

## Problem sheet 2

1. **Carbon cycles** Consider the dimensionless model from lectures for the evolution of albedo and partial pressure of atmospheric CO<sub>2</sub>,

$$\begin{aligned}\dot{a} &= f(a, p) = B(\Theta) - a, \\ \dot{p} &= g(a, p) = \alpha(1 - wp^\mu e^\Theta),\end{aligned}$$

where  $\Theta(a, p) = \frac{q(1-a)^{-1}}{\nu} + \lambda p$ , and  $B(\theta)$  is a monotonic function decreasing from  $a_+$  to  $a_-$ . Here,  $\mu$ ,  $\alpha$ ,  $\nu$ ,  $\lambda$ ,  $w$ , and  $q$  are all constant parameters.

- (i) Show that the  $p$  nullcline,  $a = G(p)$  say, is a monotonically increasing function of  $p$ , and that the  $a$  nullcline,  $a = F(p)$ , is a monotonically decreasing function if  $-B'(\theta) < \nu/q$  for all  $\theta$ , but is multivalued if  $-B'(\theta) > \nu/q$  for some range of  $\theta$ .
- (ii) Now suppose that the  $a$  nullcline is indeed multivalued, but that there is always a unique steady state, which may lie on the lower, intermediate, or upper branch depending on the value of  $w$ . Sketch the nullclines for each of these cases. By considering the signs of the partial derivatives of  $f(a, p)$  and  $g(a, p)$  (but without detailed calculation), show that steady states on the upper or lower branch are stable, but the intermediate state is unstable if  $\alpha$  is small enough. How would you expect the solutions to behave if  $\alpha \ll 1$ ?
2. **Ocean carbon** A model for the global climate is

$$\begin{aligned}c \frac{dT}{dt} &= \frac{1}{4}Q(1-a) - \sigma\gamma(p)T^4, & t_i \frac{da}{dt} &= a_0(T) - a, \\ \frac{A_E M_{\text{CO}_2}}{g M_a} \frac{dp}{dt} &= v - h(p - p_s), & \rho_O V_O \frac{dC}{dt} &= \frac{h(p - p_s)}{M_{\text{CO}_2}} - bC,\end{aligned}$$

where  $p_s = C/K$  is the effective partial pressure of CO<sub>2</sub> in the ocean (*i.e.* the partial pressure of a gas in equilibrium with the water).

- (i) Briefly explain the meaning of the terms in this model and the physical principles on which it is based.
- (ii) Estimate the timescales involved using the parameter values listed below. Hence show that a suitable quasi-steady approximation of the model is

$$t_i \dot{a} = a_0(T) - a, \quad t_C \dot{C} = C_v - C,$$

where  $t_C = \rho_O V_O / b$ ,  $C_v = v / M_{\text{CO}_2} b$ , and where

$$p \approx \frac{C}{K} + \frac{v}{h}, \quad T \approx \left( \frac{Q(1-a)}{4\sigma\gamma(p)} \right)^{1/4}.$$

- (iii) Assuming that the ocean was in equilibrium with pre-industrial emissions, infer the value of those emissions (*i.e.*  $v$ ) given the present day value of  $C \approx 2 \times 10^{-3}$  mol kg<sup>-1</sup>, and estimate the pre-industrial value of atmospheric CO<sub>2</sub> given by  $p$ .
- (iv) Suppose the present-day emissions  $v \approx 30 \times 10^{12}$  kg y<sup>-1</sup> are maintained indefinitely. Use the model to show that on a timescale of centuries  $p$  will reach an approximate equilibrium and find its value. Show that thereafter  $p$  will continue to increase, on a timescale of millennia. What is the eventual value of  $p$ ?

Parameter values:  $c = 10^7$  J m<sup>-2</sup> K<sup>-1</sup>,  $Q = 1370$  W m<sup>-2</sup>,  $\sigma = 5.67 \times 10^{-8}$  W m<sup>-2</sup> K<sup>-4</sup>,  $t_i = 10^4$  y,  $A_E = 5.1 \times 10^{14}$  m<sup>2</sup>,  $g = 9.8$  m s<sup>-2</sup>,  $M_{\text{CO}_2} = 44 \times 10^{-3}$  kg mol<sup>-1</sup>,  $M_a = 29 \times 10^{-3}$  kg mol<sup>-1</sup>,  $h = 0.73 \times 10^{12}$  kg y<sup>-1</sup> Pa<sup>-1</sup>,  $\rho_O = 10^3$  kg m<sup>-3</sup>,  $V_O = 1.35 \times 10^{18}$  m<sup>3</sup>,  $b = 0.83 \times 10^{16}$  kg y<sup>-1</sup>,  $K = 7.1 \times 10^{-5}$  mol kg<sup>-1</sup> Pa<sup>-1</sup>.

### 3. River cross-sections

- (i) Calculate the relationship between hydraulic radius  $R$  and cross-sectional area  $A$  for (i) a rectangular cross-section of fixed width  $w$  (you may assume the width is much wider than the depth), and (ii) a triangular cross-section with transverse slope angle  $\beta$ .
- (ii) Use Manning's law,  $u = R^{2/3}S^{1/2}/n$ , to derive the equation

$$\frac{\partial A}{\partial t} + cA^m \frac{\partial A}{\partial x} = E,$$

for the cross-sectional area of a river, where  $E$  is a prescribed source term, giving explicit formulas for  $c$  and  $m$  in each of case (i) and (ii).

- (iii) What initial and boundary conditions you would expect to apply to this equation? Why would this equation not be able to describe the behaviour of a tidal river such as the Thames in London?
- (iv) For the case  $E = 0$ , with  $A(x, 0) = A_0(x)$  on  $-\infty < x < \infty$ , find an implicit solution to the equation. Show that if  $A'_0(x) < 0$  for some  $x$  then a shock will form, and find expressions for the time and location at which the shock first forms in terms of  $A_0(x)$ .

### 4. Overland flow

Overland flow on a hill slope is described by the equation

$$\frac{\partial h}{\partial t} + ch^m \frac{\partial h}{\partial x} = E,$$

where  $E = P - I$  is the excess rainfall rate, being the difference between precipitation and infiltration rates. The equation is to be solved in  $x > 0$ , and the initial and boundary condition are

$$h = 0 \quad \text{at} \quad t = 0, x > 0 \quad \text{and} \quad x = 0, t > 0.$$

- (i) First consider the case of constant  $E > 0$ . Solve the equation and sketch the solution at various times.
- (ii) Next, consider the case where  $E(t)$  is time dependent, such that  $E \geq 0$  for  $0 \leq t \leq t_*$ , and  $E < 0$  for  $t > t_*$ . Find an implicit expression for the solution in terms of integrals of  $E$  for  $t \leq t_*$ .
- (iii) For  $t > t_*$ , a drying front moves down the slope (behind which  $h = 0$ ). Determine the position of the front  $x_d(t)$  as a function of time and hence find the complete solution for all  $t > 0$ .