Topics in fluid mechanics

PROBLEM SHEET 4.

1. Derive a reference state for a dry atmosphere (no condensation) by using the equation of state

$$p = \frac{\rho RT}{M_a},$$

the hydrostatic pressure

$$\frac{\partial p}{\partial z} = -\rho g_z$$

and the dry adiabatic temperature equation

$$\rho c_p \frac{dT}{dt} - \frac{dp}{dt} = 0.$$

Show that

$$\bar{T} = T_0 - \frac{gz}{c_p}, \quad \bar{p} = p_0 p^*(z),$$

where

$$p^*(z) = \left(1 - \frac{gz}{c_p T_0}\right)^{M_a c_p/R}$$

Use the typical values $c_p T_0/g \approx 29$ km, $M_a c_p/R \approx 3.4$, to show that the pressure can be adequately represented by

$$\bar{p} = p_0 \exp(-z/H),$$

where here the scale height is defined as

$$H = \frac{RT_0}{M_a g} \approx 8.4 \text{ km.}$$

(A slightly better numerical approximation near the tropopause is obtained if the scale height is chosen as 7 km.)

2. The mass and momentum equations for atmospheric motion in the rotating frame of the Earth can be written in the form

$$\rho_t + \boldsymbol{\nabla} \cdot [\rho \mathbf{u}] = 0,$$
$$\rho \left[\frac{d\mathbf{u}}{dt} + 2\boldsymbol{\Omega} \times \mathbf{u} \right] = -\boldsymbol{\nabla} p - \rho g \hat{\mathbf{k}},$$

where (x, y, z) are local Cartesian coordinates at latitude $\lambda = \lambda_0$. What is the magnitude of Ω ?

Scale the variables by writing

$$x, y \sim l, \quad z \sim h, \quad u, v \sim U, \quad w \sim \delta U, \quad t \sim \frac{l}{U},$$

$$\rho \sim \rho_0, \quad T \sim T_0, \quad p = p_0 \bar{p}(z) + 2\rho_0 \Omega U l \sin \lambda_0 P_s$$

where

$$\delta = \frac{h}{l}, \quad p_0 = \rho_0 g h = \frac{\rho_0 R T_0}{M},$$

and show that the horizontal components take the form

$$\varepsilon \frac{du}{dt} - fv = -\frac{1}{\rho} P_x,$$

$$\varepsilon \frac{dv}{dt} + fu = -\frac{1}{\rho} P_y,$$

where

$$f = \frac{\sin \lambda}{\sin \lambda_0},$$

and give the definition of the Rossby number ε . Show that in a linear approximation,

$$f \approx 1 + \varepsilon \beta y,$$

where

$$\beta = \frac{l}{R_E} \frac{\cot \lambda_0}{\varepsilon} = O(1),$$

and R_E is Earth's radius.

The dimensionless pressure $\Pi = p/p_0$, density ρ , temperature T and potential temperature θ in the atmosphere satisfy the relations

$$\rho = \frac{\Pi}{T}, \quad T = \theta \Pi^{\alpha}, \quad -\frac{\partial \Pi}{\partial z} = \rho,$$

where $\alpha = \frac{R}{M_a c_p}$ is constant. Assuming that

$$\Pi = \bar{p} + \varepsilon^2 P, \quad \theta = \bar{\theta} + \varepsilon^2 \Theta,$$

and that $\varepsilon \ll 1$, deduce that $\rho \approx \bar{\rho}(z)$, and thence that

$$w = O(\varepsilon), \quad \bar{\rho}u \approx -P_y, \quad \bar{\rho}v \approx P_x.$$

Show also that consistency between the two forms of scaled pressure requires the definition of the velocity scale to be

$$U = \frac{8(\Omega l \sin \lambda_0)^3}{gh},$$

and determine this value, if l = 1,000 km, $\lambda_0 = 45^{\circ}$, g = 9.8 m s⁻², h = 8 km. Show that

$$\Theta \approx \bar{\theta}^2 \frac{\partial}{\partial z} \left[\frac{P}{\bar{p}^{1-\alpha}} \right],$$

and by defining a stream function via $P = \bar{\rho}\psi$ and assuming that $\bar{\theta} \approx 1$, deduce that $\Theta \approx \psi_z$, and hence deduce the *thermal wind equations*:

$$\frac{\partial u}{\partial z} = -\frac{\partial \Theta}{\partial y}, \quad \frac{\partial v}{\partial z} = \frac{\partial \Theta}{\partial x}.$$

3. The quasi-geostrophic potential vorticity equation is

$$\frac{d}{dt} \left[\nabla^2 \psi + \frac{1}{\bar{\rho}} \frac{\partial}{\partial z} \left(\frac{\bar{\rho}}{S} \frac{\partial \psi}{\partial z} \right) \right] + \beta \psi_x = \frac{1}{\bar{\rho}} \frac{\partial}{\partial z} \left(\frac{\bar{\rho}H}{S} \right),$$

where $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$, and $\bar{\rho}$, S and H are functions of z, the first two being positive. The horizontal material derivative is

$$\frac{d}{dt} = \frac{\partial}{\partial t} + u\frac{\partial}{\partial x} + v\frac{\partial}{\partial y}, \quad u = -\psi_y, \quad v = \psi_x.$$

In the Eady model of baroclinic instability, solutions to the QGPVE are sought in a channel 0 < y < 1, 0 < z < 1, with boundary conditions

$$\frac{d}{dt}\psi_z = 0 \quad \text{at} \quad z = 0, 1, \qquad \psi_x = 0 \quad \text{at} \quad y = 0, 1,$$

and it is supposed that $\bar{\rho}$ and S are constant, and $\beta = H = 0$. Show that a particular solution is the zonal flow $\psi = -yz$, and describe its velocity field. By considering the thermal wind equations, explain why this is a meaningful solution.

By writing $\psi = -yz + \Psi$ and linearising the equations, derive an equation for Ψ , and show that it has solutions

$$\Psi = A(z)e^{ik(x-ct)}\sin n\pi y,$$

providing

$$(z-c)(A''-\mu^2 A) = 0,$$

 $(z-c)A' = A$ on $z = 0, 1,$

where you should define μ .

Using the fact that $x\delta(x) = 0$, show that if 0 < c < 1, the solution can be found as a Green's function for the equation $A'' - \mu^2 A = 0$.

Give a criterion for instability, and show that for the normal mode solutions in which A is analytic,

$$c = \frac{1}{2} \pm \frac{1}{\mu} \left\{ \left(\frac{\mu}{2} - \coth \frac{\mu}{2} \right) \left(\frac{\mu}{2} - \tanh \frac{\mu}{2} \right) \right\}^{1/2},$$

and hence show that the zonal flow is unstable if $\mu < \mu_c$, where

$$\frac{\mu}{2} = \coth\frac{\mu}{2},$$

and calculate this value. Deduce that the flow is unstable for $S < S_c$, and calculate S_c .

4. A basic two fluid model of two-phase flow is given by the equations

$$(\alpha \rho_g)_t + (\alpha \rho_g v)_z = \Gamma,$$

$$\{\rho_l(1-\alpha)\}_t + \{\rho_l(1-\alpha)u\}_z = -\Gamma,$$

$$\rho_g[v_t + vv_z] = -p_z - M,$$

$$\rho_l[u_t + D_l uu_z] = -p_z + M,$$

where α is void fraction, u and v are liquid and gas phase velocities, p is pressure, and ρ_g and ρ_l are gas and liquid densities; the constant $D_l > 1$ is a profile coefficient, and Γ and M are interfacial source and drag terms, which are prescribed algebraic functions of the variables.

Explain how to find the characteristics of this system when written in the form

$$A\boldsymbol{\psi}_t + B\boldsymbol{\psi}_z = \mathbf{c}.$$

(i) Assuming ρ_g and ρ_l are constant and $\rho_g \ll \rho_l$, show that the characteristics are generally real.

(ii) If

$$\frac{d\rho_g}{dp} = \frac{1}{c_g^2}, \quad \frac{d\rho_l}{dp} = \frac{1}{c_l^2};$$

calculate approximate values of the characteristics if $u \sim v \ll c_l \sim c_g$ and $\rho_g \ll \rho_l$, and comment on the physical significance of these.

5. The energy equation for a one-dimensional two-phase flow in a tube is given by

$$\Gamma L + \alpha \rho_g c_{pg} (T_t + vT_z) + (1 - \alpha) \rho_l c_{pl} (T_t + uT_z) - \{ (\alpha p_g)_t + (\alpha p_g v)_z \} - [\{ (1 - \alpha) p_l \}_t + \{ (1 - \alpha) p_l u \}_z] = Q,$$

where

$$\Gamma = (\alpha \rho_g)_t + (\alpha \rho_g v)_z = -[\{(1 - \alpha)\rho_l\}_t + \{(1 - \alpha)\rho_l u\}_z],$$

and the temperatures of the two phases are assumed equal, and denoted by T. The enthalpy of each phase satisfies $dh_k = c_{pk} dT$, and is related to the internal energy e_k by

$$h_k = e_k + \frac{p_k}{\rho_k};$$

 $L = h_g - h_l$ is the latent heat. Deduce that the energy equation can be written in the form

$$(\alpha \rho_g e_g)_t + (\alpha \rho_g e_g v)_z + [(1 - \alpha) \rho_l e_l]_t + [(1 - \alpha) \rho_l e_l u]_z = Q.$$

Define the mixture density by

$$\rho = \rho_l (1 - \alpha) + \rho_g \alpha,$$

the mixture pressure by

$$p = (1 - \alpha)p_l + \alpha p_g,$$

the mixture internal energy by

$$\rho e = \alpha \rho_g e_g + (1 - \alpha) \rho_l e_l,$$

and the mixture enthalpy by

$$h = e + \frac{p}{\rho};$$

deduce that

$$\rho h = \alpha \rho_g h_g + (1 - \alpha) \rho_l h_l$$

If the flow is homogeneous, deduce that

$$\rho \frac{de}{dt} = 0,$$

where $\frac{d}{dt}$ is the material derivative, and if the pressure drop along the tube $\Delta p \ll \rho_g L$, show that $h \approx e$, and deduce that

$$\frac{\partial u}{\partial z} = \frac{(\rho_l - \rho_g)Q}{\rho_g \rho_l L}$$

6. An approximate homogeneous two-phase model for density wave oscillations in a pipe of length l is given by

$$\rho_t + u\rho_z = -u_z\rho,$$

$$\rho(u_t + uu_z) = -p_z - \rho g - \frac{4f\rho u^2}{d},$$

$$\rho(h_t + uh_x) = Q,$$

where Q is constant, and

$$h \approx h^* + \frac{\rho_g L}{\rho}$$

in the two-phase region; h^* , L and Q are constants, ρ_g and ρ_l are (constant) gas and liquid densities, h is enthalpy, and ρ , p and u are mixture density, pressure and velocity. For $h < h_{\text{sat}}$, the saturation enthalpy, only liquid is present, $\rho = \rho_l$, and the above relation for h is irrelevant.

Boundary conditions for the flow are that

$$h = h_0 < h_{\text{sat}}, \quad u = U(t) \quad \text{at} \quad z = 0,$$

 $h = h_{\text{sat}} \quad \text{on} \quad z = r(t),$

where the unknown boiling boundary r(t) is to be determined, and the pressure drop along the pipe, Δp , is prescribed.

Show that

$$r(t) = \int_{t-\tau}^{t} U(s) \, ds,$$

and give the definition of τ .

Non-dimensionalise the two-phase model by scaling

$$\rho \sim \rho_l, \quad z, r \sim l, \quad t \sim \tau, \quad u, U \sim u_0,$$

and show that the two-phase velocity and density satisfy

$$u = U + \frac{z - r}{\varepsilon}, \quad z = r + \varepsilon \int_0^{-\ln \rho} U_1(t - \varepsilon \xi) e^{\xi} d\xi, \quad r = \int_{t-1}^t U(s) ds,$$

where $U_1(t) = U(t-1)$, and give the definition of ε .

Show that the pressure drop in the single phase region is

$$\Delta p_{sp} = [\Delta p_i \dot{U} + \Delta p_g + \Delta p_f U^2]r,$$

where

$$\Delta p_i = \rho_l u_0^2, \quad \Delta p_g = \rho_l g l, \quad \Delta p_f = \frac{4f l \rho_l u_0^2}{d}, \quad u_0 = \frac{l}{\tau}.$$

Write down an integral expression for the two-phase pressure drop in the form

$$\Delta p_{tp} = \int_{r}^{1} (\Delta p_{i} \Phi_{i} + \Delta p_{g} \Phi_{g} + \Delta p_{f} \Phi_{f}] dz,$$

where the functions Φ_k depend on u and ρ and their derivatives.

If U = V in the steady state, explain why 0 < V < 1. Write down an expression for Δp as a function of V. Show that if V is sufficiently close to one, Δp is an increasing function of V, but that if ε is sufficiently small, it is a decreasing function of V.

Now suppose that $\Delta p_i = \Delta p_g = 0$. To examine the stability of the steady state (denoted by a suffix zero for r, u and ρ), write

$$U = V + v, \quad r = r_0 + r_1, \quad u = u_0 + u_1, \quad \rho = \rho_0 + \rho_1,$$

and linearise the equations. Hence derive expressions for r_1 , u_1 and ρ_1 .

By taking $v = e^{\sigma t}$, derive an algebraic equation for σ from the condition that the perturbation to Δp is zero. If only the single phase pressure drop term is included, show that

$$\sigma = -\frac{1}{2}(1 - e^{-\sigma}),$$

and deduce that the steady state is stable.

If only the two-phase pressure drop is included, and ε is assumed to be small, show that

$$\sigma = \gamma (e^{\sigma} - 1), \quad \gamma = \frac{2V}{1 - V},$$

and deduce that $\operatorname{Re} \sigma \to \infty$ as $\sigma \to \infty \in \mathbf{C}$, and thus that the model is ill-posed. If both pressure drops are included (and the two-phase approximation for small ε is used), show that

$$\sigma = \frac{\gamma(1 - e^{-\sigma})}{\delta + e^{-\sigma}}, \quad \delta = \frac{4\varepsilon V^2}{(1 - V)^2},$$

and deduce that the model is ill-posed for $\delta < 1$.

Finally, if the inertial term in the single phase region (only) is included, show that

$$\nu\sigma^2 + \sigma(\delta + e^{-\sigma}) - \gamma(1 - e^{-\sigma}) = 0, \quad \nu = \frac{2\varepsilon\Delta p_i}{(1 - V)^2\Delta p_f},$$

and deduce that the model is well-posed, but the steady state is unstable for small $\varepsilon.$