

### B5.3 Viscous Flow: Sheet 4

**Q1 Slow flow past a circular cylinder.** Consider the two-dimensional steady viscous flow of a uniform stream with velocity  $U\mathbf{i}$  past a rigid circular cylinder of radius  $a$  whose centre is at the origin of the plane polar coordinate system  $(r, \theta)$ .

- (a) By scaling  $(r, \psi, \omega)$  with  $(a, Ua, U/a)$  in the vorticity–streamfunction formulation in sheet 1, Q5(c)(iii), show that the dimensionless problem is given by

$$Re \frac{1}{r} \frac{\partial(\psi, \omega)}{\partial(\theta, r)} = \nabla^2 \omega, \quad -\omega = \nabla^2 \psi \equiv \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \psi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2}.$$

with (upon taking  $\psi$  to be equal to zero on the cylinder)

$$\psi = \frac{\partial \psi}{\partial r} = 0 \text{ on } r = 1; \quad \psi \sim r \sin \theta \text{ as } r \rightarrow \infty,$$

where the Reynolds number  $Re = Ua/\nu$ .

- (b) When the Reynolds number is *small* (i.e.  $Re \ll 1$ ), show that the slow flow approximation leads to

$$\nabla^4 \psi = 0,$$

and by separating the variables as  $\psi = f(r) \sin \theta$  show that

$$f = \frac{A}{r} + Br + Cr \log r + Dr^3.$$

- (c) Write down the boundary conditions which  $f$  must satisfy at  $r = 1$  and show that if  $f$  satisfies these conditions then  $\psi$  cannot approach the free stream at infinity. Explain, without detailed calculations, how this paradox is resolved. Given that the resolution of the paradox leads to  $C = 1/\ln(1/Re)$ ,  $D = 0$ , use the remaining boundary conditions to determine  $A$  and  $B$ .

**Q2 Slow flow past a sphere.** Incompressible Newtonian fluid flows with constant velocity  $U\mathbf{k}$  past a sphere of radius  $a$  whose centre is at the origin of the spherical polar coordinate system  $(r, \theta, \phi)$ .

- (a) Starting from the steady incompressible Navier-Stokes equations with no body forces, explain how the *dimensionless* slow flow approximation

$$(\text{curl})^3 \mathbf{u} = \mathbf{0}, \quad \nabla \cdot \mathbf{u} = 0 \tag{1}$$

can be determined when the Reynolds number is small.

- (b) An axisymmetric solution of (??) can be written as

$$\mathbf{u} = \text{curl} \left( \frac{\psi}{r \sin \theta} \mathbf{e}_\phi \right) = \frac{1}{r^2 \sin \theta} \frac{\partial \psi}{\partial \theta} \mathbf{e}_r - \frac{1}{r \sin \theta} \frac{\partial \psi}{\partial r} \mathbf{e}_\theta,$$

where  $\mathbf{e}_r$ ,  $\mathbf{e}_\theta$  and  $\mathbf{e}_\phi$  are unit vectors in the  $r$ -,  $\theta$ - and  $\phi$ -directions. Given that

$$\text{curl}^2 \left( \frac{\psi}{r \sin \theta} \mathbf{e}_\phi \right) = -\frac{D^2 \psi}{r \sin \theta} \mathbf{e}_\phi \quad \text{where} \quad D^2 = \frac{\partial^2}{\partial r^2} - \frac{\cot \theta}{r^2} \frac{\partial}{\partial \theta} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2},$$

show that  $\psi$  satisfies

$$D^4 \psi = 0 \text{ for } r > 1; \quad \psi = \frac{\partial \psi}{\partial r} = 0 \text{ on } r = 1; \quad \psi \sim \frac{1}{2} r^2 \sin^2 \theta \text{ as } r \rightarrow \infty.$$

- (c) By separating the variables as  $\psi = f(r) \sin^2 \theta$ , show that

$$\psi = \left( \frac{1}{2} r^2 - \frac{3}{4} r + \frac{1}{4} r^{-1} \right) \sin^2 \theta.$$

**Q3 Lubrication theory for a slider-bearing.** Incompressible Newtonian fluid occupies the thin gap, of thickness  $O(\delta L)$ , between a flat plate  $z = 0$  moving with constant velocity  $U$  in the  $x$ -direction and a stationary rigid surface described by  $z = h(x)$ ,  $0 < x < L$ . There is no gravitational field and the ends of the slider-bearing are held at the ambient pressure  $p_{atm}$ . Assume that the flow is two-dimensional with velocity  $\mathbf{u} = u(x, z)\mathbf{i} + w(x, z)\mathbf{k}$  and pressure  $p(x, z)$ , and governed by the incompressible Navier-Stokes equations with no body forces.

(a) By using the dimensionless variables

$$x^* = \frac{x}{L}, \quad z^* = \frac{z}{\delta L}, \quad h^* = \frac{h}{\delta L}, \quad u^* = \frac{u}{U}, \quad w^* = \frac{w}{\delta U}, \quad p^* = \frac{p - p_{atm}}{\mu U / \delta^2 L},$$

show that the Navier-Stokes equations become (dropping the stars \* on the dimensionless variables)

$$\begin{aligned} \delta^2 Re \left( u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial z} \right) &= -\frac{\partial p}{\partial x} + \delta^2 \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2}, \\ \delta^4 Re \left( u \frac{\partial w}{\partial x} + w \frac{\partial w}{\partial z} \right) &= -\frac{\partial p}{\partial z} + \delta^4 \frac{\partial^2 w}{\partial x^2} + \delta^2 \frac{\partial^2 w}{\partial z^2}, \\ \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} &= 0, \end{aligned}$$

with  $(u, w) = (1, 0)$  on  $z = 0$  and  $(u, w) = (0, 0)$  on  $z = h(x)$  for  $0 < x < 1$ , where  $Re = \rho UL / \mu$ .

(b) Deduce that if  $\delta \ll 1$  and  $\delta^2 Re \ll 1$ , then the lubrication equations

$$\frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial x}, \quad \frac{\partial p}{\partial z} = 0, \quad \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

pertain at leading order. Hence deduce Reynolds equation for  $p(x)$  in the form

$$\frac{d}{dx} \left( h^3 \frac{dp}{dx} \right) = 6 \frac{dh}{dx}.$$

(c) In dimensionless variables a slider bearing has gap thickness  $h(x) = (1 - \lambda x)$  for  $0 < x < 1$  and  $0 < \lambda < 1$ . Calculate the pressure  $p(x)$  within the bearing and show that the total load supported by the bearing per unit length in  $y$  is given by

$$\int_0^1 p(x) dx = \frac{6}{\lambda^2} \left( \log \frac{1}{1 - \lambda} - \frac{2\lambda}{2 - \lambda} \right).$$

**Q4 Injection problem in a Hele-Shaw cell.** In a Hele-Shaw cell, a viscous fluid is injected with velocity  $U$  between two rigid parallel plates which are of lateral extent  $L$  and a fixed distance  $\delta L$  apart. There is no gravitational field.

(a) Starting from the incompressible Navier-Stokes equations with no body forces and the  $z$ -axis normal to the plates, show that, provided  $\delta \ll 1$  and  $\delta^2 \rho UL / \mu \ll 1$ , the flow satisfies at leading order the *dimensional* lubrication equations

$$0 = -\frac{\partial p}{\partial x} + \mu \frac{\partial^2 u}{\partial z^2}, \quad 0 = -\frac{\partial p}{\partial y} + \mu \frac{\partial^2 v}{\partial z^2}, \quad 0 = -\frac{\partial p}{\partial z}, \quad \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0,$$

with  $u = v = w = 0$  on  $z = 0$  and  $z = h$ .

(b) Hence show that, if  $\bar{u}, \bar{v}$  are the *mean* velocities in the  $x$ - and  $y$ -directions respectively, then

$$(\bar{u}, \bar{v}) = -\frac{h^2}{12\mu} \left( \frac{\partial p}{\partial x}, \frac{\partial p}{\partial y} \right) \quad \text{and} \quad \frac{\partial}{\partial x} (h\bar{u}) + \frac{\partial}{\partial y} (h\bar{v}) = 0.$$

Deduce that  $p(x, y)$  satisfies Laplace's equation.

(c) A circular blob of fluid of radius  $R_0$  centred at the origin is at rest within the cell. At  $t = 0$ , a source of constant strength  $Q$  is introduced at the origin so that in the subsequent flow the fluid is contained within a circle of radius  $R(t)$ . What are the boundary conditions on  $p$  and  $\bar{\mathbf{u}} = (\bar{u}, \bar{v})$  on  $r = R(t)$ ?

(d) Show that a possible solution gives

$$R(t) = \sqrt{R_0^2 + \frac{Qt}{\pi h}}$$

and determine the corresponding pressure. Do you expect this solution to be valid for both  $Q > 0$  and  $Q < 0$ ?

**Q5 Gravity-driven flow of a thin film.** A thin two-dimensional sheet of viscous fluid lies on a plate which is at an angle  $\alpha$  to the horizontal. Initially the sheet is of width  $L$  and maximum height  $\delta L$  where  $\delta \ll 1$ , and the fluid flows over the plate under gravity. Choose Cartesian coordinates  $(x, z)$  tangential and normal to the plate respectively, with  $x$  measured down the plate along the line of greatest slope. Denote by  $\mathbf{u} = u(x, z, t)\mathbf{i} + w(x, z, t)\mathbf{k}$  the liquid velocity, by  $p(x, z, t)$  the pressure and by  $z = h(x, t)$  the free surface at which the kinematic and zero stress conditions pertain. The flow is governed by the incompressible Navier-Stokes equations with a body force due solely to the gravitational acceleration  $\mathbf{F} = g(\mathbf{i} \sin \alpha - \mathbf{k} \cos \alpha)$ .

(a) By using the dimensionless variables

$$x^* = \frac{x}{L}, \quad z^* = \frac{z}{\delta L}, \quad h^* = \frac{h}{\delta L}, \quad u^* = \frac{u}{U}, \quad w^* = \frac{w}{\delta U}, \quad t^* = \frac{t}{L/U}, \quad p^* = \frac{p}{\mu U / \delta^2 L},$$

where  $U$  is a representative velocity scale, show that the Navier-Stokes equations become (dropping the stars \* on the dimensionless variables)

$$\begin{aligned} \delta^2 Re \left( \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial z} \right) &= -\frac{\partial p}{\partial x} + \delta^2 \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2} + \frac{\delta^2 \rho g L^2}{\mu U} \sin \alpha, \\ \delta^4 Re \left( \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + w \frac{\partial w}{\partial z} \right) &= -\frac{\partial p}{\partial z} + \delta^4 \frac{\partial^2 w}{\partial x^2} + \delta^2 \frac{\partial^2 w}{\partial z^2} - \frac{\delta^3 \rho g L^2}{\mu U} \cos \alpha, \\ \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} &= 0, \end{aligned}$$

where the Reynolds number  $Re = \rho U L / \mu$ .

(b) Show that the stress tensor is given by

$$\sigma_{11} \sim \sigma_{33} \sim -\frac{\mu U}{\delta^2 L} p, \quad \sigma_{13} = \sigma_{31} \sim \frac{\mu U}{\delta L} \frac{\partial u}{\partial z} \quad \text{as } \delta \rightarrow 0$$

(c) If the plate angle  $\alpha = O(1)$  as  $\delta \rightarrow 0$ , show that, in the thin-film regime in which  $\delta \ll 1$  and  $\delta^2 Re \ll 1$ , an appropriate velocity scale is  $U = \delta^2 \rho g L^2 \sin \alpha / \mu$  and at leading order the lubrication equations

$$0 = -\frac{\partial p}{\partial x} + \frac{\partial^2 u}{\partial z^2} + 1, \quad 0 = -\frac{\partial p}{\partial z}, \quad \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

pertain, with

$$u = w = 0 \quad \text{on } z = 0,$$

and

$$p = \frac{\partial u}{\partial z} = 0, \quad w = \frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x} \quad \text{on } z = h(x, t).$$

Hence show  $h(x, t)$  satisfies the equation

$$\frac{\partial h}{\partial t} + h^2 \frac{\partial h}{\partial x} = 0.$$

Verify that  $h = f(x - h^2 t)$  solves this equation, so that particular values of  $h$  propagate down the plate with speed proportional to  $h^2$ . Draw rough sketches of the evolution with time of the initial profile  $h(x, 0) = \exp(-x^2)$ .

(d) If the plate is horizontal (*i.e.*  $\alpha = 0$ ), show that an appropriate velocity scale is  $U = \delta^3 \rho g L^2 / \mu$  and that lubrication theory leads in this case to the thin-film equation

$$\frac{\partial h}{\partial t} = \frac{\partial}{\partial x} \left( \frac{h^3}{3} \frac{\partial h}{\partial x} \right).$$