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$$\rho [\underline{u}_t + (\underline{u} \cdot \underline{\nabla}) \underline{u}] = -\underline{\nabla} p - \rho g \underline{k} + \mu \nabla^2 \underline{u}$$

$$p = p_0 [1 - \alpha (T - T_0)]$$

(a) $u \sim d$ $t \sim \frac{d^2}{\nu}$, $u \sim \frac{\nu}{d}$, $p + p_0 \delta z \sim \frac{\mu \nu}{d^2}$

$T - T_0 \sim \Delta T$, $\rho \sim \rho_0$

(also $T_t + \underline{\nabla} \cdot (p \underline{u}) = 0$)

$T_t + \underline{\nabla} \cdot (T \underline{u}) = \kappa \nabla^2 T$)

\Rightarrow $\frac{\mu \nu \Delta T \rho_0}{\rho_0 \nu} \rho_0$

$\rho = 1 - \beta T$ $\beta = \alpha \Delta T$

$\rho_t + \underline{\nabla} \cdot (p \underline{u}) = 0$

$T_t + \underline{\nabla} \cdot (T \underline{u}) = \nabla^2 T$

and

$$\rho_0 \frac{\nu^2}{d^3} \rho [\underline{u}_t + (\underline{u} \cdot \underline{\nabla}) \underline{u}] = -\frac{\mu \nu}{d^3} \underline{\nabla} p + \alpha \rho_0 \Delta T g T \underline{k} + \frac{\mu \nu}{d^3} \nabla^2 \underline{u}$$

$$\Rightarrow \frac{\rho_0 \nu}{\mu} \rho [\underline{u}_t + (\underline{u} \cdot \underline{\nabla}) \underline{u}] = -\underline{\nabla} p + \frac{\alpha \rho_0 \Delta T g d^3}{\mu \nu} T \underline{k} + \nabla^2 \underline{u}$$

$$\text{or } \frac{1}{Pr} \rho [\underline{u}_t + (\underline{u} \cdot \underline{\nabla}) \underline{u}] = -\underline{\nabla} p + Ra T \underline{k} + \nabla^2 \underline{u}$$

$Pr = \frac{\mu}{\rho_0 \nu}$ $Ra = \frac{\alpha \rho_0 \Delta T g d^3}{\mu \nu}$

(b) $B \ll 1 \Rightarrow \rho = 1$

neglect $(\underline{u} \cdot \nabla) \underline{u}$ (apparently)

$\Rightarrow \nabla \cdot \underline{u} = 0$
 $T_t + \underline{u} \cdot \nabla T = \nabla^2 T$

$\frac{1}{Pr} \underline{u}_t = -\nabla p + Ra T_t + \nabla^2 \underline{u}$

take curl, $\underline{\omega} = \text{curl} \underline{u} = \begin{pmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{pmatrix} = (w_y - v_z, u_z - w_x, v_x - u_y)$

$\frac{1}{Pr} \underline{\omega}_t = Ra \text{curl}(T_t) + \text{curl}[\text{grad div} \underline{u} - \text{curl} \text{curl} \underline{u}]$
 $= Ra \begin{pmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 0 & T \end{pmatrix} - \text{curl} \text{curl} \underline{\omega} \quad [+ \text{grad div} \underline{\omega}]$

$= Ra(T_y, -T_x, 0) + \nabla^2 \underline{\omega}$

Now if $\underline{\omega} = \underline{\omega} \cdot \underline{k} = v_x - u_y$

then $\zeta_t = Pr \nabla^2 \zeta$

(c) If $u = dx - \psi_y, v = dy + \psi_x$ (so ∇^2 is 2-D here)
then $u_x + v_y = \nabla^2 \phi, v_x - u_y = \nabla^2 \psi$

so $w_z = -\nabla^2 \phi, \zeta = \nabla^2 \psi$

if we take $\underline{u} = (u_1(z) \exp[i(k_1 x + k_2 y) + \sigma t])$ (so $\phi = \bar{\phi} \exp$
 $\psi = \bar{\psi} \exp$)

we have $w_1' = +k^2 \bar{\phi}, \zeta = -k^2 \bar{\psi}$ $\zeta = \bar{\zeta} \exp$

and $u_1 = ik_1 \bar{\phi} - ik_2 \bar{\psi}$
 $v_1 = ik_2 \bar{\phi} + ik_1 \bar{\psi}$

$\bar{\phi} = + \frac{w_1'}{k^2}$, ~~$\bar{\psi} = \frac{1}{k^2} z$~~ $\bar{\psi} = -\frac{1}{k^2} z$

$\Rightarrow u_1 = + ik_1 \frac{w_1'}{k^2} + ik_2 z$

$v_1 = + ik_2 \frac{w_1'}{k^2} - ik_1 z$

Δ x by $\exp[ik_x x + ik_y y + i\omega t]$

$\Rightarrow u = \frac{1}{k^2} [+w_{xz} + \zeta_y]$
 $v = \frac{1}{k^2} (w_{yz} - \zeta_x)$

(d) Stress free boundaries at $z=0, 1$ (non-d) $\Rightarrow \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} = \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} = 0$

$\Rightarrow u_z = v_z = 0$ (as $w=0$)

$\Rightarrow \frac{\partial \zeta}{\partial z} = 0$

$\zeta_t = \rho \nabla^2 \zeta$ here ∇^2 is 3-D

$\zeta = \eta \exp[ik_x x + ik_y y + i\omega t]$ but $\sigma \neq 0$

so $\zeta_{zz} - k^2 \zeta = 0 \Rightarrow \zeta_z = 0$ at $z=0, 1$

$\Rightarrow \zeta = A \cosh k z$ can't satisfy bc's $\Rightarrow A=0$

$u_z \zeta = 0$ [actually wrong, $\nabla^2 \zeta = 0, \zeta = 0 \Rightarrow u_z \zeta = 0$]

(e) $w = A \sin \bar{u} t \cos k_1 x \cos k_2 y$

$\zeta = 0$

$u = \frac{1}{k^2} w_{yx} = -\frac{A \bar{u} k_1}{k^2} \cos \bar{u} t \sin k_1 x \cos k_2 y$

$v = \frac{1}{k^2} w_{yz} = -\frac{A \bar{u} k_2}{k^2} \cos \bar{u} t \cos k_1 x \sin k_2 y$

$k_1 = k_2 = k$

$u = -\frac{A \bar{u} k \cos \bar{u} t}{k^2} \sin k x \cos k y$

$v = -\frac{A \bar{u} k \cos \bar{u} t}{k^2} \cos k x \sin k y$

Streamlines in horizontal plane ~~as for~~ as for

~~$v = -\frac{A \bar{u} k \cos \bar{u} t}{k^2} \cos k x \sin k y$~~ $(\sin k x \sin k y)$ y

~~$u = -\frac{A \bar{u} k \cos \bar{u} t}{k^2} \sin k x \cos k y$~~

$u = \sin k x \cos k y$

$v = \cos k x \sin k y$

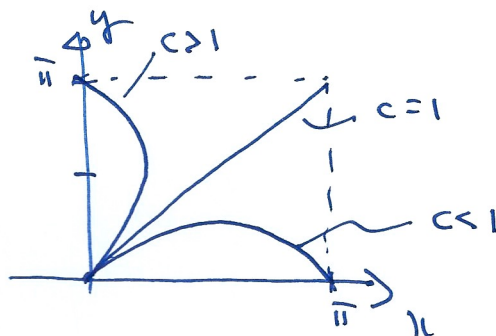
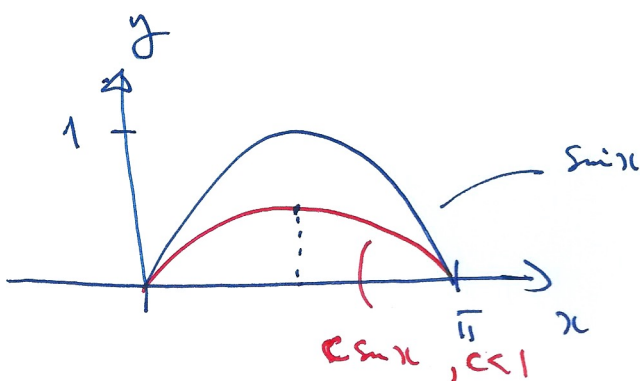
or... 'streamlines' are $\frac{dy}{dx} = \frac{v}{u} = \frac{\cos k x \sin k y}{\sin k x \cos k y}$

$\Rightarrow \sin k y = c \sin k x$ or ?

Did he really mean this? Quite challenging I'd say

$\sin y = c \sin x$ ($k=1 \text{ wlog}$)

and in a single cell say $0 < x < \bar{\pi}$, $0 < y < \bar{\pi}$ (so $x=0$ or $x=\bar{\pi}$, $y=0$ or $y=\bar{\pi}$)



so $y \uparrow 0$ to $\bar{\pi}$ as $c \downarrow$ and $x \rightarrow \bar{\pi}$

if $c \geq 1$ $\sin x = \sin y \Rightarrow x = y$

if $c > 1$ $\sin x = \frac{1}{c} \sin y$ so just reflected

what happens if c is close to ($<$) 1?

~~then $y = x$ for all x near $\bar{\pi}$~~

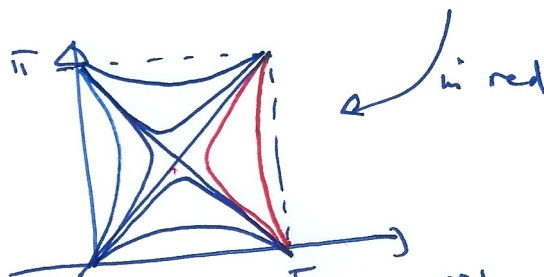
~~for $x = \bar{\pi}$~~

~~$\sin y$~~

well there is a choice

$y = \sin^{-1}(c \sin x) \in (0, \bar{\pi})$

or $\bar{\pi}$ - the above



two projections of shear lines

then repeated (oddly) as

same 'shear lines' but opposite sign of 'shear factor'

