_e e_e$$

$$+ \alpha p_g + (1-\alpha) p_e$$

$$= \alpha \rho_g h_g + (1-\alpha) \rho_e h_e$$

D

Now suppose $u=v$ (homogeneous flow)

The energy equation is then

$$\{\alpha \rho_g e_g + (1-\alpha) \rho_e e_e\}_F + [\{\alpha \rho_g e_g + (1-\alpha) \rho_e e_e\} u]_Z = Q$$

$$\text{i.e. } (\rho e)_F + (\rho eu)_Z = Q$$

$$\leftarrow \rho_F + (\rho u)_Z = 0 \quad \text{so} \quad \underline{\rho \frac{de}{dt}} = Q, \quad \frac{d}{dt} = \frac{\partial}{\partial t} + u \frac{\partial}{\partial Z}$$

We have $h = e + \frac{p}{\rho}$. When $\alpha=0$, $\rho = \rho_e$, $e = e_e$, $p = p_e$

$$\Rightarrow h = h_e$$

$$\text{and if } \alpha=1 \quad h = h_g$$

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$$\text{so as } \alpha : 0 \rightarrow 1 \quad \Delta h \approx \bar{h}_g - \bar{h}_e = L$$

$$\text{and } \Delta h = \Delta e + \frac{\Delta f}{P}$$

$$\Delta(f) < \frac{\Delta p}{P_g}$$

$$\text{so if } \Delta p \ll P_g L \text{ then } \Delta(f) \ll \Delta h$$

$$\Rightarrow \underline{h} \approx e$$

$$\text{In this case } P \frac{dh}{dt} \approx Q$$

$$\text{Now } P = P_e - \Delta p \alpha \quad \Delta p = P_e - P_g$$

$$\Rightarrow \alpha = \frac{P_e - P}{\Delta p}$$

$$\begin{aligned} h_e &= \alpha P_g L + (1-\alpha) P_e L \\ &= P_e L + (P_g L - P_e L) \frac{(P_e - P)}{\Delta p} \\ &= \frac{P_e L (P_e - P_g) + (P_g L - P_e L) P_e}{\Delta p} - (P_g L - P_e L) P \end{aligned}$$

$$\text{thus } h = \frac{P_e P_g L}{\Delta p P} - \frac{(P_g L - P_e L)}{\Delta p} \cancel{P}$$

$$\text{thus } P \frac{dh}{dt} = \frac{P_e P_g L}{\Delta p} \cdot P \cdot -\frac{1}{P^2} \frac{dp}{dt} = \frac{P_e P_g L}{\Delta p} u_2 = Q \quad (\text{note } \frac{dp}{dt} = -P u_2)$$

$$\Rightarrow u_2 = \frac{(P_e - P_g) Q}{P_e P_g L}$$

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$$\rho_f + u\rho_2 = -u_2 \rho$$

$$\rho(u_f + uu_2) = -p_2 - \rho g - \frac{4f\rho_e u^2}{d}$$

$$\rho(u_f + uu_2) = Q$$

$$h \approx h^* + \frac{\rho_g L}{\rho} \quad (\text{if } \alpha > 0)$$

$$z=0 \quad h=h_0, u=U(t)$$

$$z=r \quad h=h_{sat}$$

$$\text{For } z < r, \quad p = p_e \quad , \quad h_f + uh_2 = \frac{Q}{\rho_e} \quad , \quad u = U(t) \quad (\text{as } u_2 = 0)$$

characteristics $\begin{aligned} \dot{z} &= U \\ \dot{t} &= \frac{Q}{\rho_e} \end{aligned}, \quad z=0, t=\gamma, h=h_0$

$$\Rightarrow h = \frac{Q}{\rho_e}(t-\gamma) + h_0, \quad z = \int_{\gamma}^t U(s) ds$$

$$\text{at } z=r(t), \quad h=h_{sat} \Rightarrow \gamma = t - \frac{\rho_e(h_{sat}-h_0)}{Q} = t - \tau, \quad \tau = \frac{\rho_e(h_{sat}-h_0)}{Q}$$

$$\text{thus } r = \int_{t-\tau}^t U(s) ds$$

In the single-phase region the pressure drop is

$$\begin{aligned} \Delta p_{sp} &= \int_0^r -p_2 dz = \int_0^r [\rho_e U + \rho_e g + \frac{4f\rho_e U^2}{d}] dz \\ &= [\rho_e U + \rho_e g + \frac{4f\rho_e U^2}{d}] r \end{aligned}$$

Non-dimensionalise via

$$\rho \sim \rho_1, z, r \sim l, t \sim \tau, u, V \sim u_0 = \frac{l}{\tau}$$

(non-d)

$$\Rightarrow \Delta p_{sp} = [\rho_1 u_0^2 \dot{V} + \rho_1 g l + \frac{4 \pi \rho_1 u_0^2}{d} U^2] r$$

$$= \underbrace{[\Delta p_i \dot{V} + \Delta p_g + \Delta p_f U^2]}_{\text{non-d}} r, \text{ where } r = \int_{t-1}^t V(s) ds$$

$$\Delta p_i = \rho_1 u_0^2$$

$$\Delta p_g = \rho_1 g l$$

$$\Delta p_f = \frac{4 \pi \rho_1 u_0^2}{d}$$

(all non-d)

For $r > r_L$

$$p_t + u p_z = -u_z p$$

$$\text{Also (dimensional: } p \cdot \rho_s L \cdot -\frac{1}{\rho^2} \frac{dp}{dt} = Q)$$

$$u_z \rho_s L u_z = Q \quad \left(\frac{dp}{dt} = -u_z p \right)$$

$$\text{So non-d} \quad u_z = \frac{Q}{\rho_s L} \frac{l}{u_0} = \frac{Q \tau}{\rho_s L} = \frac{\rho_t \Delta h}{\rho_s L}, \quad \Delta h = h_{sat} - h_0$$

$$\text{Define } \varepsilon = \frac{\rho_s L}{\rho_t \Delta h} \quad \text{then } u_z = \frac{1}{\varepsilon} \text{ (so, } u = V \text{ at } z = r)$$

$$\Rightarrow u = V + \frac{z - r}{\varepsilon}$$

The characteristics for φ are thus $(\text{var}-1)$

$$\dot{z} = u = U + \frac{z-r}{\varepsilon}$$

$$\dot{p} = -\frac{1}{\varepsilon} p$$

$$\Delta \quad t=\eta, \quad z=r(\eta), \quad p=1$$

$$\text{giving } p = \exp[-(t-\eta)/\varepsilon] \quad \Rightarrow \quad \eta = t - \varepsilon \ln \frac{1}{p}$$

$$\dot{z} = U + \frac{z-r}{\varepsilon}$$

$$z - \frac{r}{\varepsilon} = U - \frac{r}{\varepsilon}$$

$$(z e^{-U\varepsilon}) = (U - \frac{r}{\varepsilon}) e^{-U\varepsilon}$$

$$z e^{-U\varepsilon} = r(\eta) e^{-\eta/\varepsilon} + \int_{\eta}^t \left\{ U(s) - \frac{r(s)}{\varepsilon} \right\} e^{-s/\varepsilon} ds$$

$$\text{w.t. } z = r(\eta) e^{\frac{t-\eta}{\varepsilon}} + \int_{\eta}^t \left\{ U(s) - \frac{r(s)}{\varepsilon} \right\} e^{\frac{t-s}{\varepsilon}} ds$$

letting $s=t-\varepsilon\xi$, $\eta=t-\varepsilon \ln \frac{1}{p}$, note when $s=\eta$, $\xi=\ln \frac{1}{p}$

$$z = r(t - \varepsilon \ln \frac{1}{p}) \frac{1}{\varepsilon} + \int_0^{\ln \frac{1}{p}} \left\{ \varepsilon U(t - \varepsilon \xi) - r(t - \varepsilon \xi) \right\} e^{\xi} d\xi$$

$$\begin{aligned} & \text{Integrating by parts, } \int_0^{\ln \frac{1}{p}} r(t - \varepsilon \xi) e^{\xi} d\xi \\ &= \left[e^{\xi} r(t - \varepsilon \xi) \right]_0^{\ln \frac{1}{p}} + \varepsilon \int_0^{\ln \frac{1}{p}} e^{\xi} r'(t - \varepsilon \xi) d\xi \\ &= r(t - \varepsilon \ln \frac{1}{p}) \frac{1}{\varepsilon} - r(t) + \varepsilon \int_0^{\ln \frac{1}{p}} e^{\xi} [U(t - \varepsilon \xi) - U_i(t - \varepsilon \xi)] d\xi \end{aligned}$$

$$\{ U_i(t) = U(t-i) \}$$

thus

$$\begin{aligned} z &= r(t - \varepsilon \ln \frac{1}{\rho}) \cdot \frac{1}{\rho} + \int_0^{\ln \frac{1}{\rho}} \varepsilon U(t - \varepsilon \xi) e^\xi d\xi \\ &\quad - \left[r(t - \varepsilon \ln \frac{1}{\rho}) \cdot \frac{1}{\rho} - r(t) + \varepsilon \int_0^{\ln \frac{1}{\rho}} e^\xi [U(t - \varepsilon \xi) - U_1(t - \varepsilon \xi)] d\xi \right] \\ &= r(t) + \varepsilon \int_0^{\ln \frac{1}{\rho}} U_1(t - \varepsilon \xi) e^\xi d\xi \end{aligned}$$

In dimensionless terms, the two-phase pressure drop is

$$\Delta p_{tp} = \int_r^1 \left[(\rho u)_f + (\rho u^2)_z + p_g + \frac{4 f \rho}{d} u^2 \right] dz$$

The RHS in dimensionless terms is (p_{tp}) is

$$\Delta p_i \underbrace{\int_r^1 \left[(\rho u)_f + (\rho u^2)_z \right] dz}_{\Phi_i} + \Delta p_g \underbrace{\int_r^1 \rho dz}_{\Phi_g} + \Delta p_f \underbrace{\int_r^1 \rho u^2 dz}_{\Phi_f}$$

Steady state

$U = V, r = V$. we need $V < 1$ so there is a two-phase region!

We have in the two-phase region $u = V + \frac{z-V}{\varepsilon}$, $\rho u = V$

Then $\Delta p = \Delta p_{np} + \Delta p_{tp}$

$$= (\Delta p_g + \Delta p_f V^2) V$$

$$+ \Delta p_i \left[\rho u \right]_r^1 + \Delta p_g \int_r^1 \frac{V}{u} dz + \Delta p_f \int_r^1 u dz$$

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$$\text{viz } \Delta p = (\Delta p_s + \Delta p_f v^2) v$$

$$+ \Delta p_i \frac{(1-v)}{\varepsilon} + \Delta p_g v \ln \left[\frac{v + \frac{(1-v)}{\varepsilon}}{v} \right] + \Delta p_f \left[v z + \frac{(z-v)^2}{2\varepsilon} \right] v$$

viz

$$\Delta p = \Delta p_i \frac{(1-v)}{\varepsilon} + \Delta p_g v \left[1 + \varepsilon \ln \left\{ 1 + \frac{(1-v)}{\varepsilon v} \right\} \right]$$

$$+ \Delta p_f \left[v^3 + v(1-v) + \frac{(1-v)^2}{2\varepsilon} \right]$$

If v is sufficiently close to 1

$$\Delta p \sim \Delta p_g v + \Delta p_f v^3 \quad \uparrow \text{ with } v$$

small ε

$$\Delta p \approx \frac{1}{\varepsilon} \left[\Delta p_i (1-v) + \frac{1}{2} \Delta p_f (1-v)^2 \right] \quad \downarrow \text{ with } v (< 1)$$

[This is the Lednev's instability, where $\frac{d\Delta p}{dv} < 0$.]

Next, $\Delta p_i = \Delta p_g = 0$, thus

$$\frac{\Delta p}{\Delta p_f} = \Pi_{\text{single phase}} = U^2 r + \int_r^l \rho u^2 dz$$

two phase

Linear Stability

with

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$$U = V + v, \quad r = r_0 + r_1, \quad u = u_0 + u_1, \quad p = p_0 + p_1$$

$$\text{we have } r_0 = V, \quad u_0 = V + \frac{z-V}{\varepsilon}, \quad p_0 = \frac{V}{u_0} \cdot = \frac{V}{V + \frac{z-V}{\varepsilon}}$$

$$r = \int_{t-1}^t U(s) ds$$

$$\underline{r_0 \quad r_1 = \int_{t-1}^t v ds}$$

$$u = U + \frac{z-r}{\varepsilon} \Rightarrow \underline{u_1 = v - \frac{r_1}{\varepsilon}}$$

$$\text{Note also } z = r(t) + \varepsilon \int_0^{t-\xi} U_1(t-\xi) e^\xi d\xi$$

$$= r_0 + r_1 + \varepsilon \int_0^{-\ln p_0 - \frac{r_1}{p_0}} \{V + v_1(t-\xi)\} e^\xi d\xi$$

$$\begin{aligned} \ln \frac{1}{p} &= -\ln p \\ &= -\ln(p_0 + p_1) \\ &= -\ln p_0 - \frac{p_1}{p_0} \dots \end{aligned}$$

linearizing

$$0 = r_1 + \varepsilon \int_0^{\ln \frac{1}{p_0}} v_1(t-\xi) e^\xi d\xi$$

$$-\frac{\varepsilon p_1}{p_0} \frac{V}{p_0}$$

$$\Rightarrow p_1 \approx \frac{p_0}{V} \left[\frac{V}{\varepsilon} + \int_0^{\ln \frac{1}{p_0}} v_1(t-\xi) e^\xi d\xi \right]$$

$$\approx V^2 r + \int_r^1 c u^2 dz$$

Linearizing the condition $\frac{\Delta p}{\Delta p_f} = \text{constant}$, we have

$$0 = V^2 r_1 + 2V^2 v_1 - \left. r_1 p_0 u_0^2 \right|_{r_0} + \int_{r_0}^1 p_1 u_0^2 dz + \int_{r_0}^1 2p_0 u_0 u_1 dz$$

single phase

$$= V^2 r_1 + 2V^2 v_1 - V^2 r_1 + \int_{r_0}^1 (p_1 u_0^2 + 2u_1) dz$$

$$\therefore 2V^2 v_1 + \int_{r_0}^1 (p_1 u_0^2 + 2u_1) dz = 0$$

s.p.

Since $p_0 u_0 = V$,

$$p_0 u_0^2 = V \left[\frac{U}{\Sigma} + \int_0^{\ln \frac{r}{r_0}} v_1(t-\xi) e^\xi d\xi \right]$$

so $\begin{bmatrix} +V_{r_1} & -V_{r_1} \end{bmatrix}$

$$0 = 2V^2 r + \int_{r_0}^1 V \left[2u_1 + \frac{U}{\Sigma} + \int_0^{\ln \frac{r}{r_0}} v_1(t-\xi) e^\xi d\xi \right] dz$$

S.P.

Now we put $v = e^{\sigma t}$

$$\text{then } r_1 = \frac{1}{\sigma} (1 - e^{-\sigma}) e^{\sigma t}$$

$$u_1 = \left[1 - \frac{1}{\sigma} (1 - e^{-\sigma}) \right] e^{\sigma t}$$

we have

$$\begin{aligned} \int_0^{\ln \frac{r}{r_0}} v_1(t-\xi) e^\xi d\xi &= \int_0^{\ln \frac{r}{r_0}} e^{\sigma(t-1-\xi)} e^\xi d\xi \\ &= e^{\sigma t} \int_0^{\ln \frac{r}{r_0}} e^{(1-\xi)\sigma} d\xi \times e^{-\sigma} \\ &= e^{\sigma t} \left[\frac{e^{-\sigma}}{1-\xi\sigma} \left\{ \frac{1}{\sigma} - 1 \right\} \right] \\ &= \frac{e^{\sigma t}}{1-\xi\sigma} \left[\left(1 + \frac{2-V}{\xi V} \right)^{1-\xi\sigma} - 1 \right], \end{aligned}$$

so $2V^2 + \underbrace{v(1-v) \left[2 \left\{ 1 - \frac{1}{\xi\sigma} (1 - e^{-\sigma}) \right\} + \frac{1}{\xi\sigma} (1 - e^{-\sigma}) \right]}_{2 - \frac{1}{\xi\sigma} (1 - e^{-\sigma})}$

S.P. $+ \frac{V e^{-\sigma}}{1-\xi\sigma} \int_V^1 \left\{ \left(1 + \frac{2-V}{\xi V} \right)^{1-\xi\sigma} - 1 \right\} dz = 0$

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viz

$$2V^2 \left[+ V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) - V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) \right]$$

single phase oszcr

$$+ V(1-V) \left[2 - \frac{1}{\sigma} (1 - e^{-\sigma}) \right]$$

$$+ \frac{Ve^{-\sigma}}{(1-\sigma)} \left[\frac{\epsilon V}{2-\sigma} \left\{ \left(1 + \frac{1-V}{\epsilon V} \right)^{2-\sigma} - 1 \right\} - (1-V) \right] = 0$$

(a) only include the single-phase pressure drop:

$$\Rightarrow 2V^2 + V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) = 0$$

$$\text{Then } \frac{1}{\sigma} (1 - e^{-\sigma}) + 2 = 0$$

$$\Rightarrow \sigma = -\frac{1}{2} (1 - e^{-\sigma})$$

Suppose $\operatorname{Re}\sigma > 0$: then $|e^{-\sigma}| < 1$, so $\operatorname{Re}(1 - e^{-\sigma}) > 0$
 so $\operatorname{Re}\sigma = -\frac{1}{2} \operatorname{Re}(1 - e^{-\sigma}) < 0$. \times $\Rightarrow \operatorname{Re}\sigma < 0$

(note $\sigma = 0$ is always a root: since $\frac{\Delta p}{\Delta p_0} = V^2(t) \int_{t-1}^t V(s) ds$)

this is associated with time translation invariance.)

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(b) only two-phase permedrop:

 $\sim \frac{1}{\varepsilon}$

$$\Rightarrow -V^2 \frac{1}{\sigma} (1-e^{-\sigma}) + 2V(1-V) - V(1-V) \frac{1}{\varepsilon^\sigma} (1-e^{-\sigma})$$

$$+ \frac{Ve^{-\sigma}}{1-\varepsilon\sigma} \left[\frac{\varepsilon V}{2-\varepsilon\sigma} \left\{ \left(1 + \frac{1-V}{\varepsilon V}\right)^{2-\varepsilon\sigma} - 1 \right\} - (1-V) \right] = 0$$

$\sim \frac{1}{\varepsilon}$

 $\varepsilon \ll 1$,

$$\text{approx } -V \frac{(1-V)}{\varepsilon} \frac{1}{\sigma} (1-e^{-\sigma}) + Ve^{-\sigma} \frac{\varepsilon V}{2} \left(\frac{1-V}{\varepsilon V} \right)^2 = 0$$

$$\Rightarrow -V(1-V) \frac{2V^2}{\sqrt{2}} \frac{(e^\sigma - 1)}{(1-V)^2} + \sigma = 0$$

$$\Rightarrow \sigma = \gamma(e^\sigma - 1), \quad \gamma = \frac{2V}{1-V} > 0$$

As $\sigma \rightarrow \infty$ (LHS) we must have $e^\sigma \rightarrow \infty \Rightarrow \operatorname{Re} \sigma > 0 \nrightarrow \infty$

\Rightarrow ill-posedness

(c) use both permedrops & the small ε approx

$$\Rightarrow 2V^2 - \frac{V(1-V)}{\varepsilon} \frac{1}{\sigma} (1-e^{-\sigma}) + \frac{\varepsilon V^2 e^{-\sigma} (1-V)}{2\varepsilon V^2} \approx 0$$

$$\Rightarrow \frac{4\varepsilon V^2}{(1-V)^2} - \gamma \frac{1}{\sigma} (1-e^{-\sigma}) + e^{-\sigma} = 0$$

$$\text{Define } \delta = \frac{4\varepsilon V^2}{(1-V)^2}, \quad \Rightarrow \delta\sigma - \gamma + \gamma e^{-\sigma} + \sigma e^{-\sigma} = 0$$

$$\Rightarrow \sigma = \frac{\gamma (1-e^{-\sigma})}{\delta + e^{-\sigma}}$$

(30)

Now as $\sigma \rightarrow \infty$ (LHS) we must have

$$e^{-\sigma} \rightarrow -\delta$$

$$n e^\sigma \rightarrow -\frac{1}{\delta}$$

$$\sigma \rightarrow \ln \frac{1}{\delta} + (2n+1)i\pi$$

is ill-posed for $\delta < 1$ (as then $\operatorname{Re}\sigma > 0$ as $n \rightarrow \infty$)

(d) If we also include the inertial term in the single phase regime

$\Delta p_i / \dot{V}$, then (c) is modified to

$$\frac{\Delta p_i}{\Delta p_f} \sigma + 2V^2 - \frac{v(1-v)}{\varepsilon} \frac{1}{\sigma} (1-e^{-\sigma}) + \frac{(1-v)^2}{2\varepsilon} e^{-\sigma} = 0$$

$$\Rightarrow v\sigma + \delta - \gamma \frac{1}{\sigma} (1-e^{-\sigma}) + e^{-\sigma} = 0, \quad v = \frac{2\varepsilon \Delta p_i}{(1-v)^2 \Delta p_f}$$

$$\Rightarrow v\sigma^2 + \sigma(\delta + e^{-\sigma}) - \gamma(1-e^{-\sigma}) = 0 \quad \delta = \frac{4\varepsilon V^2}{(1-v)^2}$$

Now as $\sigma \rightarrow \infty$ we must have

$$\sigma(\delta + e^{-\sigma}) \gg \gamma(1-e^{-\sigma})$$

& so we must have

$$v\sigma^2 \approx -\sigma(\delta + e^{-\sigma})$$

$$\text{i.e. } v\sigma \approx -\delta - e^{-\sigma}$$

$$\text{LHS} \rightarrow 0 \Rightarrow e^{-\sigma} \rightarrow \infty \Rightarrow \operatorname{Re}\sigma \rightarrow \infty \Rightarrow \text{well-posed.}$$

Instability Clearly as $v, \delta \rightarrow 0$ there's instability because of (b)

Therefore the steady state is unstable for sufficiently small $v + \delta$, i.e. small enough Σ .