Further Partial Differential Equations Problem Sheet 4

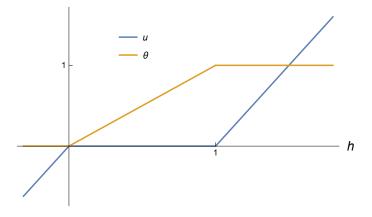


Figure 1: Normalised temperature u and liquid fraction θ versus enthalpy h.

1. Enthalpy for mushy layers

Show that the free boundary problem (2.31) may be posed as

$$\frac{\partial h}{\partial t} = \frac{\partial^2 u}{\partial x^2} + q,$$

where $h = \text{St}u + \theta$ is the (dimensionless) *enthalpy*. Deduce that u is a piecewise linear function of h, as indicated in figure 1.

2. Unsteady electropainting

Consider the unsteady version of the model problem depicted in Figure 2.9, i.e., with the conditions on y = 0 replaced by

$$\begin{split} \frac{\partial \phi}{\partial y} &= \frac{\phi}{h}, \quad \frac{\partial h}{\partial t} &= \frac{\partial \phi}{\partial y} - \delta & \qquad y = 0, \ |x| < c, \\ \phi &= 0 & \qquad y = 0, \ |x| > c, \end{split}$$

where now c = c(t). Find the small-time behaviour of the solution by expanding

$$\phi(x, y, t) \sim \phi_0(x, y) + t\phi_1(x, y) + \cdots,$$

$$h(x, t) \sim th_1(x) + t^2h_2(x) + \cdots,$$

$$c(t) \sim c_0 + tc_1 + \cdots.$$

Show that painting commences provided $\delta < 1/\pi$, in which case the layer initially grows over a half-width $c_0 = \sqrt{1/(\delta \pi) - 1}$.

3. One-dimensional welding

(a) Consider the dimensionless one-dimensional welding problem (2.31). Show that, before melting occurs, the solution is given by

$$u(x,t) = -1 + \frac{q}{2} \left(1 - x^2\right) + \sum_{n=0}^{\infty} c_n \cos\left[\left(n + \frac{1}{2}\right) \pi x\right] e^{-\left(n + \frac{1}{2}\right)^2 \pi^2 t / \text{St}}$$

and use Fourier series to evaluate the constants c_n .

(b) Deduce that the sample will eventually melt provided q > 2, at a time $t_{\rm m}$ that satisfies

$$q = \left(\frac{1}{2} - 2\sum_{n=0}^{\infty} \frac{(-1)^n \mathrm{e}^{-\left(n+\frac{1}{2}\right)^2 \pi^2 t_{\mathrm{m}}/\mathrm{St}}}{\left(n+\frac{1}{2}\right)^3 \pi^3}\right)^{-1}.$$
 (1)

(c) Show that the leading-order asymptotic dependence of equation (1) between $t_{\rm m}/{\rm St}$ and q is

$$\begin{split} \frac{t_{\rm m}}{{\rm St}} &\sim \frac{1}{q} & {\rm as} \quad t_{\rm m}/{\rm St} \to 0, \\ \frac{t_{\rm m}}{{\rm St}} &\sim \frac{4}{\pi^2} \log\left(\frac{64}{\pi^3(q-2)}\right) & {\rm as} \quad t_{\rm m}/{\rm St} \to \infty. \end{split}$$

- (d) For $t > t_{\rm m}$, consider the free boundary problem (2.31). Explain why $s_2(t) = 0$ until $t = t_{\rm m} + 1/q$.
- (e) Now consider the limit $\text{St} \to 0$. Show that the plate will have melted entirely to a depth $x = 1 \sqrt{2/q}$ (so the mush has disappeared) after a time $t_c \sim t_m + 1/q + O(\text{St})$.
- (f) Show that the subsequent leading-order behaviour of the solid–liquid free boundary x = s(t) is governed by

$$\frac{\mathrm{d}s}{\mathrm{d}t} = \frac{q}{2}(1+s) - \frac{1}{1-s}, \qquad s(t_{\rm c}) = 1 - \sqrt{\frac{2}{q}}.$$

(g) Deduce that the solid ahead of the free boundary is not superheated, and that the system approaches a steady state with the plate melted to a depth $x = \sqrt{1 - 2/q}$.