

## Consultation session questions

- A quick question about supersonic flow past a thin wing. On page 60 of the notes, where we're finding the value of  $\phi$  in each of the 6 regions, in regions 3 and 6, is  $\phi$  supposed to be 0 or a constant (so that we have continuity between regions 2 and 3, 5 and 6)? The notes say that  $\phi$  should be 0 (so that they are zones of silence) but in the lectures, you imposed continuity so that  $\phi$  are non-zero constants instead, so I was just wondering which one I should use? Can we still say that there are zones of silence if  $\phi$  is non-zero?
- 2012 Q1(b)(iv) Could you talk through whether the waves are dispersive?
- 2012 Q2(b) Could you just talk through how to apply FT for this question?
- 2021 Q3(c)(ii) Unsure of how to approach this part!!
- 2013 Q1(c) Could you talk through the BCs we need to apply here?
- 2013 Q2(a)(iii) Could you just quickly cover region of silence?
- ✓ 2013 Q2(b) I think I got the correct BCs and solution, but could I perhaps check these?
- 2013 Q2(c)(ii) Less sure on this part. Behaviour changes at  $y=0$  but not sure what this means!
- 2016 Q3(b) Why must the fluid depths and velocities satisfy these relations to the left and the right of  $x = Vt$ ? How come the shock / expansion fan doesn't at  $x = bt$  doesn't get in the way? Why do we know that the shock is a straight line?
- 2017 Q2(c,d) Please could you go over them.
- 2017 Q3(c) Please could you go over it.
- 2014 Q1(c) We will end up with  $AJ_0 + BY_0$  as our solution, but could you just discuss the BCs we need here?
- 2014 Q3(d) Not quite sure how to combine previous parts? Was happy with all previous parts however.
- 2017 Q1(c) I'd much appreciate if we could go through the computations.
- ✓ 2017 Q1(c) Is contour integration examinable? *Yes but very unlikely!*
- ✓ 2014 Q3(d) Please can we go through the sketches.
- ✓ 2015 Q2(c), Q3(b) and Q3(c) Please can we go through the sketches.

1. The flow of a stratified incompressible fluid with density  $\rho$ , velocity  $\mathbf{u}$  and pressure  $p$  is governed by

$$\frac{\partial \rho}{\partial t} + (\mathbf{u} \cdot \nabla) \rho = 0, \quad \nabla \cdot \mathbf{u} = 0, \quad \rho \left( \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right) = -\nabla p - \rho g \mathbf{k},$$

where  $g$  the acceleration due to gravity.

- (a) [7 marks] (i) Determine the pressure  $p = p_0(z)$  in the stationary state in which the fluid is at rest with density  $\rho_0(z) = \rho_a e^{-\beta z}$  and  $p = p_a$  on  $z = 0$ , where  $\rho_a > 0$ ,  $\beta$  and  $p_a$  are constants.
- (ii) Small amplitude waves perturb the stationary state so that  $\rho = \rho_0(z) + \rho'$ ,  $p = p_0(z) + p'$  and  $\mathbf{u} = u'\mathbf{i} + v'\mathbf{j} + w'\mathbf{k}$ , where the primed variables are small. Write down the linearized versions of the governing equations and deduce that  $w'$  satisfies

$$\frac{\partial^2}{\partial t^2} \left( \frac{\partial^2 w'}{\partial x^2} + \frac{\partial^2 w'}{\partial y^2} + \frac{\partial^2 w'}{\partial z^2} \right) = -\beta g \left( \frac{\partial^2 w'}{\partial x^2} + \frac{\partial^2 w'}{\partial y^2} - \frac{1}{g} \frac{\partial^3 w'}{\partial z \partial t^2} \right). \quad (\star)$$

- (b) [6 marks] Suppose that the flow is two dimensional and gravity dominated with the fluid occupying the channel  $x > 0$ ,  $0 < z < h$  between rigid walls at  $z = 0$  and  $z = h$ , so that  $w'(x, z, t)$  is governed by

$$\frac{\partial^2}{\partial t^2} \left( \frac{\partial^2 w'}{\partial x^2} + \frac{\partial^2 w'}{\partial z^2} \right) = -\beta g \frac{\partial^2 w'}{\partial x^2} \quad \text{for } x > 0, 0 < z < h,$$

with  $w' = 0$  on  $z = 0, h$  for  $x > 0$ . A wave-maker at  $x = 0$  disturbs the fluid such that

$$w' = a e^{-i\Omega t} \sin\left(\frac{\pi z}{h}\right) \quad \text{on } x = 0, 0 < z < h,$$

where  $a$  and  $\Omega > 0$  are constants. By imposing as  $x \rightarrow \infty$  either boundedness of  $w'$  or a radiation condition on  $w'$ , as appropriate, solve for  $w'$  when (i)  $\Omega^2 > \beta g$  and (ii)  $\Omega^2 < \beta g$ .

- (c) [12 marks] Now suppose that the flow is three dimensional with  $\mathbf{u} = u\mathbf{i} + v\mathbf{j} + w\mathbf{k}$  below a free surface at  $z = \eta(x, y, t)$  on which

$$w = \frac{\partial \eta}{\partial t} + u \frac{\partial \eta}{\partial x} + v \frac{\partial \eta}{\partial y}, \quad p - p_a = -\gamma \kappa,$$

where  $\gamma$  is the surface tension and  $\kappa$  is the curvature. The primed variables and  $\eta$  are small, so that  $w'(x, y, z, t)$  is governed by  $(\star)$  for  $z < 0$ .

- (i) Assuming that  $\kappa = \nabla^2 \eta$  after linearization for small  $\eta$ , derive the linearized boundary condition

$$\rho_a \frac{\partial^3 w'}{\partial z \partial t^2} = \rho_a g \left( \frac{\partial^2 w'}{\partial x^2} + \frac{\partial^2 w'}{\partial y^2} \right) - \gamma \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)^2 w' \quad \text{on } z = 0.$$

- (ii) Show that there are waves of the form

$$w' = A \exp(i(kx \cos \alpha + ky \sin \alpha - \omega t) + \lambda z)$$

with  $A$ ,  $k$ ,  $\alpha$ ,  $\omega$  and  $\lambda$  being constant and  $\text{Re}(\lambda) \geq 0$  only if the frequency  $\omega$  is such that  $\omega^2$  is a function of the wavenumber  $k$  that you should determine.

2020/BS.4/Q1

(a)(i) All equations satisfied with  $\underline{u} = \underline{0}$ ,  $\rho_0 = \rho_a e^{-\beta z}$ ,  $p = p_0(z)$  provided  $\nabla p_0 = -\rho_0 g \underline{k}$  in  $z < 0$  with  $p_0 = p_a$  on  $z = 0$ .

[B2] Hence,  $p_0(z) = p_a - \int_0^z \rho_0(s) g ds = p_a + \frac{\rho_a g}{\beta} (e^{-\beta z} - 1)$ .

(a)(ii) The linearized PDEs are (with  $\underline{u}' = u' \underline{i} + v' \underline{j} + w' \underline{k}$ )

$$\rho'_t + w' \frac{d\rho_0}{dz} \quad (1), \quad \nabla \cdot \underline{u}' = 0 \quad (2), \quad \rho_0 \underline{u}'_t = -\nabla p' - \rho' g \underline{k} \quad (3)$$

Eliminate  $u'$  &  $v'$ :  $p'_{xx} + p'_{yy} = -\rho_0 u'_t x - \rho_0 v'_t y \quad (\text{by } (3))$

$$= \rho_0 w'_{zt} \quad (\text{by } (2))$$

Since  $\frac{d\rho_0}{dz} = -\beta \rho_0$ , we are left with

$$\rho'_t = \beta \rho_0 w' \quad (4), \quad p'_{xx} + p'_{yy} = \rho_0 w'_{zt} \quad (5), \quad \rho_0 w'_t = -p'_z - \rho' g \quad (6)$$

Now eliminate  $\rho'$  and  $p'$ :

$$\begin{aligned} (\rho_0 w'_{zt})_{zt} &= (\partial_x^2 + \partial_y^2) p'_{zt} \quad (\text{by } (5)) \\ &= (\partial_x^2 + \partial_y^2) (-\rho_0 w'_{tt} - \rho'_t g) \quad (\text{by } (6)) \end{aligned}$$

$$\Rightarrow \rho_0 w'_{zztt} + \frac{d\rho_0}{dz} w'_{ztt} = (\partial_x^2 + \partial_y^2) (-\rho_0 w'_{tt} - \beta g \rho_0 w')$$

$$\Rightarrow (w'_{xx} + w'_{yy} + w'_{zz})_{tt} = -\beta g (w'_{xx} + w'_{yy} - \frac{1}{g} w'_{zzt}) \quad (*)$$

(as  $\frac{d\rho_0}{dz} = -\beta \rho_0$ )

[B5]

$$(b) \quad w' = e^{-i\omega t} f(x) \sin\left(\frac{\pi z}{h}\right) \Rightarrow (-i\omega)^2 \left(f'' - \frac{\pi^2}{h^2} f\right) = -\beta g f''$$

$$\text{or } f'' + \frac{\pi^2}{h^2 \left(\frac{\beta g}{\omega^2} - 1\right)} f = 0 \quad \text{for } \omega > 0 \text{ and } \omega^2 \neq \beta g.$$

$$(i) \underline{\kappa^2 > \beta g} \Rightarrow f'' - \omega^2 f = 0, \quad \omega = \frac{\pi}{h(1 - \frac{\beta g}{\kappa^2})^{1/2}} > 0$$

$$\Rightarrow f = A e^{\omega x} + B e^{-\omega x} \quad (A, B \in \mathbb{C} \text{ arb.})$$

$$BC \text{ on } x=0 \text{ \& } \omega' \text{ odd at } \infty \Rightarrow f(0)=a, |f(\infty)| < \infty \Rightarrow A=0, B=a$$

$$\text{Hence, } \omega' = a e^{-i\omega t - \omega x} \sin\left(\frac{\pi z}{h}\right), \quad \omega \text{ as above.}$$

$$(ii) \underline{\kappa^2 < \beta g} \Rightarrow f'' + \mu^2 f = 0, \quad \mu = \frac{\pi}{h(\frac{\beta g}{\kappa^2} - 1)^{1/2}} > 0$$

$$\Rightarrow f = A e^{i\mu x} + B e^{-i\mu x} \quad (A, B \in \mathbb{C} \text{ arb.})$$

$$\text{Hence, } \omega' = (A e^{i(\mu x - \omega t)} + B e^{-i(\mu x + \omega t)}) \sin\left(\frac{\pi z}{h}\right)$$

$$BC \text{ on } x=0 \text{ \& radiation condition} \Rightarrow f(0)=a, B=0$$

(no inward waves)

$$[56] \quad \text{Hence } \omega' = a e^{i(\mu x - \omega t)} \sin\left(\frac{\pi z}{h}\right), \quad \mu \text{ as above}$$

$$(c)(i) \quad BCs \Rightarrow \omega' = u'_t + v'_x + w'_y, \quad p'_0(\eta) - p'_a + p' = -\gamma \eta \text{ on } z=\eta.$$

For small  $\eta$ , Taylor's Theorem gives

$$\omega'|_{z=\eta} = \omega'|_{z=0} + \eta \omega'_z|_{z=0} + \text{h.o.t.}$$

$$p'_0(\eta) = p'_0(0) + \eta \frac{dp'_0}{dz}(0) + \text{h.o.t.}$$

and similarly for  $u', v'$  and  $p'$ . Hence, the linearized BCs are

$$\omega' \Big|_{\textcircled{7}} = u'_t \Big|_{\textcircled{7}}, \quad p' \Big|_{\textcircled{8}} = (\rho_a g \eta - \gamma(\eta x + \eta y)) \text{ on } z=0$$

where we used the fact  $\nabla \cdot \mathbf{u} = \nabla^2 \eta$  after linearizing for small  $\eta$  and  $p'_0(0) = p_a$ ,  $\frac{dp'_0}{dz}(0) = -p'_0(0)g = -\rho_a g$ .

Eliminate  $n$  &  $p'$  :

$$(+1) \quad \rho_a \omega'_{ztt} = (\partial_x^2 + \partial_y^2) p'_t \quad (\text{by } \textcircled{5} \text{ on } z=0)$$

$$(+1) \quad = \rho_a g (\partial_x^2 + \partial_y^2) (n_t - \Gamma (\partial_x^2 + \partial_y^2) n_t) \quad (\text{by } \textcircled{6}, \Gamma = \frac{\sigma}{\rho_a g})$$

$$(+1) \quad = \rho_a g (\partial_x^2 + \partial_y^2) (\omega' - \Gamma (\partial_x^2 + \partial_y^2) \omega') \quad (\text{by } \textcircled{7})$$

$$[S/N6] \text{ giving } \rho_a \omega'_{ztt} \underset{**}{=} \rho_a g (\partial_x^2 + \partial_y^2) \omega' - \gamma (\partial_x^2 + \partial_y^2)^2 \omega' \text{ on } z=0$$

$$(c)(ii) \text{ Substituting } \omega' = A \exp \{ i k \cos \alpha x + i k \sin \alpha y - i \omega t + \lambda z \},$$

$$\textcircled{*} \Rightarrow (-i\omega)^2 ((ik \cos \alpha)^2 + (ik \sin \alpha)^2 + \lambda^2) = -\beta g ((ik \cos \alpha)^2 + (ik \sin \alpha)^2 - \frac{\lambda(-i\omega)^2}{g})$$

$$\textcircled{**} \Rightarrow \frac{1}{g} \lambda (-i\omega)^2 = (ik \cos \alpha)^2 + (ik \sin \alpha)^2 - \Gamma ((ik \cos \alpha)^2 + (ik \sin \alpha)^2)^2$$

$$+2 \quad \text{Hence, } \omega^2 (k^2 - \lambda^2 + \beta \lambda) = \beta g k^2, \quad \lambda \omega^2 \underset{\oplus}{=} g k^2 (1 + \Gamma k^2)$$

$$\text{Eliminate } \omega^2 : (1 + \Gamma k^2)(k^2 - \lambda^2 + \beta \lambda) = \beta \lambda$$

$$\Rightarrow \lambda^2 - \frac{\beta \Gamma k^2}{1 + \Gamma k^2} \lambda - k^2 = 0, \quad 2\lambda \underset{\oplus}{=} \frac{\beta \Gamma k^2 \pm ((\beta \Gamma k^2)^2 + 4(1 + \Gamma k^2)k^2)^{1/2}}{1 + \Gamma k^2}$$

But only the +ve root is admissible for  $\text{Re}(\lambda) \geq 0$ ,  
so that  $\textcircled{\oplus}$  and  $\textcircled{\#}$  give the dispersion relation

$$\left\{ \beta \Gamma |k| + (4(1 + \Gamma k^2)^2 + \beta^2 \Gamma^2 k^2)^{1/2} \right\} \omega^2 = 2g |k| (1 + \Gamma k^2)^2,$$

[N6] where we divided through by  $|k| = \sqrt{k^2}$ .

$$+2 \quad \text{Thus, } \omega^2 = \frac{2g |k| (1 + \Gamma k^2)^2}{\beta \Gamma |k| + (4(1 + \Gamma k^2)^2 + \beta^2 \Gamma^2 k^2)^{1/2}}$$

$$[N156] \text{ where } \Gamma = \frac{\sigma}{\rho_a g}.$$

2. (a) [10 marks] Small-amplitude waves disturb a barotropic gas contained in a two-dimensional rectangular pipe between rigid walls at  $x = 0$ ,  $x = a$  and free ends at  $y = 0$ ,  $y = b$  maintained at constant pressure  $p_0$ . You may assume that the linearized equations for the potential  $\phi(x, y, t)$  for the velocity perturbations and for the pressure  $p(x, y, t)$  are given by

$$\frac{\partial^2 \phi}{\partial t^2} = c_0^2 \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} \right), \quad p = p_0 - \rho_0 \frac{\partial \phi}{\partial t}$$

in  $0 < x < a$ ,  $0 < y < b$ , where the sound speed  $c_0$  and undisturbed density  $\rho_0$  are constant.

- (i) State the boundary conditions for  $\phi$  on the boundary of the pipe.
  - (ii) By seeking a separable solution of the form  $\phi = e^{-i\omega t} F(x) G(y)$ , find the normal modes and the natural frequencies  $\omega$ .
- (b) [15 marks] Small deflections  $\eta(x, t)$  of an elastic beam lying on a shallow water layer satisfy the equation

$$\frac{\partial^2 \eta}{\partial t^2} = \beta^2 \frac{\partial^6 \eta}{\partial x^6} \quad \text{for} \quad -\infty < x < \infty, \quad t > 0,$$

where  $\beta$  is a positive constant. The beam is released from rest such that

$$\eta(x, 0) = \frac{\alpha}{\epsilon \sqrt{\pi}} e^{-x^2/\epsilon^2}, \quad \frac{\partial \eta}{\partial t}(x, 0) = 0 \quad \text{for} \quad -\infty < x < \infty,$$

where  $\alpha$  and  $\epsilon$  are positive constants.

- (i) Show that the solution may be written in the form

$$\eta(x, t) = \int_{-\infty}^{\infty} F(k) \cos(\omega(k)t) e^{ikx} dk,$$

where the function  $F(k)$  should be defined and  $\omega(k) = \beta|k|^3$ .

[You may assume that the Fourier transform of  $e^{-x^2/\epsilon^2}$  is  $\epsilon\sqrt{\pi}e^{-\epsilon^2 k^2/4}$ .]

- (ii) Use the method of stationary phase to show that if  $\epsilon$  is sufficiently small then

$$\eta(x, t) \sim \frac{A}{(xt)^{1/4}} \cos\left(\frac{Bx^{3/2}}{t^{1/2}} - \frac{\pi}{4}\right)$$

as  $x, t \rightarrow +\infty$  with  $x/t$  held constant, where the constants  $A$  and  $B$  should be determined.

[You may assume that if  $f(k)$  and  $\psi(k)$  are sufficiently well behaved, and  $\psi(k)$  is real-valued and such that  $\psi'(k)$  has a single zero at  $k_*$ , then

$$\int_{-\infty}^{\infty} f(k) e^{i\psi(k)t} dk \sim f(k_*) e^{i(\psi(k_*)t \pm \pi/4)} \sqrt{\frac{2\pi}{|\psi''(k_*)|t}} \quad \text{as} \quad t \rightarrow \infty,$$

where the  $\pm$  takes the sign of  $\psi''(k_*)$ .]

2020/BS.4/Q2

(a)(i) No normal flow through rigid walls  $\Rightarrow \phi_x = 0$  on  $x=0, a$ .

Since  $p = p_0 - \rho_0 \phi_t$ , the condition of constant pressure  $p_0$  in the free ends  $\Rightarrow \phi_t = 0$  on  $y=0, b$ .

(a)(ii) Seek nontrivial separable solution  $\phi = e^{-i\omega t} F(x) G(y)$ .

Wave equation  $\Rightarrow -\frac{\omega^2}{c_0^2} = \frac{F''(x)}{F(x)} = \frac{G''(y)}{G(y)}$  ( $FG \neq 0$ )

LHS ind.  $y$  & RHS ind.  $x \Rightarrow$  LHS = RHS ind.  $x$  &  $y$  and hence constant.

Hence,  $\frac{F''}{F} = -\lambda^2$ ,  $\frac{G''}{G} = -\mu^2$ ,  $\omega^2 = c_0^2(\lambda^2 + \mu^2)$ ,

where  $\lambda, \mu \in \mathbb{R}$  and the signs of the constants have been chosen to give the oscillatory solutions required for nontrivial solutions for which the BCs in (a)(i) require  $F'(0) = F'(a) = 0$ ,  $G(0) = G(b) = 0$ .

For  $\lambda = 0$ ,  $F = \text{constant}$ , but for  $\lambda \neq 0$ ,  $F = A \cosh \lambda x + B \sinh \lambda x$  ( $A, B \in \mathbb{C} \text{ arb.}$ ), so BCs  $\Rightarrow B = 0$  and  $\lambda a = m\pi$  with  $m \in \mathbb{Z} \setminus \{0\}$ . Combo  $\Rightarrow F \propto \cos\left(\frac{m\pi x}{a}\right)$ ,  $\lambda = \frac{m\pi}{a}$ ,  $m \in \mathbb{Z}$ .

For  $\mu = 0$ ,  $G = 0$ , but for  $\mu \neq 0$ ,  $G = C \cosh \mu y + D \sinh \mu y$  ( $C, D \in \mathbb{R} \text{ arb.}$ ), so BCs  $\Rightarrow C = 0$ ,  $\mu b = n\pi$  with  $n \in \mathbb{Z} \setminus \{0\}$ . Hence,  $G \propto \sin\left(\frac{n\pi y}{b}\right)$ ,  $\mu = \frac{n\pi}{b}$ ,  $n \in \mathbb{Z} \setminus \{0\}$ .

Combo  $\Rightarrow$  normal modes are  $\phi = E e^{-i\omega t} \cos\left(\frac{m\pi x}{a}\right) \sin\left(\frac{n\pi y}{b}\right)$  ( $E \in \mathbb{C} \text{ arb.}$ ) with natural frequencies  $\omega$  s.t.

$\omega^2 = c_0^2 \pi^2 \left( \frac{m^2}{a^2} + \frac{n^2}{b^2} \right)$  for  $m \in \mathbb{Z}$ ,  $n \in \mathbb{Z} \setminus \{0\}$ .

(b)(i) Fourier transform in  $x$ :  $\hat{u}(k, t) = \int_{-\infty}^{\infty} u(x, t) e^{-ikx} dx$ .

$$\text{PDE} \Rightarrow \hat{u}_{tt} = \beta^2 (ik)^6 \hat{u} = -\beta^2 k^6 \hat{u} \text{ for } t > 0.$$

+3  
(hint)  $\text{ICs} \Rightarrow \hat{u} = \alpha e^{-\varepsilon^2 k^2/4}, \hat{u}_t = 0 \text{ at } t=0.$

Hence,  $\hat{u}(k, t) = A(k) \cos(\omega(k)t) + B(k) \sin(\omega(k)t)$ ,  
where  $A(k), B(k)$  are arbitrary and  $\omega^2 = \beta^2 k^6$ ,  
so that  $\omega(k) = \beta |k|^3$  wlog.

+2  
 $\text{ICs} \Rightarrow A(k) = \alpha e^{-\varepsilon^2 k^2/4}, B(k) = 0.$

Inverse Fourier transform  $u(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{u}(k, t) e^{ikx} dk$ .

Hence,  $u(x, t) = \int_{-\infty}^{\infty} F(k) \cos(\omega(k)t) e^{ikx} dk,$

+2  
[56] where  $F(k) = \frac{\alpha}{2\pi} e^{-\varepsilon^2 k^2/4}$  and  $\omega(k) = \beta |k|^3$ .

(b)(ii) Let  $\frac{x}{t} = V = O(1)$  as  $x, t \rightarrow +\infty$  and use  $\cos(\omega t) = \frac{e^{-i\omega t} + e^{i\omega t}}{2}$

$\Rightarrow u(Vt, t) = \int_{-\infty}^{\infty} \frac{1}{2} F(k) (e^{-i\omega t} + e^{i\omega t}) e^{ikVt} dk$

$\Rightarrow u(Vt, t) = \frac{1}{2} (I_+(t) + I_-(t)), \text{ where}$

$$I_{\pm}(t) = \int_{-\infty}^{\infty} F(k) e^{i\psi_{\pm}(k)t} dk,$$

+2  
 $\psi_{\pm}(t) = kV \mp \omega(k).$

[B2] Can now apply the method of stationary phase to  $I_{\pm}(t)$ .

The main contribution to  $I_{\pm}(t)$  as  $t \rightarrow +\infty$  comes  
from wavenumbers  $k = k_{\pm}^*$ , where the phase  $\psi_{\pm}(k)$   
is stationary, i.e.  $\psi'_{\pm}(k_{\pm}^*) = 0$ .

Calculate:  $\omega = \beta |k|^3 \Rightarrow \omega'(k) = 3\beta k|k|, \omega''(k) = 6\beta |k|$ .

Hence  $\psi_{\pm}'(k_{\pm}^{\pm}) = 0 \Rightarrow V \mp \omega'(k_{\pm}^{\pm}) = 0 \Rightarrow 3\beta k_{\pm}^{\pm} |k_{\pm}^{\pm}| = \pm V$ ,  
giving the critical wavenumbers  $k_{\pm}^{\pm} = \pm \left(\frac{V}{3\beta}\right)^{1/2}$

These are each simple zeros because  $\psi_{\pm}''(k_{\pm}^{\pm}) = \pm 6\beta |k_{\pm}^{\pm}| \neq 0$  and  $\psi_{\pm}$  is twice continuously diff, while  $F(k)$  is  $\infty$  diff and decays exponentially rapidly as  $k \rightarrow \pm\infty$ , so hint applies giving

$$I_{\pm}(t) \sim F(k_{\pm}^{\pm}) \exp\left\{i\left(\psi_{\pm}(k_{\pm}^{\pm})t \mp \frac{\pi}{4}\right)\right\} \left(\frac{2\pi}{|\psi_{\pm}'(k_{\pm}^{\pm})|t}\right)^{1/2}$$

as  $t \rightarrow \infty$  because  $\text{sgn}(\psi_{\pm}''(k_{\pm}^{\pm})) = \mp 1$

Calculate:  $F(k_{\pm}^{\pm}) = \frac{\alpha}{2\pi} e^{-\varepsilon^2 V^2 / 12\beta}$

$$\psi_{\pm}(k_{\pm}^{\pm}) = \pm \frac{V^{3/2}}{(3\beta)^{1/2}} \mp \beta \left|\frac{V^{1/2}}{(3\beta)^{1/2}}\right|^3 = \pm \frac{2V^{3/2}}{3(3\beta)^{1/2}}$$

$$|\psi_{\pm}''(k_{\pm}^{\pm})| = 6\beta \left(\frac{V}{3\beta}\right)^{1/2} = 2(3\beta V)^{1/2}$$

Hence,  $I_{\pm}(t) \sim \frac{\alpha}{2\pi} e^{-\varepsilon^2 V^2 / 12\beta} \exp\left\{\pm i\left(\frac{2V^{3/2}t}{3(3\beta)^{1/2}} - \frac{\pi}{4}\right)\right\} \left(\frac{2\pi}{2(3\beta V)^{1/2}t}\right)^{1/2}$

as  $t \rightarrow \infty$ , giving

$$n(Vt, t) \sim \frac{2e^{-\varepsilon^2 V^2 / 12\beta}}{(4\pi(3\beta V)^{1/2}t)^{1/2}} \cos\left(\frac{2V^{3/2}t}{3(3\beta)^{1/2}} - \frac{\pi}{4}\right)$$

Finally,  $e^{-\varepsilon^2 V^2 / 12\beta} \sim 1$  for  $\varepsilon$  sufficiently small and replace  $V$  with  $x/t$  elsewhere to obtain

$$n(x, t) \sim \frac{A}{(x/t)^{1/4}} \cos\left(\frac{2x^{3/2}}{3(3\beta t)^{1/2}} - \frac{\pi}{4}\right)$$

[N/S7] as  $x, t \rightarrow +\infty$  with  $\frac{x}{t} = O(1)$ , where  $A = \frac{\alpha}{(4\pi)^{1/2}(3\beta)^{1/4}}$ .

3. (a) [12 marks] Shallow water of uniform depth  $h_0$  is held at rest in  $x < 0$  by a dam at  $x = 0$ . The dam is suddenly removed at time  $t = 0$ , so that the water flows into  $x > 0$  forming a shallow layer of depth  $h(x, t)$  and horizontal fluid velocity  $u(x, t)$  under the action of gravity with acceleration  $g$ . You may assume that the *Riemann invariants*  $u \pm 2c$  are conserved along *characteristics* satisfying  $dx/dt = u \pm c$ , where the wave speed  $c = \sqrt{gh}$ .

(i) Show that

$$u = 0, \quad c = c_0 \quad \text{for} \quad x < -c_0 t, \quad t > 0,$$

where  $c_0 = \sqrt{gh_0}$ . Derive the solution given by

$$u = \frac{2}{3} \left( c_0 + \frac{x}{t} \right), \quad c = \frac{1}{3} \left( 2c_0 - \frac{x}{t} \right) \quad \text{for} \quad -c_0 t < x < 2c_0 t, \quad t > 0,$$

explaining why it is not valid for  $x > 2c_0 t, t > 0$ .

(ii) Find the time taken by a fluid element initially at  $x = -a < 0$  to reach  $x = 0$ .

- (b) [13 marks] Now suppose that shallow water of uniform depth  $h_0$  is held at rest in  $x > 0$  by a dam at  $x = 0$ . At time  $t = 0$  the dam suddenly starts to move into the water and to leak, so that  $h(u - U) = -\lambda h^2$  on the dam at  $x = Ut$  for  $t > 0$ , where  $U$  and  $\lambda$  are positive constants. Suppose that the flow separates into a region of uniform velocity and uniform depth  $\beta h_0$  in  $Ut < x < Vt$  and a stationary region of uniform depth  $h_0$  in  $x > Vt$ , with a shock at  $x = Vt$  moving at constant speed  $V$ . You may assume the *Rankine-Hugoniot conditions*,

$$[h(u - V)]_{-}^{+} = 0, \quad \left[ h(u - V)^2 + \frac{gh^2}{2} \right]_{-}^{+} = 0,$$

where  $[ ]_{-}^{+}$  denotes the change in the quantity from one side of the shock to the other.

(i) Find the shock speed  $V$  in terms of  $\beta$  and  $c_0 = \sqrt{gh_0}$ , and deduce that

$$\frac{(\beta - 1)\sqrt{\beta + 1}}{\sqrt{2}\beta} = \frac{U}{c_0} - \frac{\lambda h_0}{c_0} \beta.$$

Using a diagram explain why this equation has a unique positive root for  $\beta$ .

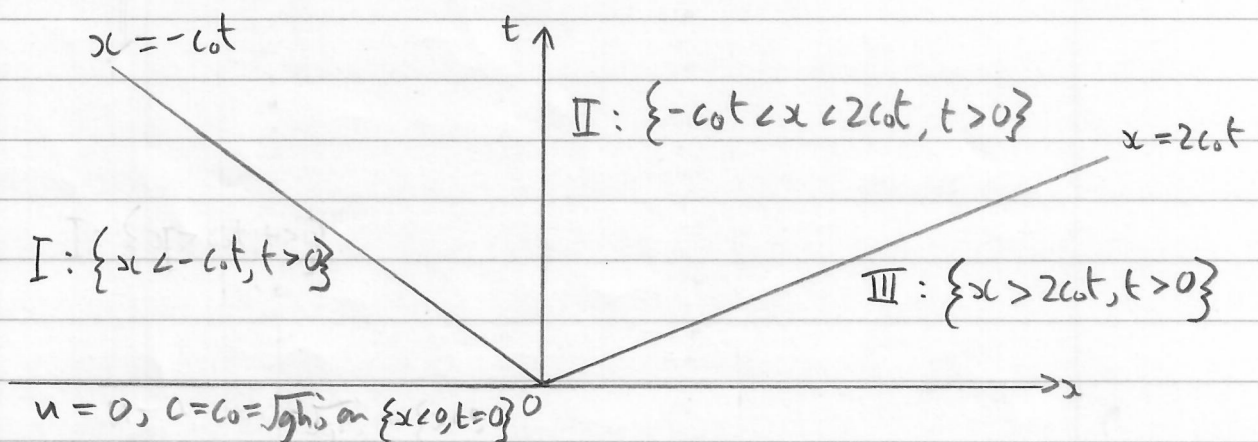
- (ii) Show from first principles that the net rate at which energy flows out of the moving shock is given by

$$\rho g h_0^2 V q(\beta),$$

where  $\rho$  is the density and  $q(\beta)$  is a function of  $\beta$  that you should determine. Hence explain why the condition  $U > \lambda h_0$  is necessary for the shock to be physical.

B5.4/2020/Q3

(a)(i)



Region I: Where  $C_+$  char<sup>s</sup> from  $\{x < 0, t = 0\}$  intersect,  $u \pm 2c = \pm 2c_0 \Rightarrow u = 0, c = c_0$ . Hence such  $C_+$  char<sup>s</sup> are straight lines with  $dx/dt = \pm c_0$  and therefore map out  $x < -c_0 t, t > 0$ , i.e.  $u = 0, c = c_0$  in region I.

Region II: Where a  $C_-$  char<sup>s</sup> intersects the family of  $C_+$  char<sup>s</sup> from  $\{x < 0, t = 0\}$ , we have  $u - 2c = \text{const.}$  and  $u + 2c = 2c_0$  on the  $C_-$  char<sup>s</sup>; hence  $u$  and  $c$  are constant on it and it is therefore straight. To avoid it crossing other  $C_-$  char<sup>s</sup> in regions I and II, it must originate from the origin and therefore have slope  $x/t = u - c$ . Solving  $u + 2c = 2c_0, u - c = x/t$  gives  $u = \frac{2}{3}(c_0 + x/t)$  and  $c = \frac{1}{3}(2c_0 - x/t)$  in region II, which therefore maps out  $-c_0 t < x < 2c_0 t, t > 0$  because we require  $c, h \geq 0$ , i.e. expansion fan terminates on  $x = 2c_0 t$  where  $c = h = 0$ .

[B/55] Region III:  $u$  and  $c$  undefined as there is no water.

(a)(ii) The fluid element at  $x = -a < 0$  at  $t = 0$  moves with the flow according to the ODE

$$\frac{dx}{dt} = u(x, t) = \begin{cases} 0 & \text{for } x < -c_0 t, t > 0, \\ \frac{2}{3}(c_0 + \frac{x}{t}) & \text{for } -c_0 t < x < 2c_0 t, t > 0. \end{cases}$$

Hence the element does not move with  $x = -a$  until  $t = a/c_0$ . After this it moves according to

$$\frac{dx}{dt} - \frac{2}{3t}x = \frac{2}{3}c_0 \Rightarrow \frac{d}{dt}\left(\frac{x}{t^{2/3}}\right) = \frac{2c_0}{3t^{4/3}}$$

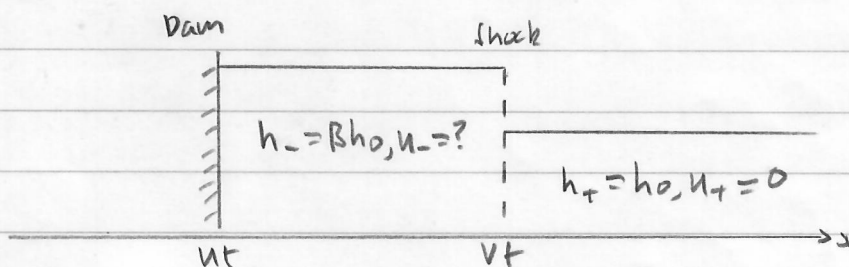
with  $x = -a$  at  $t = a/c_0$ ; thus  $\frac{x}{t^{2/3}} = 2c_0 t^{1/3} + A$

where  $-a\left(\frac{c_0}{a}\right)^{2/3} = 2c_0\left(\frac{a}{c_0}\right)^{1/3} + A$ , giving  $A = -3a^{1/3}c_0^{2/3}$ .

[N5] The element therefore reaches the origin at time  $t = t_c$  where  $0 = 2c_0 t_c^{1/3} + A \Rightarrow t_c^{1/3} = -A/2c_0 \Rightarrow t_c = \frac{27a}{8c_0}$ .

~~(b)(i) The BC on the dam says that the mass flux of water lost through the dam, i.e.  $-p h(u-u)|_{x=ut}$  where  $p$  is density, is proportional to the force exerted by the water on the dam, i.e.  $\int_0^h p - p_{atm} dz = \int_0^h \rho g z dz \times h^2$ .~~

(b)(i)



Rankine-Hugoniot conditions give

$$B h_0 (u_- - v) = -h_0 v, \quad B h_0 (u_- - v)^2 + \frac{1}{2} g B^2 h_0^2 = h_0 v^2 + \frac{1}{2} g h_0^2$$

$$\Rightarrow u_- - v = -\frac{v}{B}, \quad B\left(-\frac{v}{B}\right)^2 + \frac{1}{2} g B^2 h_0 = v^2 + \frac{1}{2} g h_0$$

$$\Rightarrow u_- = \left(1 - \frac{1}{B}\right)v, \quad v^2\left(1 - \frac{1}{B}\right) = \frac{1}{2} c_0^2 (B^2 - 1)$$

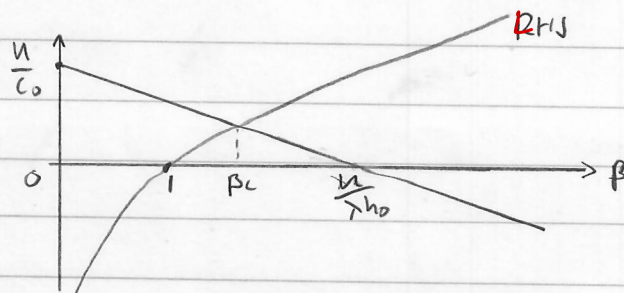
[B/S2] Since we're assuming there is a shock  $B \neq 1$  and  $v > u > 0$ , so taking +ve root gives  $v = \frac{c_0}{2^{1/2}} B^{1/2} (B+1)^{1/2}$

The BC on the dam implies  $u_- - U = -\lambda h_-$ , giving

$$U - \lambda \beta h_0 = u_- = \frac{\beta-1}{\beta} V = c_0 \frac{(\beta-1)(\beta+1)^{1/2}}{(2\beta)^{1/2}}$$

$$\text{i.e. } \frac{(\beta-1)(\beta+1)^{1/2}}{(2\beta)^{1/2}} = \frac{U}{c_0} - \frac{\lambda h_0}{c_0} \beta. \quad (+)$$

Since the LHS  $\nearrow$  with  $\beta > 0$  and RHS  $\searrow$  with  $\beta > 0$  as illustrated,  $\exists!$  root  $\beta = \beta_c$  to (+) as illustrated.



[S/N3]

(b)(ii) Rate at which energy flows out of a stationary shock is

$$Q = \left[ \underbrace{\int_0^h \left( \frac{1}{2} \rho u^2 + p g z \right) u dz}_{\text{Rate at which KE + PE}} + \underbrace{\int_0^h (p - p_{\text{atm}}) u dz}_{\text{Rate at which work is done by pressure}} \right]_-^+$$

Since  $p - p_{\text{atm}} = \rho g z$  in shallow water theory and  $[h u]_-^+ = 0$ ,

$$Q = \left[ \frac{1}{2} \rho h u^3 + \rho g h^2 u \right]_-^+ = \underbrace{\rho h_-}_{\text{Conward}} u_- \left[ \frac{1}{2} u_-^2 + g h_- \right]_-^+$$

Hence for our moving shock, replacing  $u$  with  $u - V$ ,

$$Q = \rho h_- (u_- - V) \left[ \frac{1}{2} (u_- - V)^2 + g h_- \right]_-^+ = \rho h_0 (-V) \left( \frac{1}{2} V^2 + g h_0 - \frac{1}{2} \left( -\frac{V}{\beta} \right)^2 - g \beta h_0 \right)$$

$$[S/N5] \Rightarrow Q = -\rho h_0 V \left( \frac{1}{2} \frac{g h_0}{2} \beta (\beta+1) \left( 1 - \frac{1}{\beta^2} \right) + g h_0 (1 - \beta) \right) = \rho g h_0^2 V \frac{(1-\beta)^3}{4\beta} \rightarrow q$$

The shock can only be physical if energy lost as fluid crosses the shock (i.e. energy cannot be created), which requires  $q < 0$ . But  $q < 0$

$$[N2] \Rightarrow \beta_c > 1 \Rightarrow \frac{U}{\lambda h_0} > \beta_c > 1 \text{ (from diagram)} \Rightarrow U > \lambda h_0.$$

2014

3. A stream flowing over a horizontal surface is governed by the shallow water equations

$$\frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x} + h \frac{\partial u}{\partial x} = 0, \quad \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + g \frac{\partial h}{\partial x} = 0,$$

where  $u(x, t)$  is the fluid velocity in the  $x$  direction,  $h(x, t)$  is the depth of the stream and  $g$  is the acceleration due to gravity.

- (a) [6 marks] Show that the shallow water equations can be rewritten as

$$\left( \frac{\partial}{\partial t} + (u \pm c) \frac{\partial}{\partial x} \right) (u \pm 2c) = 0,$$

where  $c = \sqrt{gh}$ , and state the significance of the quantities  $Q_{\pm} = u \pm 2c$  and the curves  $dx/dt = u \pm c$ .

At  $t = 0$ , a previously uniform stream  $u = 1$ ,  $h = 1$  is suddenly blocked by a dam at  $x = 0$ , so that  $u(x, 0) = h(x, 0) = 1$ , but  $u(0, t) = 0$  for  $t > 0$ . You may assume that  $g > 1$ .

- (b) [12 marks] Concentrate on  $x > 0$ ,  $t > 0$ . By considering the characteristics that come from  $\{t = 0, x > 0\}$ , and  $\{x = 0, t > 0\}$ , deduce that the value of  $c$  immediately downstream of the dam is  $c(0, t) = \sqrt{g} - \frac{1}{2}$ . Also considering characteristics that come from  $\{x = 0, t = 0\}$ , deduce that the fluid velocity is given by

$$u(x, t) = \begin{cases} 0 & 0 < x < (\sqrt{g} - \frac{1}{2})t, \\ \frac{2}{3} \left( \frac{x}{t} - \sqrt{g} \right) + \frac{1}{3} & (\sqrt{g} - \frac{1}{2})t < x < (\sqrt{g} + 1)t, \\ 1 & (\sqrt{g} + 1)t < x, \end{cases}$$

and find a similar expression for  $c(x, t)$ .

- (c) [4 marks] In  $x < 0$ , a shock propagates upstream with speed  $V$ , separating the uniform stream  $u = 1$ ,  $h = 1$  from a region of stationary water with depth  $h_0 > 1$  adjacent to the dam. Show that the shock speed is

$$V = \frac{1}{h_0 - 1},$$

and that  $h_0$  satisfies

$$2h_0 = g(h_0 + 1)(h_0 - 1)^2.$$

- (d) [3 marks] Combining your solutions from parts (b) and (c), draw a sketch of the height profiles  $h(x, t)$  (as a function of  $x$ ) at  $t = 1$  and at  $t = 2$ , on the same pair of axes.

[You may assume the conditions for a shallow water shock moving with velocity  $-V$ ,

$$[h(u + V)]_{-}^{+} = [h(u + V)^2 + \frac{1}{2}gh^2]_{-}^{+} = 0,$$

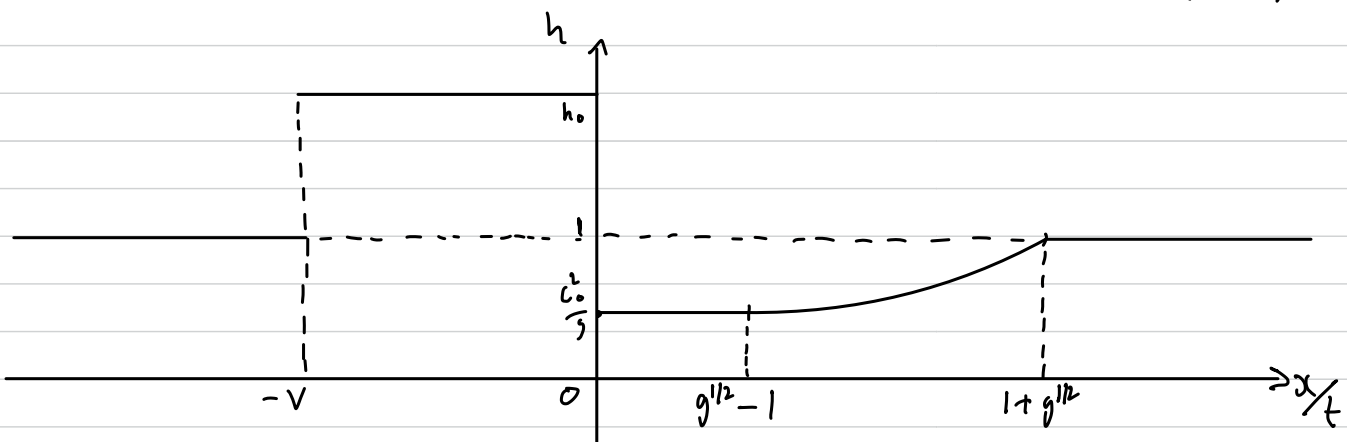
where  $[ ]_{-}^{+}$  denotes the change in the quantity from one side of the shock to the other. ]

2014 Q3(d) Not quite sure how to combine previous parts? Was happy with all previous parts however.

Parts (b) & (c)  $\Rightarrow$

$$h_0(x,t) = \begin{cases} 1 & \text{for } x < -Vt \\ h_0 & \text{for } -Vt < x < 0 \\ c_0^2/g & \text{for } 0 < x < (g^{1/2} - \frac{1}{2})t \\ \left(\frac{x}{t} + 2g^{1/2} - 1\right)^2 / 4g & \text{for } (g^{1/2} - \frac{1}{2})t < x < (1 + g^{1/2})t \\ g^{1/2} & \text{for } x > (1 + g^{1/2})t \end{cases}$$

$$(c_0 = g^{1/2} - \frac{1}{2})$$



2. A barotropic gas with pressure-density relation  $p = P(\rho)$  flows steadily past a thin symmetric wing, which occupies the region  $|x| \leq a$  and has upper and lower surfaces given by  $y = \pm f(x)$ , where  $f(\pm a) = 0$  and  $|f| \ll a$ . The flow is governed by Euler's equations for an inviscid compressible fluid,

$$\nabla \cdot (\rho \mathbf{u}) = 0, \quad \rho \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p.$$

Far upstream of the wing the flow is uniform, with speed  $U$  in the  $x$  direction, density  $\rho_0$ , pressure  $p_0 = P(\rho_0)$ , and sound speed given by  $c_0^2 = P'(\rho_0)$ .

- (a) [10 marks] Assuming the flow is irrotational and writing  $\mathbf{u} = U\hat{\mathbf{e}}_x + \nabla\phi$ , find a linearised expression for the pressure perturbation in terms of the velocity potential, and show that  $\phi(x, y)$  satisfies

$$(M^2 - 1) \frac{\partial^2 \phi}{\partial x^2} = \frac{\partial^2 \phi}{\partial y^2},$$

where the Mach number  $M$  should be defined. Also derive the linearised boundary conditions

$$\frac{\partial \phi}{\partial y} = \pm U f'(x) \quad \text{on} \quad y = 0\pm, \quad |x| \leq a,$$

where  $y = 0\pm$  denotes the boundary approached from above and below, respectively.

Briefly describe the conditions that should be applied at infinity if  $M < 1$ , and explain why an appropriate condition in the case  $M > 1$  is  $\phi \rightarrow 0$  as  $x \rightarrow -\infty$ .

- (b) [8 marks] Suppose now that  $M > 1$ . With the aid of a diagram to identify distinct regions of the flow, find the solution for  $\phi(x, y)$ .
- (c) [7 marks] Suppose further that  $f(x) = b(1 - x^2/a^2)$ . Sketch the streamlines of the flow, and calculate the drag force  $D$  on the wing. Show that  $D$  is minimised (for  $M > 1$ ) when  $U = \sqrt{2}c_0$ .

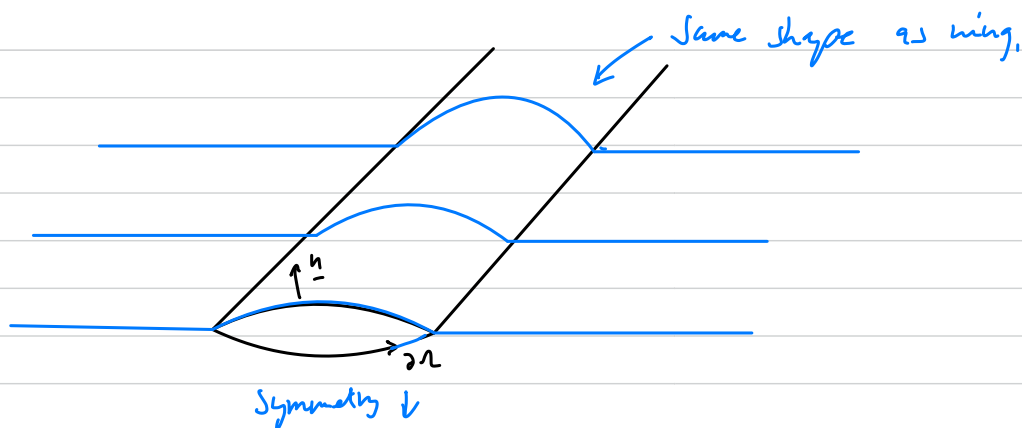
[You may assume the expression

$$D = \int_{-a}^a f'(x) [p(x, 0-) + p(x, 0+)] dx,$$

for the drag force on the wing.]

Would it be possible to go over 2015 q2c please?

2015/Q2(c)



Force on wing  $E = \int_{\partial\Omega} -p \underline{n} ds$ ,  $\underline{n} = \frac{(-f'(x), 1)}{\sqrt{1+f'(x)^2}}$

But given  $D = \int_{-a}^a f'(x) (p(x, 0-) + p(x, 0+)) dx$  after linearization.

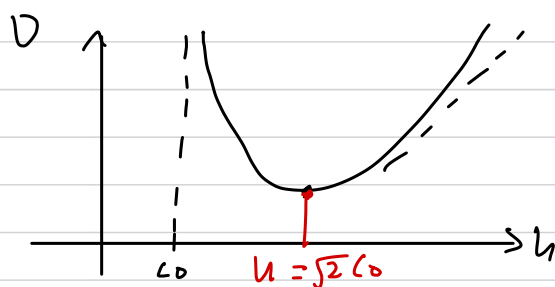
$$= -\rho_0 u \int_{-a}^a f'(x) (\phi_2(x, 0-) + \phi_2(x, 0+)) dx \quad (p = -\rho_0 u \phi_x)$$

$$= +\frac{\rho_0 u^2}{\beta} \int_{-a}^a 2 f'(x)^2 dx \quad \left( \begin{array}{l} \text{by part (b)} \\ (\beta = \sqrt{u^2 - c_0^2}) \end{array} \right)$$

$$= \frac{\rho_0 u^2}{\beta} \int_{-a}^a 2b^2 \left( -\frac{2x}{a^2} \right)^2 dx$$

$$= \frac{8\rho_0 u^2}{\beta} \frac{b^2}{a^4} \frac{2a^3}{3}$$

i.e.  $D = \frac{16}{3} \frac{\rho_0 b^2 u^2}{a \sqrt{\frac{u^2}{c_0^2} - 1}}$



Want min of  $D$  for  $u > c_0$ .

$$\frac{dD}{du^2} = \frac{16}{3} \frac{\rho_0 b^2}{a} \left[ \frac{1}{\frac{u^2}{c_0^2} - 1} - \frac{u^2}{2(\frac{u^2}{c_0^2} - 1)^{3/2} c_0^2} \right] = 0$$

$$\Rightarrow 2\left(\frac{u^2}{c_0^2} - 1\right) = \frac{u^2}{c_0^2} \Rightarrow u^2 = 2c_0^2 \Rightarrow u = \sqrt{2} c_0. \quad \square$$

3. A homentropic gas with pressure-density relation  $p = k\rho^\gamma$  occupies a one-dimensional tube. The gas is initially at rest with density  $\rho_0$  and pressure  $p_0$ , and lies to the right of an impermeable piston at  $x = 0$ . A measuring device is placed in the tube ahead of the piston, at  $x = L$ .

- (a) [3 marks] Briefly describe the physical principles underlying the Rankine-Hugoniot conditions for a shock moving with speed  $V$ ,

$$[\rho(u - V)]_-^+ = [p + \rho(u - V)^2]_-^+ = \left[ \frac{1}{2}(u - V)^2 + \frac{\gamma p}{(\gamma - 1)\rho} \right]_-^+ = 0.$$

- (b) [10 marks] For  $t > 0$  the piston is pushed forwards with constant speed  $U$ , causing a shockwave to travel ahead of it.

Use the Rankine-Hugoniot conditions to show that the speed of the shock is given by

$$V = \frac{(\gamma + 1)U}{4} \left[ 1 + \left( 1 + \frac{16c_0^2}{(\gamma + 1)^2 U^2} \right)^{1/2} \right],$$

where  $c_0^2 = \gamma p_0 / \rho_0$ .

Sketch the density  $\rho(L, t)$  measured as a function of time at  $x = L$ , labelling all the important points on your graph. (Consider only  $t < L/U$ .)

- (c) [12 marks] Now suppose that instead of being pushed forwards, the piston is pulled backwards for  $t > 0$ , with constant speed  $U$  in the negative  $x$  direction.

Assuming  $U < 2c_0/(\gamma + 1)$ , and with the aid of a characteristic diagram to help find the solution  $c(x, t)$ , carefully sketch the sound speed  $c(L, t)$  measured as a function of time at  $x = L$ , labelling all the important points on your graph.

What is different if  $U > 2c_0/(\gamma + 1)$ ?

[You may assume that the equations of one-dimensional homentropic gas dynamics,

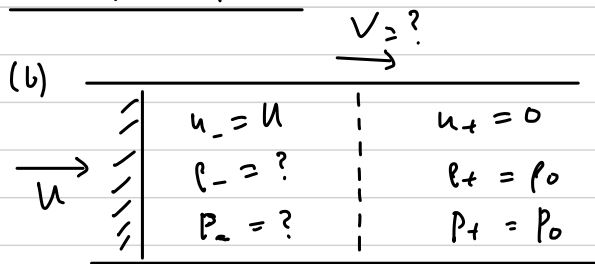
$$\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + \rho \frac{\partial u}{\partial x} = 0, \quad \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \frac{1}{\rho} \frac{\partial p}{\partial x} = 0,$$

can be written as

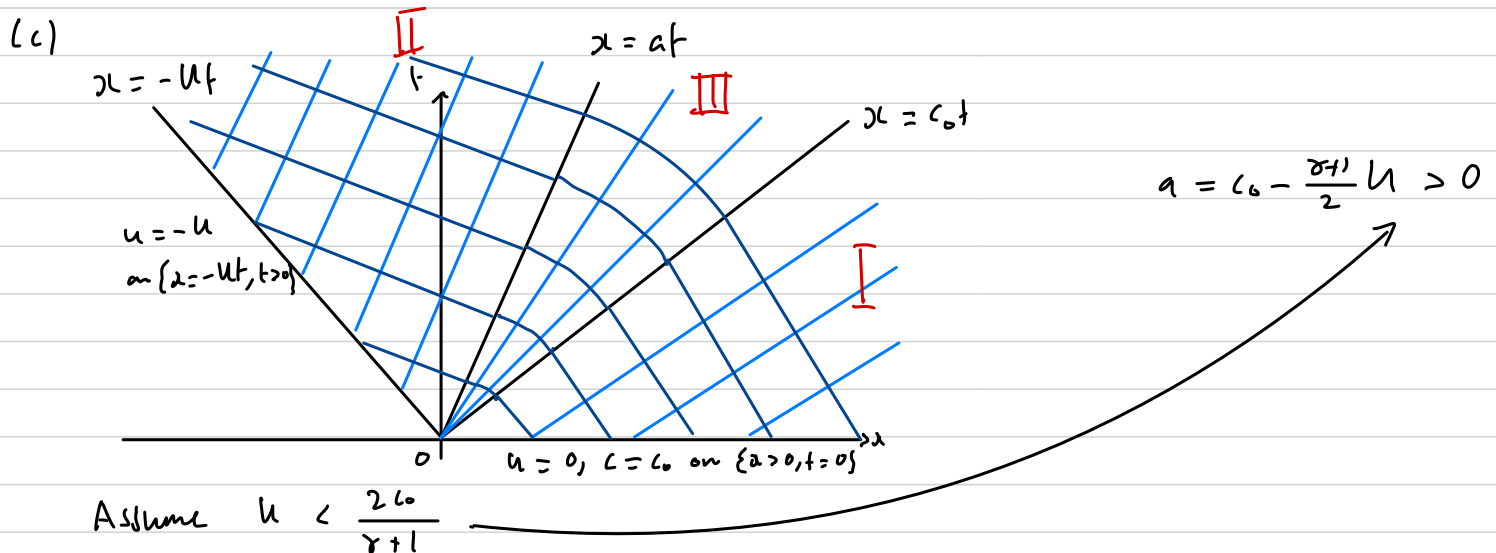
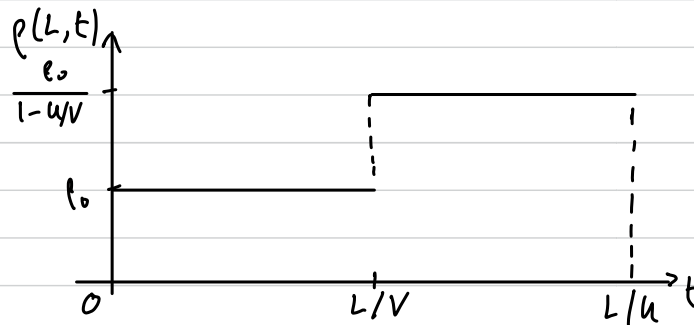
$$\left( \frac{\partial}{\partial t} + (u \pm c) \frac{\partial}{\partial x} \right) \left( u \pm \frac{2c}{\gamma - 1} \right) = 0,$$

where  $c^2 = \gamma p / \rho$ .]

2015/BS.4/Q3

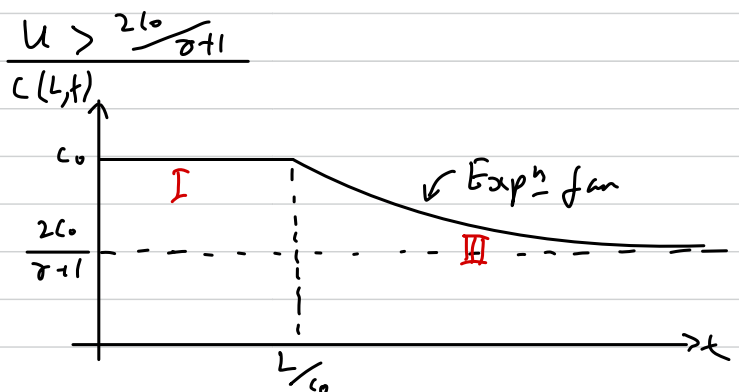
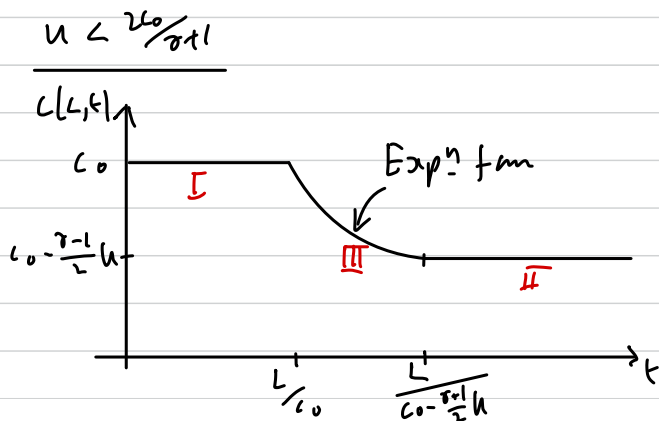


RHC  $\Rightarrow \rho_- = \rho_0 \frac{1}{1 - \frac{u}{V}} > \rho_0 = \rho_+$   
as  $V > u$

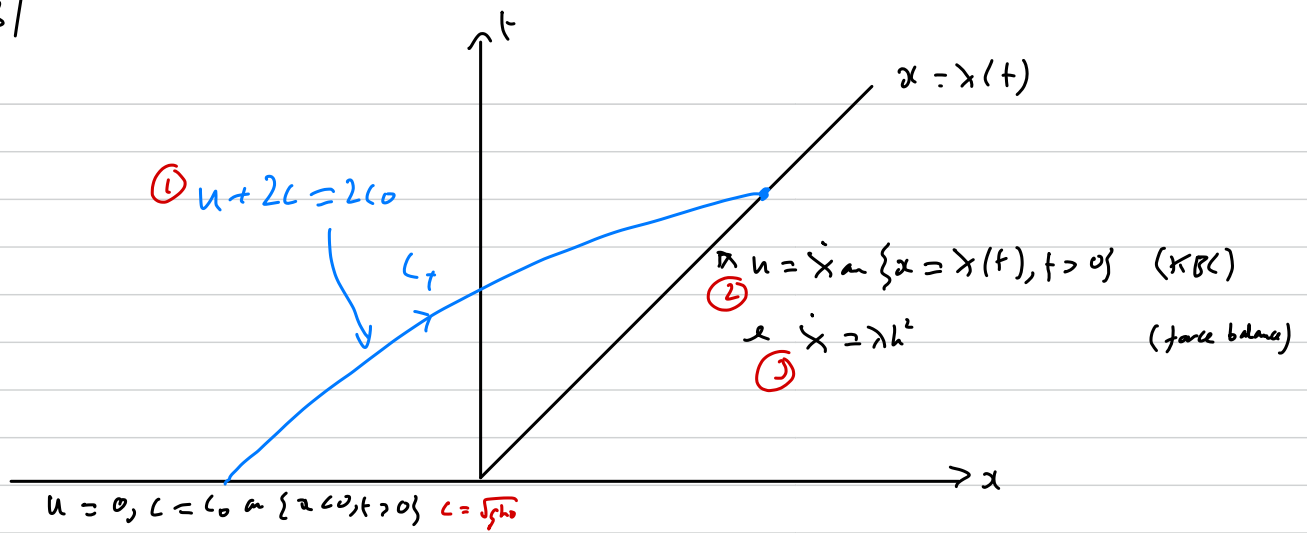


know from lectures this means gas not left behind by piston (forming a vacuum),  
so that  $u - \frac{2c}{\gamma-1} = -\frac{2c_0}{\gamma-1}$  everywhere (from char<sup>s</sup> originating from  $\{x > 0, t = 0\}$ )

- I: + char<sup>s</sup> also from  $\{x > 0, t = 0\} \Rightarrow u = 0, c = c_0$  in  $x > ct, t > 0$   
 II: + char<sup>s</sup> from  $\{x = -ut, t > 0\} \Rightarrow u = -u, c = c_0 - \frac{\gamma-1}{2}u$  in  $-ut < x < (c_0 - \frac{\gamma-1}{2}u)t$   
 III: + char<sup>s</sup> from  $\{x = 0, t = 0\} \Rightarrow c = \frac{2c_0}{\gamma+1} + \frac{\gamma-1}{\gamma+1} \frac{x}{t}$  for  $(c_0 - \frac{\gamma-1}{2}u)t < x < ct$



2015/Q3/



$$\textcircled{1} - \textcircled{3} \text{ with } c = \sqrt{gh} \Rightarrow \left. \begin{aligned} u + 2c &= 2c_0 \\ u &= \dot{\chi} \\ \dot{\chi} &= \lambda h^2 = \frac{\lambda c^4}{g^2} \end{aligned} \right\} \text{ in } x = \chi(t)$$

$$\Rightarrow u + 2c = 2c_0 \text{ and } u = \frac{\lambda c^4}{g^2}$$

i.e.  $u$  and  $c$  constant in piston, so  $\dot{\chi} = \text{const.}$

Let  $c(x, t) = \beta c_0$  where  $\beta > 0$ , then  $u(x, t) = 2(c_0 - c) = 2(1 - \beta)c_0$

and

$$2(1 - \beta)c_0 = u(x, t) = \frac{\lambda c(x, t)^4}{g^2} = \frac{\lambda \beta^4 c_0^4}{g^2}$$

$$\Rightarrow 1 - \beta = \frac{\lambda (gh_0)^{3/2}}{g^2} \beta^4 = \frac{\lambda h_0^{3/2}}{g^{1/2}} \beta^4$$

Now problem is identical to a piston withdrawal problem as  $\dot{\chi} = 2(1 - \beta)c_0$ .