

2014 Q(1)b $\frac{1}{r} \frac{d}{dr} \left(r \frac{dw}{dr} \right) = \frac{G}{\mu}$, constant,

with $w=0$ on $r=b$ (outer wall)
 $w=-U$ on $r=a$ (inner wall).

$$w = \frac{G}{4\mu} (r^2 - b^2) + \frac{\log(r/b)}{\log(b/a)} \left(U - \frac{G}{4\mu} (b^2 - a^2) \right)$$

iii) The drag force is $\iint_{\text{bdry}} \underline{\sigma} \cdot \underline{n} \, dS$ in the z direction



$$\sigma_{13} = \mu \frac{dw}{dr} = \mu \left(\frac{Gr}{2\mu} + \frac{A}{r} \right)$$

The drag on the $r=a$ wall is

$$\iint_{r=a} \sigma_{13} \, dS = 2\pi a \mu \left(\frac{Ga}{2\mu} + \frac{A}{a} \right) = \pi Ga^2 + 2\pi A \mu$$

The drag on the $r=b$ wall is

$$- \iint_{r=b} \sigma_{13} \, dS = -\pi Gb^2 - 2\pi A \mu$$

The total drag is $\pi G(a^2 - b^2)$, which is $G \times$ cross-sectional area.

This comes from $\nabla^2 w = \frac{G}{\mu}$ and the divergence theorem.

$$\iint_{\text{annulus}} \nabla \cdot (\nabla w) \, dS = \iint_{\text{annulus}} \frac{G}{\mu} \, dS$$

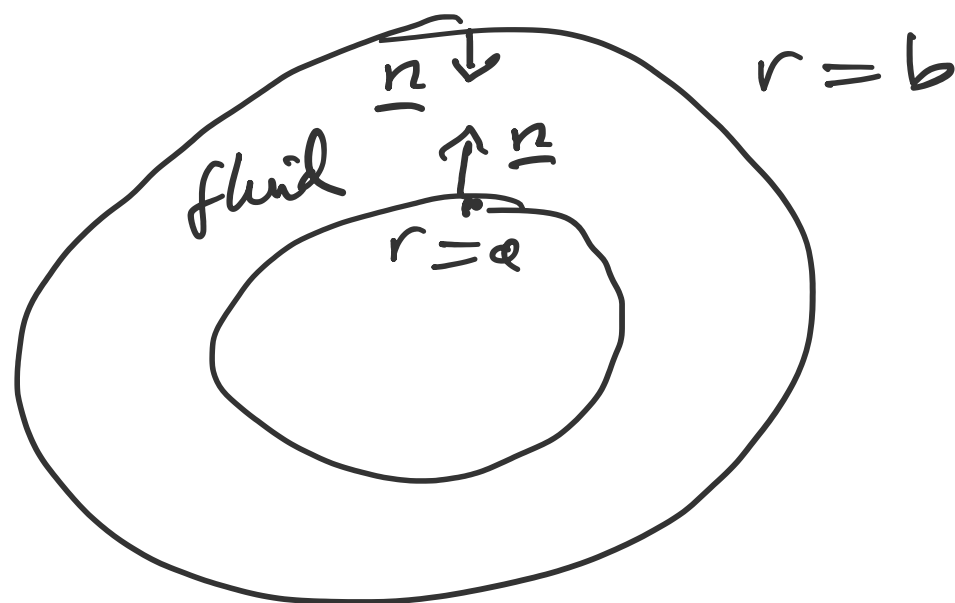
$$\int_{\partial(\text{annulus})} \mu \frac{\partial w}{\partial n} \, dS = G \iint_{\text{annulus}} dS$$

$= G \times$ cross-sectional area.

$\underline{\sigma} \cdot \underline{n}$ is the force exerted by the fluid towards which \underline{n} points.

$\underline{n} = \underline{e}_r$ on $r=a$

$\underline{n} = -\underline{e}_r$ on $r=b$



The only velocity component is w , and the only coordinate is r , so the only nonzero component of the viscous stress is $\sigma_{13} = \mu \frac{dw}{dr}$.

If w depended on θ , we'd need

$$\int_{\partial V} \mu \frac{\partial w}{\partial n} \, dS \quad \text{where} \quad \frac{\partial w}{\partial n} \quad \text{might have} \quad \frac{\partial w}{\partial \theta} \quad \text{term.}$$

$$\text{general} \quad = \int_{\partial V} \underline{k} \cdot \underline{\sigma} \cdot \underline{n} \, dS \quad \text{using}$$

$$\underline{\sigma} = -p \underline{\underline{I}} + \mu \left((\nabla \underline{u}) + (\nabla \underline{u})^T \right)$$

In complete generality, the drag force is

$$\iint_{\text{bdry}} \underline{\sigma} \cdot \underline{n} \, dS$$

with \underline{n} pointing into the fluid.

2014 Q3.

We've told that $\frac{SLWP}{\mu} \ll 1$, as well as $S \ll 1$.

M determines h , and hence $S = \frac{h}{L}$.

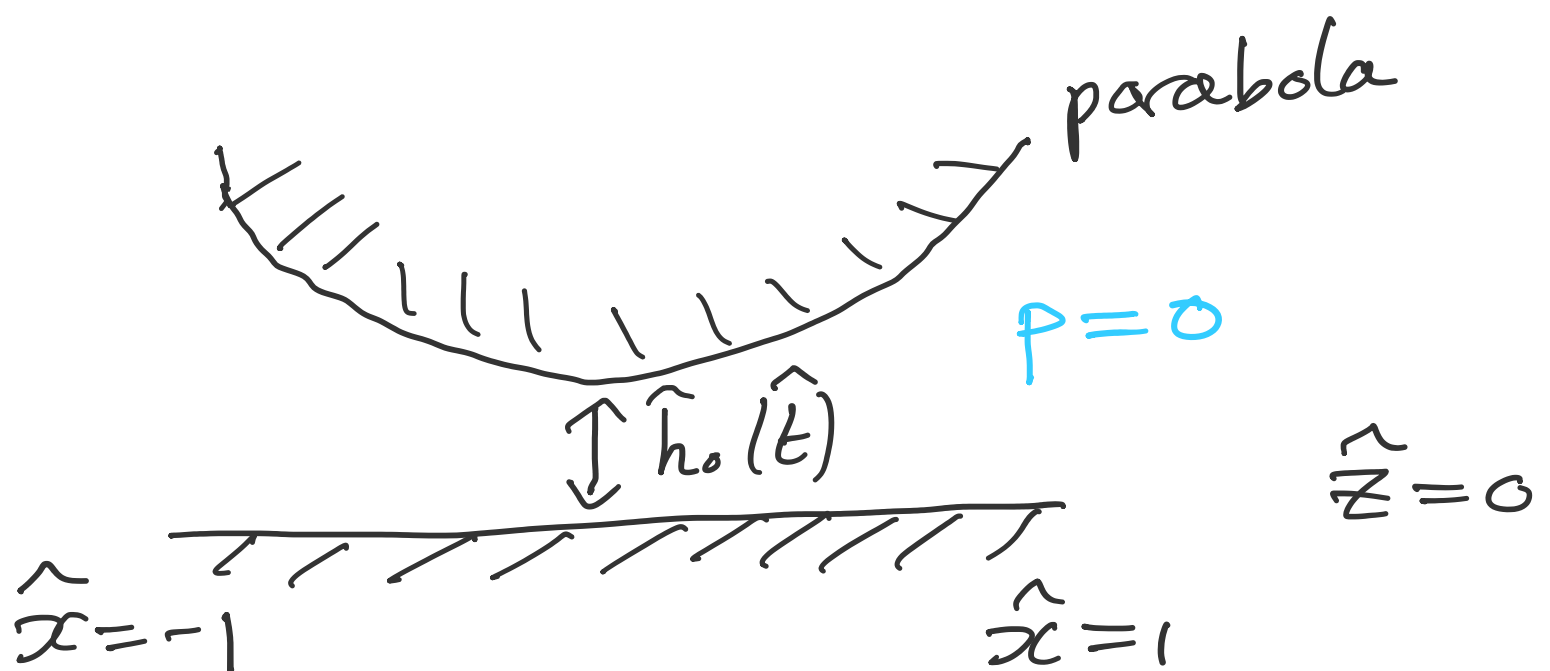
We need M large enough to ensure $S \ll 1$.

However, W, L, P, μ are all prescribed and don't depend on M .

$$\therefore S \text{ sufficiently small} \Rightarrow \frac{SLWP}{\mu} \ll 1.$$

We need $S \ll \min \left(1, \frac{\mu}{LWP} \right)$.

2013 Q3



Atmospheric pressure at $\hat{x}=1$, and also at $\hat{x}=-1$, so $\hat{p}(\pm 1, \hat{t}) = 0$.

This problem is symmetric about $\hat{x}=0$.

The pressure \hat{p} is an even fn of \hat{x} .

$\Rightarrow \frac{\partial \hat{p}}{\partial \hat{x}}$ is an odd function of \hat{x}

$\Rightarrow \frac{\partial \hat{p}}{\partial \hat{x}} = 0$ on $\hat{x}=0$ for all \hat{t} .

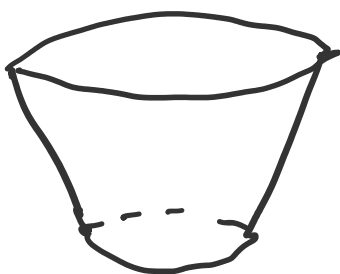
2017 Q3

The flux through a surface S is

$$\iint_S \underline{u} \cdot \underline{n} dS.$$

S

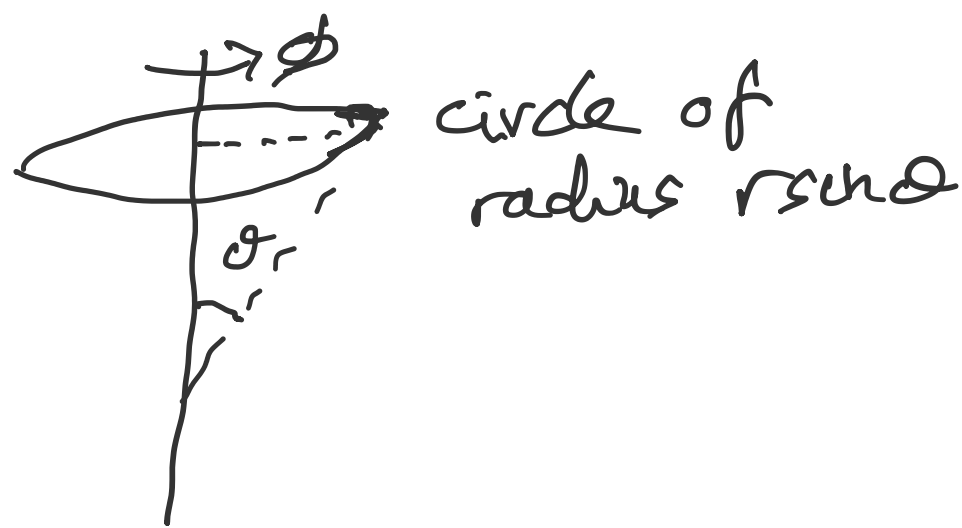
The surface $\theta = \theta_0$ is a truncated cone



The flux $F = \int_0^{2\pi} d\phi \int_a^{\lambda a} dr (r \sin \theta) u_\theta$

$$d\underline{r} = dr \underline{e}_r + r d\theta \underline{e}_\theta + r \sin \theta d\phi \underline{e}_\phi$$

In plane polar the area element would be $r dr d\phi$, for circles of radius r .



In spherical polar, changing ϕ moves around a circle of radius $r \sin \theta$, so our area element is $r \sin \theta dr d\phi$.

$$F = \int_0^{2\pi} d\phi \int_a^{\lambda a} dr (r \sin \theta) \left(-\frac{1}{r \sin \theta} \frac{\partial \Psi}{\partial r} \right)$$

$$= -2\pi \int_a^{\lambda a} \frac{\partial \Psi}{\partial r} dr$$

$$= -2\pi \left[\Psi \right]_{r=a}^{r=\lambda a}.$$