

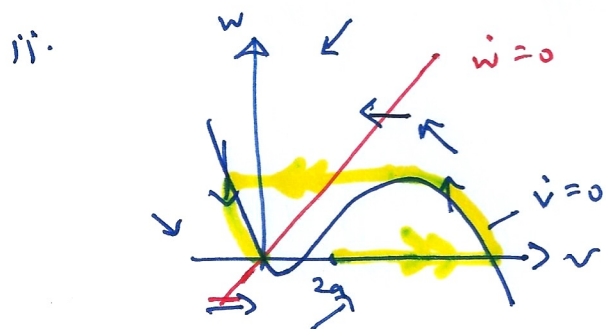
1/ (a)

$$\epsilon \dot{v} = Av(v-a)(1-v) - w$$

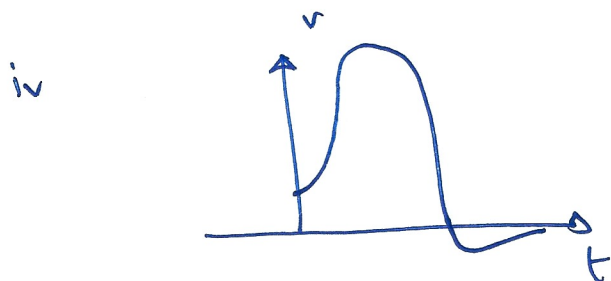
$$\dot{w} = -w + bv$$

$$\epsilon \ll 1, a \ll 1$$

(i)  $v$  intracellular electrical potential relative to resting state  
 space clamp - forced to be independent of spatial variable  $x$



iii At large  $w$ ,  $\dot{v} < 0$ ,  $\dot{w} < 0 \Rightarrow$  trajectory moves as shown  
 However,  $\epsilon \ll 1 \Rightarrow$  almost horizontal away from  $v$  nullcline  
 $\Rightarrow$  excursion as shown (yellow)



(b)

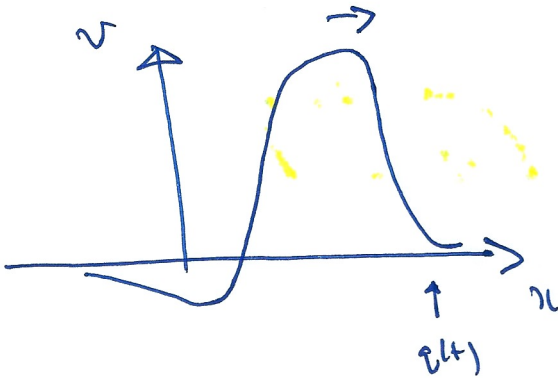
2

$$\epsilon v_t = \epsilon \tilde{v}_{xx} + Av(v-a)(1-v) - (1+\delta \sin t)w$$

$$w_t = -w + bv$$

$$\delta \ll 1$$

$$v, w \rightarrow 0 \text{ at } \pm \infty$$



$$(i) \quad y = x - v(t) \quad \tau = t$$

$$\Rightarrow \frac{\partial}{\partial x} = \frac{\partial}{\partial y}, \quad \frac{\partial}{\partial t} = \frac{\partial}{\partial \tau} - v \frac{\partial}{\partial y}$$

$$\Rightarrow w_\tau = v w_y - w + bv$$

$$A \quad \epsilon (v_\tau - v w_y) = \epsilon \tilde{v}_{yy} + Av(v-a)(1-v) - (1+\delta \sin \tau)w$$

(ii) ~~Now we~~ Now I suppose ~~we~~ ahead of the front, still  $w \sim 0(1)$ ,

$w$  and  $v$  are small, neglect  $\epsilon$

$$\Rightarrow Av(v-a)(1-v) \approx Av \approx -aAv \approx (1+\delta \sin \tau)w$$

$$\text{So } v \approx -\frac{(1+\delta \sin \tau)w}{aA} \quad \text{also } a \ll 1 \text{ but also } \delta \ll 1 \dots$$

$$\begin{aligned} \text{suppose } w_\tau - v w_y &\approx -w - \frac{v(1+\delta \sin \tau)}{aA} w \\ &\approx -w \left[ 1 + \frac{v(1+\delta \sin \tau)}{aA} \right] \end{aligned}$$

of requested form with

$$f(\tau) = 1 + \frac{f(1 + \delta \sin \tau)}{aA}$$

- well this is a bit tedious  $a \ll 1$  but I suppose  $\delta \ll 1$

iii  $w_\tau - \dot{q} w_y = -fw$

So  $f > 0$  &  $\dot{q} > 0$

can solve with characteristics

Note  $\dot{y} = -\dot{q} < 0$  characteristics emerge from  $y = \infty$ !

Since  $f = \text{constant}$  (as  $\delta \ll 1$ )

~~Suppose  $w = w_0(s)$  at  $y = s > 0$  at  $\tau = 0$~~

~~(then  $\dot{y} = -\dot{q} \Rightarrow y = \frac{3}{2} [q(s) - q(\tau)]$ )~~

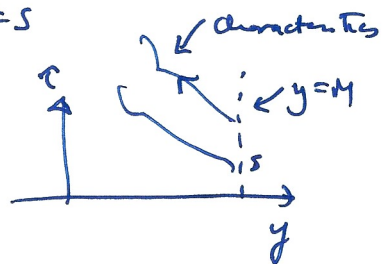
Suppose we apply  $w = w_M(s)$  at  $y = M$  and  $\tau = s$

then  ~~$w = w_0$~~   $w = w - fw$

$$\dot{y} = -\dot{q}$$

$$\Rightarrow y = M - [q(\tau) - q(s)]$$

$$w \approx w_M(s) e^{-(\tau-s)}$$



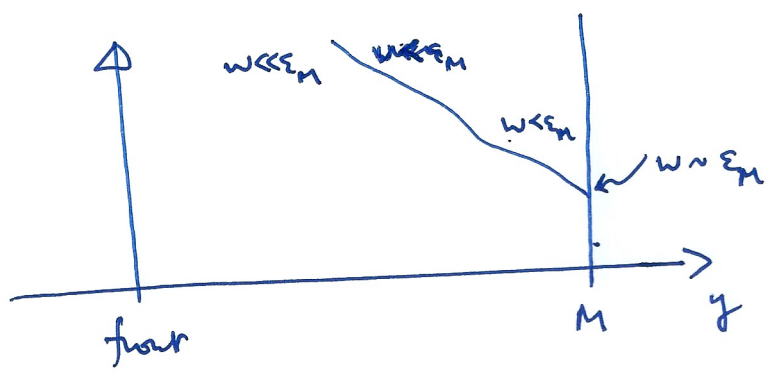
Since  $\delta \ll 1$  we have approximately  $q = c\tau$  (convenient assumption)

$$\text{so } \tau - s \approx \frac{M-y}{c}$$

$$\Rightarrow w \approx w_M \left[ \tau - \frac{(M-y)}{c} \right] \exp \left[ \frac{y-M}{c} \right]$$

& in order for this to  $\rightarrow 0$  at  $\infty$  we need  $w_M \rightarrow 0$  rapidly  $\Rightarrow w \approx 0$ .

This is not very well put. Basically  $w$  decays exponentially along the characteristics as  $y$  decreases, so if  $w \rightarrow 0$  as  $y \rightarrow \infty$ , it enforces  $w = 0$  ahead of the front.



If  $M \gg 1$ ,  $w \sim \epsilon_M \ll 1$  for  $y \sim 1$  for sufficiently large  $\tau$ .

That's a bit awkward.

(iv) well, if we take  $w = 0$  ahead of the front and now in the front  $y = \epsilon^y$

at leading order  $\Rightarrow -\frac{1}{2} v_y = v_{yy} + Av(v-a)(1-v)$  as  $w = 0$

$v \rightarrow 0 \quad y \rightarrow \infty$   
 $v \rightarrow 1 \quad y \rightarrow -\infty$

f using the hint

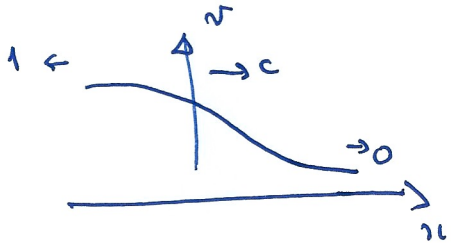
$$v'' + \frac{1}{2} v' - Av(v-a)(v-1)$$

$$U_0 = 0, U_1 = a, U_2 = 1 \quad \begin{matrix} v \rightarrow U_0 = 0 & y \rightarrow \infty \\ v \rightarrow U_2 = 1 & y \rightarrow -\infty \end{matrix}$$

$$\Rightarrow c = \sqrt{\frac{A}{2}} (U_0 + U_2 - 2U_1) = \sqrt{\frac{A}{2}} (1 - 2a) > 0.$$

Rather weird question

2/  $\nabla_t^2 v = \nabla^2 v + v(1-v) f(v) \quad v > 0$



(a) plane waves  $\nabla^2 v = v_{xx}$   
 $v = v(\eta) \quad \eta = x - ct$

$-cv' = v'' + v(1-v) f(v)$

(b) 2-D

$\underline{x} = \underline{X}(\underline{a}, t) \quad \underline{a} = \underline{A}(\underline{x}, t)$

$\underline{\nabla} v = \underline{e}_i \frac{\partial v}{\partial x_i} \quad \frac{\partial}{\partial x_i} = \frac{\partial a_j}{\partial x_i} \frac{\partial}{\partial a_j} = \alpha_{ij} \frac{\partial}{\partial a_j}$

so  $\underline{\nabla} v = \underline{e}_i \alpha_{ij} \frac{\partial v}{\partial a_j}$

summation convention assumed

$\nabla^2 v = \frac{\partial}{\partial x_j} \alpha_{ij} \frac{\partial}{\partial x_k} \alpha_{kj} \frac{\partial v}{\partial a_j}$

$= \alpha_{kl} \frac{\partial}{\partial a_l} \left[ \alpha_{kj} \frac{\partial v}{\partial a_j} \right]$

$= \alpha_{kl} \alpha_{kj} \frac{\partial^2 v}{\partial a_l \partial a_j} + \alpha_{kl} \frac{\partial \alpha_{kj}}{\partial a_l} \frac{\partial v}{\partial a_j}$

as for  
with

$k \rightarrow p$   
 $l \rightarrow i$

We need to show

$$\begin{aligned} \alpha_{kl} \frac{\partial \alpha_{kj}}{\partial a_l} \frac{\partial v}{\partial a_j} &= \frac{\partial \alpha_{pi}}{\partial x_p} \frac{\partial v}{\partial a_i} + \alpha_{ij} \frac{\partial x_i}{\partial t} \frac{\partial v}{\partial a_j} \\ &= \frac{\partial \alpha_{kj}}{\partial x_k} \frac{\partial v}{\partial a_j} + \alpha_{kj} \frac{\partial x_k}{\partial t} \frac{\partial v}{\partial a_j} \\ &= \left( \frac{\partial \alpha_{kj}}{\partial x_k} + \alpha_{kj} \frac{\partial x_k}{\partial t} \right) \frac{\partial v}{\partial a_j} \end{aligned}$$

know  $\alpha_{kl} = \frac{\partial a_l}{\partial x_k}$

we want to show  $\alpha_{kl} \frac{\partial \alpha_{kj}}{\partial a_l} = \frac{\partial \alpha_{kj}}{\partial x_k} + \alpha_{kj} \frac{\partial x_k}{\partial t}$

ugh  
well I don't get this. I think she is now considering  $v$  as  $v(\underline{a}, t)$

So that  $\frac{\partial v(\underline{x}, t)}{\partial t} = \frac{\partial v}{\partial t} + \frac{\partial v}{\partial x_i} \frac{\partial x_i}{\partial t}$  should be  $v$  really  
 $(v(\underline{x}, t) = v(\underline{x}(\underline{a}, t), t) \equiv v(\underline{a}, t)$

so  $\frac{\partial v}{\partial t} \Big|_{\underline{a}} = \frac{\partial v}{\partial t} \Big|_{\underline{x}} + \frac{\partial x_i}{\partial t} \frac{\partial v}{\partial x_i}$

his required  $\nabla^2 v$

now this is particle velocity  
 $\frac{\partial v}{\partial t} \Big|_{\underline{x}} = \frac{\partial v}{\partial t} \Big|_{\underline{a}} - \frac{\partial x_i}{\partial t} \frac{\partial v}{\partial x_i} = \nabla^2 v + \dots$

so  $\frac{\partial v}{\partial t} \Big|_{\underline{a}} = \alpha_{kl} \alpha_{kj} \frac{\partial^2 v}{\partial a_l \partial a_j} + \alpha_{kl} \frac{\partial \alpha_{kj}}{\partial a_l} \frac{\partial v}{\partial a_j} + \frac{\partial x_i}{\partial t} \frac{\partial v}{\partial x_i} + v(\underline{a}, t)$

As before

$$\frac{\partial v}{\partial x_i} = \frac{\partial a_j}{\partial x_i} \frac{\partial v}{\partial a_j} = \alpha_{ij} \frac{\partial v}{\partial a_j}$$

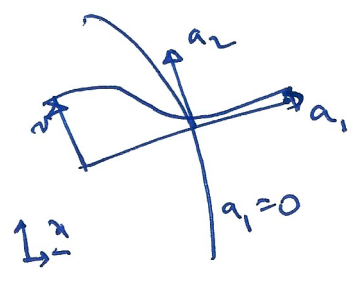
and also  $\frac{\partial \alpha_{ki}}{\partial x_k} = \frac{\partial \alpha_{kj}}{\partial a_j} \frac{\partial a_j}{\partial x_k} = \alpha_{kj} \frac{\partial \alpha_{ki}}{\partial a_j}$  (1)

So  $\frac{\partial v}{\partial t} \Big|_a = \alpha_{kl} \alpha_{kj} \frac{\partial^2 v}{\partial a_l \partial a_j} + \frac{\partial \alpha_{kj}}{\partial x_k} \frac{\partial v}{\partial a_j} + \alpha_{ij} \frac{\partial v}{\partial a_j} \frac{\partial x_i}{\partial t} + v(1-v)f(v)$

$k \rightarrow p, j \rightarrow i$

It's fine there is a prettier way

(c)



$$\underline{a} = (a_1, a_2), \quad |\underline{a}| = 1$$

$$\underline{\alpha} = \left( \frac{\partial a_1}{\partial x_1}, \frac{\partial a_2}{\partial x_2} \right) = \underline{\nabla} \phi$$

(i) The normal to the wave front is  $\underline{\nabla} \phi = \underline{\alpha} \Rightarrow \underline{n}$ .

(ii) We assume  $v$  changes rapidly in the front ~~the~~ whose variation along the front is slow.

Specifically we suppose  $\frac{\partial}{\partial a_1} \sim 1, \frac{\partial}{\partial a_2} \sim \epsilon$  say

Now note that the curvature is  $2\kappa = \underline{\nabla} \cdot \underline{n} = \underline{\nabla} \cdot \underline{\alpha}$

and the front velocity is  $\frac{\partial x}{\partial t} \cdot \underline{n} = \frac{\partial x_i}{\partial t} \alpha_{ij}$

So approximately we have

$$v_t = \frac{d^2 p_1}{dt^2} \alpha_{p_1} + \frac{\partial \alpha_{p_1}}{\partial x_p} v_{a_1} + \alpha_{i1} \frac{\partial x_i}{\partial t} v_{a_1} + v(1-v)f(v)$$

The front velocity is  $v_n = \alpha_{i1} \frac{\partial x_i}{\partial t}$

The curvature  $K = 2\kappa = \frac{\partial^2 \alpha}{\partial x_i^2} = \frac{\partial \alpha_{i1}}{\partial x_i}$

So we have  $\alpha_{p_1} \alpha_{p_1} = \alpha_{11}^2 + \alpha_{21}^2 = 1$  as  $|\underline{\alpha}| = 1$

$$\Rightarrow v_t = v_{a_1} + (K + v_n) v_{a_1} + v(1-v)f(v)$$

and this has a steady solution (we are via travelling wave)

iff  $K + v_n = c$

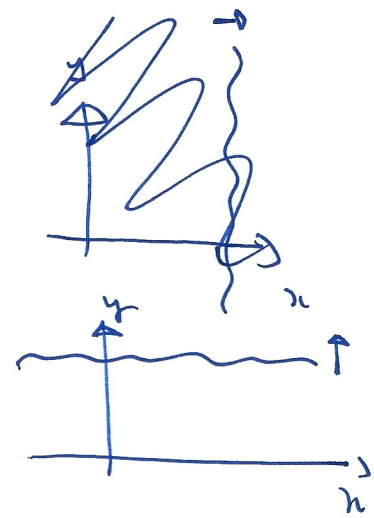
Since we know  $v'' + cv' + v(1-v)f(v) = 0$  works.



(d) wave front is

$$x = s, \quad y = ct + \delta h(s, t)$$

$$k = \frac{-\delta h_{ss}}{(1 + \delta^2 h_s^2)^{3/2}}$$



$$\Rightarrow \frac{-\delta h_{ss}}{(1 + \delta^2 h_s^2)^{3/2}} + v_n = c$$

The curve is

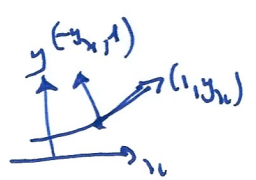
$$y = ct + \delta h(x, t)$$

$$\text{So } y_x = \delta h_x = \delta h_s$$

$$\vec{n} = \frac{(-\delta h_s, 1)}{(1 + \delta^2 h_s^2)^{1/2}}$$

$$\underline{v} = (\dot{x}, \dot{y}) = (0, c + \delta h_t)$$

$$v_n = \frac{c + \delta h_t}{(1 + \delta^2 h_s^2)^{1/2}} \quad \text{Eq. } = F$$



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$$\text{So } \frac{-\delta h_{ss}}{(1 + \delta^2 h_s^2)^{3/2}} + \frac{c + \delta h_t}{(1 + \delta^2 h_s^2)^{1/2}} = c$$


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ii

6

Expanding for small  $\delta$

$$-\delta h_{ss} + c + \delta h_f + O(\delta^2) = c$$

$$\Rightarrow h_f = h_{ss}$$

diffusion so stable

[ for what is this  $h \in L^2$  ?! ]

↑  
maybe he wants  $\frac{d}{dt} \int_{-\infty}^{\infty} h^2 ds = - \int_{-\infty}^{\infty} h_s^2 ds < 0$  ! ]

1/

$$\epsilon \dot{v} = -m^3(v) (0.8 - n)(v - 1) - \gamma_K n^4 (v + v_K) = g(v, n)$$

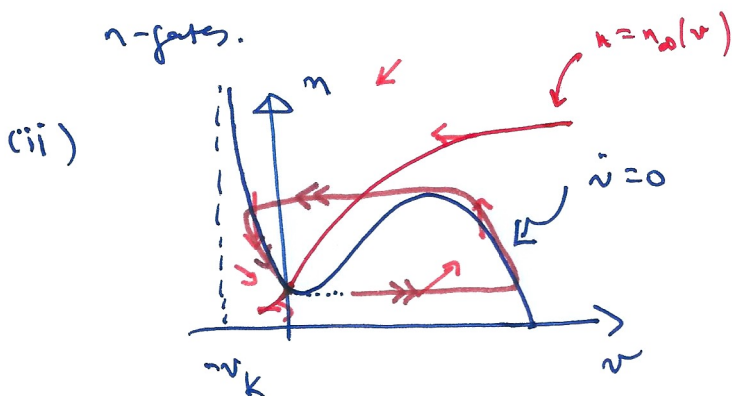
$$\tau_n \dot{n} = n_\infty(v) - n$$

$$\epsilon = 2 \times 10^{-3}$$

$$v_K = 0.1$$

Equilibrium is  $v=0, n=n_{eqm}$ , unique, stable

(a) (i)  $m$  is a gate variable for potassium ion channel transport (each channel has 4  $n$ -gates):  $n$  represents the fraction of open  $n$ -gates.



doesn't ask for proof of this

(ii) with also the  $n$  nullcline as above

$$\text{- large } n : \dot{n} < 0, \dot{v} < 0$$

$\Rightarrow$  as indicated by arrows, trajectories cycle round the equilibrium

$\Rightarrow \epsilon \ll 1 \Rightarrow$  as shown in brown a small disturbance causes a large disturbance  $\Rightarrow$  excitable

$$(b) \quad \epsilon n_T = \epsilon \hat{v}_{n_T} + g(v, n)$$

(g as defined top of p1)

$$\tau_n n_T = n_\infty(v) - n$$

$$v \rightarrow 0, n \rightarrow n_{eq} \quad \text{as} \quad x \rightarrow \pm \infty$$

$$(i) \quad y = x - ct$$

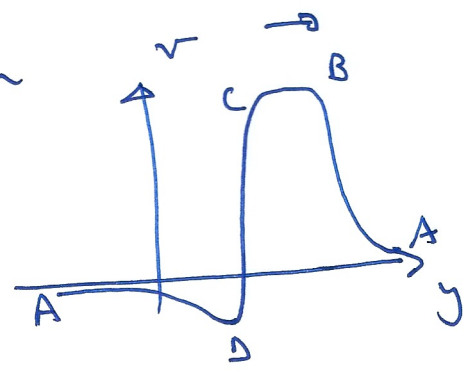
$$Y = \frac{y}{\epsilon}, \quad c > 0$$

v(y) etc

$$-\epsilon c v' = \epsilon^2 v'' + g$$

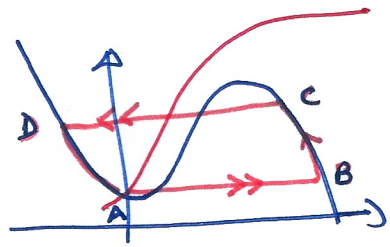
$$-c \tau_n n' = n_\infty - n$$

The wave will be as shown



A coexisting trajectory in

(v, n) space



The wave front is a front phase,  $y = \epsilon Y$

$$\Rightarrow -c v' = v'' + g(v, n)$$

$$' = \frac{d}{dY}$$

$$-c \tau_n n' = \epsilon (n_\infty - n)$$

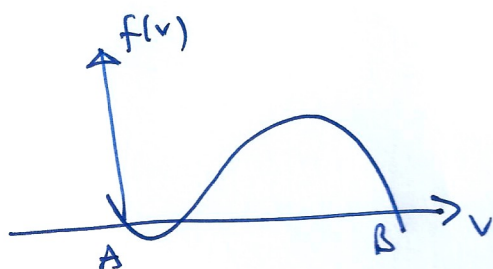
$$\Rightarrow n \approx n_{eq}, \quad v'' + c v' + f(v) = 0 \quad \text{where} \quad f(v) = g(v, n_{eq})$$

From the figures above

$$v \rightarrow 0 \rightsquigarrow \gamma \rightarrow +\infty$$

(ii) Also  $\rightsquigarrow \gamma \rightarrow -\infty$   $v \rightarrow v_B$  where  $f(v_B) = 0$

$$v_B \dot{\equiv} -m^3(v_B) (0.8 - n_{ev}) (v_B - 1) - \gamma_k n_{ev}^4 (v_B + v_k) = f(v_B)$$



$$\text{we note that } -m^3(0) (0.8 - n_{ev}) \cdot -1 - \gamma_k n_{ev}^4 v_k = 0$$

$$(\text{since } g(0, n_{ev}) \equiv 0 \text{ \& } v \dot{\equiv} f(0) = 0)$$

therefore  $v_B$  satisfies

$$-m^3(v_B) (0.8 - n_{ev}) (v_B - 1) - \left(\frac{v_B}{v_k} + 1\right) m^3(0) (0.8 - n_{ev}) = 0$$

$$\Delta \text{ thus } \underline{v_B - 1 = \left(\frac{v_B}{v_k} + 1\right) \frac{m^3(0)}{m^3(v_B)}}$$

and the approximate value of this for small  $m^3(0)$

$$(\underline{m^3(0) \ll \gamma_k m^3(v_B)})$$

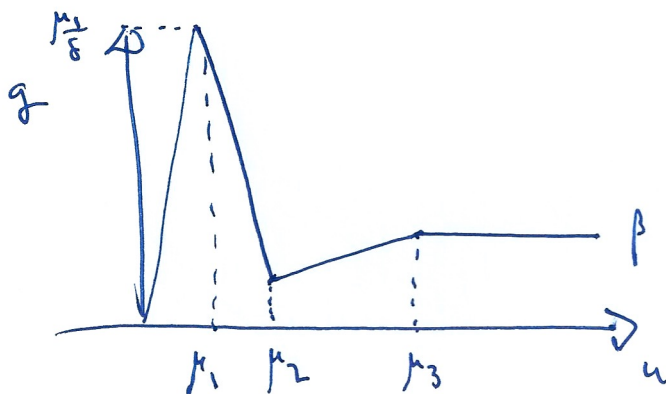
$$\underline{v_B \dot{\approx} 1} \quad (\text{the other two values are } v_B = 0 \text{ \& } v_B \ll 1)$$

CS-12 Math Physics 2013 q2

2/

$$\dot{u} + v = \mu - u$$

$$\varepsilon \dot{v} = -v + g(u)$$



$$\mu = \frac{2}{3}$$

$$0 < \varepsilon \ll \delta \ll 1$$

$$\beta = 0.1 \gg \delta$$

$\mu_2, \mu_3$  so  $g \dot{u}$ .

$$g(\mu_2) = \frac{\mu_1}{\varepsilon} - \frac{1}{\varepsilon}(\mu_2 - \mu_1) = \delta$$

$$g(\mu_3) = \delta + \delta(\mu_3 - \mu_2) = \beta$$

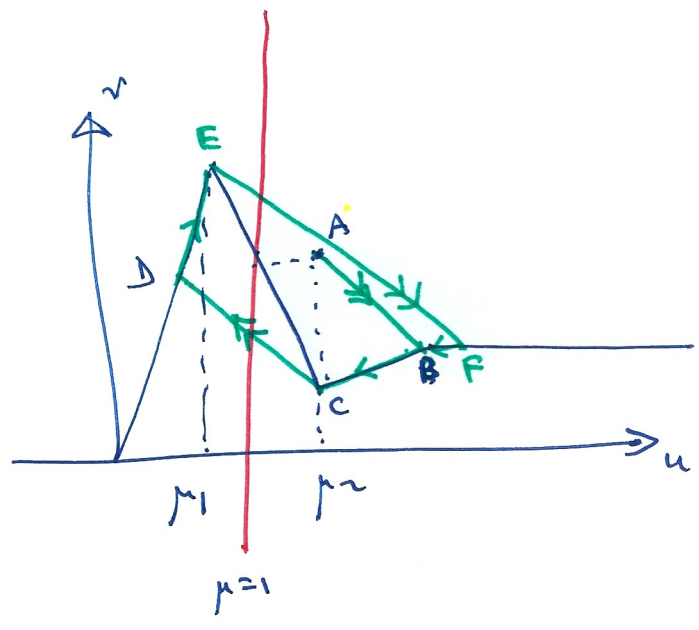
(i) so  $\mu_2 - \mu_1 = \mu_1 - \delta^2$   $\mu_2 = \frac{4}{3} - \delta^2$

$\hookrightarrow \mu_3 - \mu_2 = \frac{\beta}{\delta} - 1 \Rightarrow$   $\mu_3 = \frac{4}{3} - \delta^2 + \frac{\beta}{\delta} - 1$

(ii) as above

$\mu = 1$  so  $\mu_1 < \mu < \mu_2$

(b)



(i) Start at A ( $\mu_2, s(1)$ )

$v$  changes rapidly to get to  $v = s(u)$   
 note at A  $v > s(u) \Rightarrow v' < 0$  so heads to right + down.  
 In this rapid change,  $u+v \approx \text{constant}$

- AB: rapidly to  $v$  nullcline
  - BC: slowly on  $v$  nullcline to  $u = \mu_2$  (as  $u+v < 0$ )
  - CD: rapidly to  $v$  nullcline on  $u+v$  constant
  - DE: slowly to  $u = \mu_1$  on  $v$  nullcline
  - EF: rapidly to  $v$  nullcline along  $u+v = \text{constant}$
- then repeat (oscillates) F C D E F ...

(ii) on AB for  $t \gg \epsilon$   $u+v \approx 0$  so  $u+v \approx \mu_2 + s(1)$

well  $t \gg \epsilon$ . In more detail  $t = \epsilon T$   $(u+v)' \approx 0$   
 $\Rightarrow u+v \approx \mu_2 + s(1)$   
 $\& v' \approx -v + \delta + \delta(u - \mu_2)$  at least while  $u < \mu_3$

thus  $v' \approx -v + \delta + \delta [g(1) - v]$

Better find where B is.

~~At B~~ At B  $\frac{v - g(1)}{u - \mu_2} = -1$

$$g(1) = \frac{2\mu_1 - 1}{\delta} = \frac{1}{3\delta}$$

$$\text{so } v = \frac{1}{3\delta} - u + \mu_2 = \frac{1}{3\delta} + \frac{\beta}{\delta} + \frac{4}{3} - 1 - \delta^2 - u$$

suppose  $v < \beta$  then  $\frac{\beta + \frac{1}{3}}{\delta} - u + \frac{1}{3} - \delta^2 < \beta$

$$\Rightarrow u \approx \frac{\beta + \frac{1}{3}}{\delta} > \frac{\beta}{\delta} = \mu_3$$

So B is actually on flat wt.

well no matter

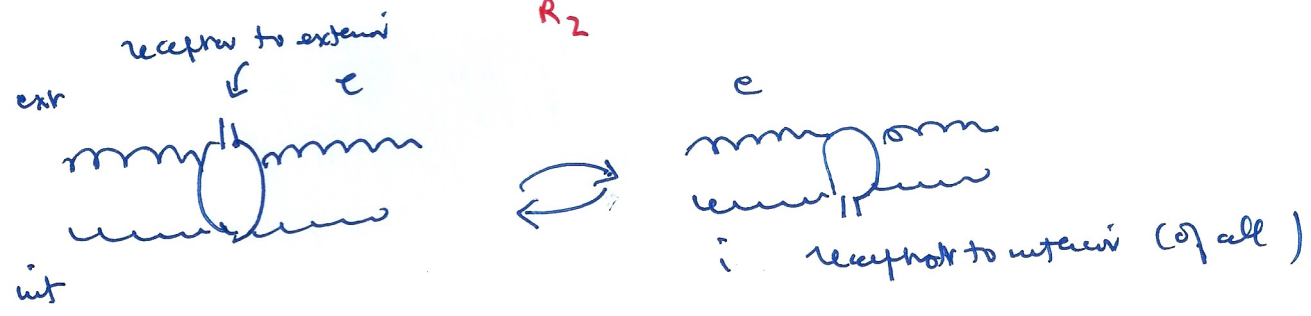
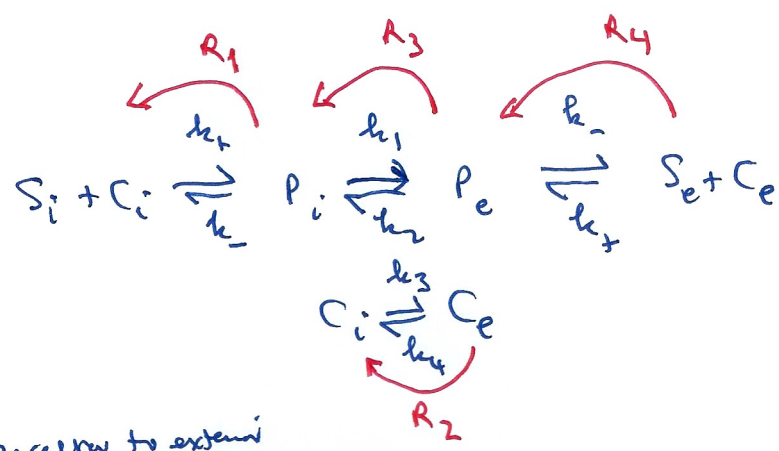
on AB  $v' \approx -v + \frac{1}{3} + O(\delta)$   
( $t = \epsilon T$ )

Seems a bit of a vague question since ~~we~~ with this approximation it takes infinite T to get there.

Seems you should just say  $t_* \sim \epsilon$



2/  
(a)



$S_i$  internal ~~leads~~ leads to  $C_i$  internal receptor  $\rightarrow$  complex switches to external receptor complex releases external substrate

Law of mass action  $A+B \xrightarrow{r} C$  rate of formation of C is  $\propto AB$

(b) As in the question, overall rates as indicated in diagram above  
 $\downarrow$  then

$$\begin{aligned}
 \dot{S}_i &= R_1 & (1) \\
 \dot{C}_i &= R_1 + R_2 & (2) \\
 \dot{P}_i &= -R_1 + R_3 & (3) \\
 \dot{P}_e &= -R_3 + R_4 & (4) \\
 \dot{S}_e &= -R_4 & (5) \\
 \dot{C}_e &= -R_4 - R_2 & (6)
 \end{aligned}$$

$$c_i + c_e + p_i + p_e :$$

Add (2) (6) (3) (4)

$$\Rightarrow (c_i + c_e + p_i + p_e) = \begin{matrix} R_1 + R_2 & -R_4 - R_2 \\ -R_1 + R_3 & -R_3 + R_4 \end{matrix} = 0$$

So  $c_i + c_e + p_i + p_e$  is constant

$$(s_i + s_e + p_i + p_e) = [(1) + (5) + (3) + (4)] \\ R_1 - R_4 - R_1 + R_3 - R_3 + R_4 = 0$$

So  $s_i + s_e + p_i + p_e = \text{constant}$

$p_i, c_i, p_e, c_e$  quasi-steady

$$\Rightarrow R_1 + R_2 = -R_1 + R_3 = -R_3 + R_4 = -R_4 = R_2 = 0$$

$$\Rightarrow \underline{R_1 = -R_2 = R_3 = R_4}$$

(c)  $k_{\pm} \rightarrow \epsilon k_{\pm} :$

$$R_1 = \epsilon [-k_+ s_i c_i + k_- p_i]$$
$$R_4 = \epsilon [-k_- p_e + k_+ s_e c_e]$$
$$R_2 = k_4 c_e - k_3 c_i$$
$$R_3 = -k_1 p_i + k_2 p_e$$

we have  $\dot{s}_e = -R_4 = -\epsilon [k_+ s_e c_e - k_- p_e]$

So approximately

$$c_i = \frac{k_4}{k_3} c_e, \quad k_2 \cdot p_i = \frac{k_2}{k_1} p_e \quad (*)$$

Also  $c_i + c_e + p_i + p_e = \text{constant}$   
 $s_i + s_e + p_i + p_e = \text{constant}$

$$\text{and } \dot{s}_e = \epsilon [k_- p_e - k_+ c_e s_e]$$

The sneaky bit here is to spot that with  $R_1 \approx R_4$

$$\dot{s}_i + \dot{s}_e = R_1 - R_4 \approx 0$$

So  $s_i + s_e \approx \text{constant}$   
 $\rightarrow p_i + p_e \approx \text{constant} \Rightarrow p_i, p_e \text{ constant}$   
 $\rightarrow c_i + c_e \approx \text{constant} \Rightarrow c_i, c_e \text{ constant}$  } (due to (\*))

So the  $\dot{s}_e = \epsilon [k_- p_e - k_+ c_e s_e]$  is a single equation for  $s_e$ .

$s_e$   
mmmmmm  
uuuuuu  
 $s_i$

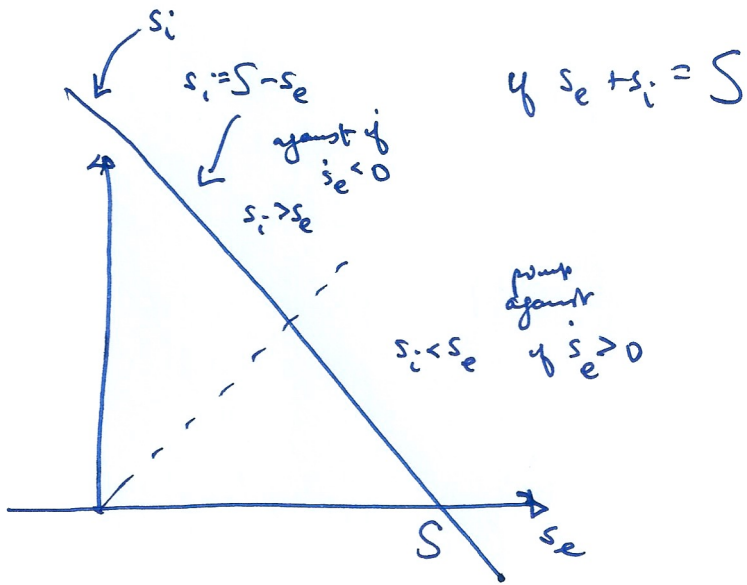
(ii) The pump acts again's w/s gradient  
of  $\dot{s}_e > 0$  when  $s_e > s_i$

well this is obviously double depend on values of

$$s_i + s_e = S, \quad p_i + p_e = P, \quad c_i + c_e = C$$

$$\text{since } s_e \rightarrow \frac{k_- p_e}{k_+ c_e} = S_\infty$$

that's the way of



(4)

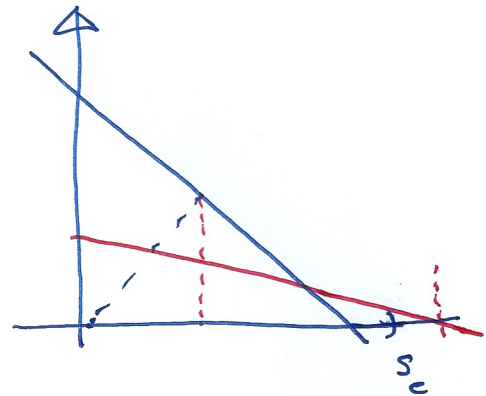
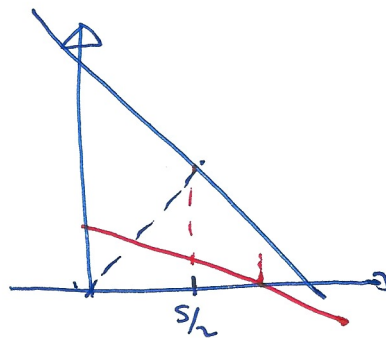
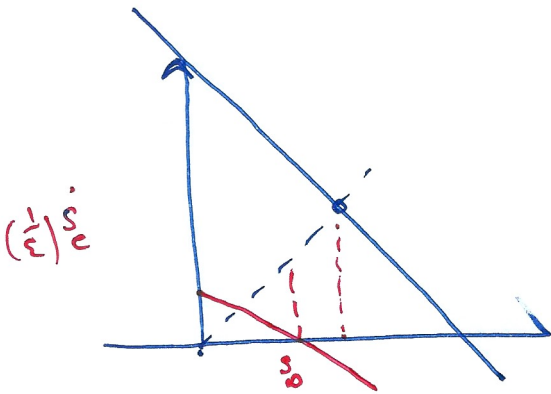
pump is against gradient if  $s_e > 0$  when  $s_e > s_i$   
 or  $s_e < 0$  when  $s_e < s_i$

3 cases

$$s_{\infty} = \frac{h - h_e}{h + c_e} < S/2$$

$$S/2 < s_{\infty} < S$$

$$s_{\infty} > S$$



$s_{\infty} < \frac{1}{2} S$  pump against for  $s_{\infty} < s_e < \frac{1}{2} S$

$\frac{1}{2} S < s_{\infty} < S$  "  $\frac{1}{2} S < s_e < s_{\infty}$

$s_{\infty} > S$  "  $\frac{1}{2} S < s_e < s_{\infty}$

So in all cases pump is against the gradient if  $s_e$  is between  $\frac{1}{2} S$  and  $s_{\infty}$ .

iii Now  $k_3 \rightarrow \epsilon^2 k_3$

$$R_1 = \epsilon [-k_3 s_i c_i + k_1 p_i]$$

$$R_2 = \epsilon [-k_2 p_e + k_4 s_e c_e]$$

$$R_3 = \epsilon [-k_3 c_i + k_4 p_e - \epsilon^2 k_3 c_i]$$

$$R_4 = -k_1 p_i + k_2 p_e$$

$$R_1 \approx -R_2 = R_3 = R_4$$

$$c_i + c_e + p_i + p_e \approx \text{constant}$$

$$s_i + s_e + p_i + p_e \approx \text{constant}$$

As before  $\dot{s}_i + \dot{s}_e \approx R_1 - R_4 \approx 0$

$$s_i + s_e = S \quad \text{constant}$$

$$c_i + c_e = C \quad \text{constant}$$

$$p_i + p_e = P \quad \text{constant}$$

$$R_1, R_4 = O(\epsilon) \Rightarrow R_2, R_3 = O(\epsilon)$$

$$\Rightarrow p_i = \frac{k_2}{k_1} p_e \Rightarrow p_e \approx \text{constant}$$

$$R_2 = O(\epsilon) = c_e = O(\epsilon)$$

$$\Rightarrow c_i \approx C \quad \text{constant}$$

$$\dot{s}_e = -R_4 = \epsilon \left[ \frac{k_2}{k_1} k_2 p_e - k_4 s_e c_e \right] \\ \approx \epsilon \left[ k_2 p_e + O(\epsilon) \right]$$

Depends on  $p_e$ : if  $P = O(\epsilon)$  then it will be eventually ok  
otherwise  $s_e \uparrow$  until  $s_e = O(\frac{1}{\epsilon})$ ,  $\dot{s}_e = \frac{1}{\epsilon} S_e \Rightarrow \dot{s}_e \approx \epsilon \left[ k_2 p_e - k_4 \frac{S_e}{\epsilon} \left( \frac{c_e}{\epsilon} \right) \right]$

6

but then this requires  $\int_e = O(\frac{1}{\epsilon})$   $c_e = \epsilon C_e$

So we would have  $(R_i \rightarrow \epsilon R_i$  wr  $R_k = - \left[ k_{-} P_e + k_{+} \int_e C_e \right]$

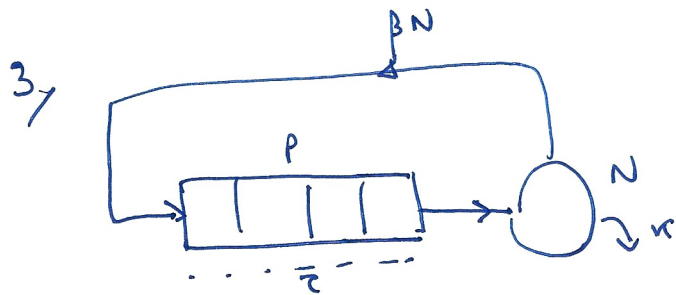
$$\dot{s}_i = \epsilon R_i$$

etc..

This is a WR open-ended since we are not told much about  $S, P$  etc.

Simple answer is it doesn't work straightforwardly.

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$$\dot{p} = -\gamma p + \beta(N)N - e^{-\gamma\tau} \beta(N_\tau)N_\tau$$

$$\dot{N} = -\beta(N)N - \kappa N + 2e^{-\gamma\tau} \beta(N_\tau)N_\tau$$

$$\beta = \beta_0 \exp\left[-N/\beta_1\right]$$

- (a)  $\gamma$  apoptosis rate  
 $\kappa$  rate of recruitment to mitosis

$e^{-\gamma\tau} \beta(N_\tau)N_\tau$  loss to resting phase after passage through mitotic cycle (with delay  $\tau$ )

$2e^{-\gamma\tau} \beta(N_\tau)N_\tau$  2x above through cell division

specific recruitment rate to mitosis decreases with increasing  $N$

- (b) evidently  $\tau \ll \tau$  : scale  $p \sim p_0$ ,  $\kappa N_\tau \sim \beta_1$

$$\Rightarrow \frac{p_0}{\tau} \dot{p} = -\gamma p_0 p + \beta_0 \beta_1 e^{-n} - e^{-\gamma\tau} \beta_0 \beta_1 e^{-n_1} n_1$$

$$\Rightarrow \dot{p} = -\gamma p + \frac{\beta_0 \beta_1 \tau}{p_0} n e^{-n} - \tau \beta_0 \beta_1 e^{-\gamma\tau} \frac{\tau}{p_0} n_1 e^{-n_1}$$

$$\frac{\beta_1}{\tau} \dot{n} = -\beta_0 \beta_1 n e^{-n} - \kappa \beta_1 n + 2e^{-\gamma\tau} \beta_0 \beta_1 n_1 e^{-n_1}$$

$$\Rightarrow \dot{n} = -\beta_0 \tau n e^{-n} - \kappa \tau n + 2\beta_0 \beta_1 \tau e^{-\gamma\tau} n_1 e^{-n_1}$$

and with  $b = e^{-n}$  this is of the requested form if

(2)

$$c_0 = \gamma \tau$$

$$b_0 = \frac{\beta_0 \beta_1 \tau}{\rho_0}$$

$$b_0 e^{-c_0} = \frac{\beta_0 \beta_1 e^{-\gamma \tau} \tau}{\rho_0} = b_0 e^{-\gamma \tau}$$

and  $b_0 = \beta_0 \tau$

$$k_0 = \kappa \tau$$

$$2 e^{-c_0} b_0 = 2 \beta_0 \tau e^{-\gamma \tau}$$

so  $c_0 = \gamma \tau$ ,  $b_0 = \beta_0 \tau$ ,  $\rho_0 = \beta_1$

$k_0 = \kappa \tau$

equilibrium  $n = -b_0 n e^{-n} - k_0 n + 2b_0 e^{-c_0} n_1 e^{-n_1}$

$$n=0 \sim k_0 = \frac{b_0}{e^{-n}} (2e^{-c_0} - 1)$$

$$\Rightarrow n \sim e^n = \frac{(2e^{-c_0} - 1) b_0}{k_0}$$

$\Rightarrow n \neq 0$  if RHS > 1 i.e.  $(2e^{-c_0} - 1) b_0 > k_0$



(c)  $n = n^* + m$

linearized  $\dot{n} = -b_0 n e^{-n} - k_0 n + 2b_0 e^{-c_0} n_1 e^{-n_1}$

define  $g(n) = n e^{-n}$

$\dot{m} = -b_0 g'(m) - k_0 m + 2b_0 e^{-c_0} g'(m_1) m_1$

where  $g' = g'(n^*) = (1 - n^*) e^{-n^*}$

$\Rightarrow \dot{m} = \alpha_1 m - \alpha_2 m_1$

$\alpha_1 = -b_0 g' - k_0$   
 $\alpha_2 = -2b_0 e^{-c_0} g'$

$k_0 = 0.1 \quad b_0 = 4 \quad e^{-c_0} = 0.6$

equilibrium  $e^{n^*} = \frac{(1.2 - 1) 4}{0.1} = 8 \quad n^* = \ln 8 \approx 2$

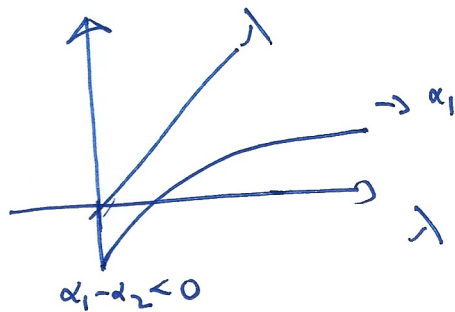
$g' \approx n - 0.125$

$\begin{cases} \alpha_1 \approx 0.4 \\ \alpha_2 \approx 0.6 \end{cases}$

$$(d) \quad u = e^{\lambda t}$$

$$(i) \quad \Rightarrow \lambda = \alpha_1 - \alpha_2 e^{-\lambda} \quad \begin{array}{l} \alpha_1 = 0.4 \\ \alpha_2 = 0.6 \end{array}$$

I. true root?



slope of lines =  $\alpha_2 e^{-\lambda} < \alpha_2 < 1$  for  $\lambda > 0$   
 $\alpha_1 - \alpha_2 < 0 \Rightarrow$  no true root.

II. true real part?

$$\lambda = \alpha_1 - \alpha_2 e^{-\lambda}$$

Since  $\alpha_1 < \alpha_2$ , usual approach doesn't work  
 $[ \text{Re } \lambda > 0 \Rightarrow |\alpha_2 e^{-\lambda}| < \alpha_2, \text{ no good} ]$

If  $\lambda = \lambda_R + i\lambda_I$  then

$$\lambda_R = \alpha_1 - \alpha_2 e^{-\lambda_R} \cos \lambda_I$$

$$\lambda_I = \alpha_2 e^{-\lambda_R} \sin \lambda_I$$

but  $\frac{\sin \lambda_I}{\lambda_I} < 1 \quad \forall \lambda_I$  so  $\lambda_R < 0$  as  $1 = \alpha_2 \frac{\sin \lambda_I}{\lambda_I} e^{-\lambda_R}$

$\Rightarrow \lambda_R < 0$  as  $\alpha_2 < 1$   $\square$ .

ii  $k_0 \downarrow \omega_0 \downarrow \frac{k_0}{\omega_0}$  fixed.

$$e^{nk} = (2e^{-c_0} - 1) \frac{\omega_0}{k_0} \text{ is fixed}$$

$\Rightarrow |g'|$  is fixed

$$\alpha_1 = \omega_0 \left[ |g'| - \frac{k_0}{\omega_0} \right]$$

$$\alpha_2 = 2\omega_0 e^{-c_0} |g'|$$

so  $\alpha_1 \downarrow \alpha_2 \downarrow$  with  $\frac{\alpha_1}{\alpha_2}$  fixed

write  $\alpha_1 = \alpha, \gamma = \frac{\alpha_2}{\alpha_1} \frac{d\alpha_2}{d\alpha_1}$

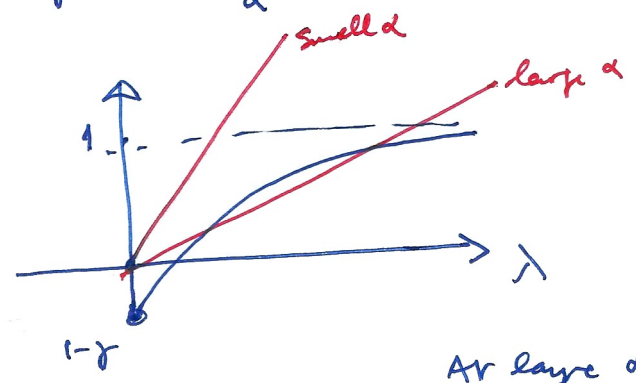
$$\lambda = \alpha [1 - \gamma e^{-\lambda}]$$

for  $\gamma > 1, \lambda = \lambda(\alpha)$ . For  $\alpha = 0.4 \text{ Re } \lambda < 0$

( $\gamma = 1.5$ ).

The argument of part II above shows that  $\Re \lambda < 0$  if  $\lambda$  is complex

$$1 - \gamma e^{-\lambda} = \frac{\lambda}{\alpha}, \lambda \text{ real}, \gamma > 1$$



~~It seems lambda will cross~~  
~~lambda to lambda > 0~~

??  
∴ lambda never crosses zero

At large  $\alpha$ , 2 true roots but via two complex roots becoming real

$\Rightarrow$  Hopf bifurcation at earlier (large  $\alpha$ )

Hopf bifurcation?

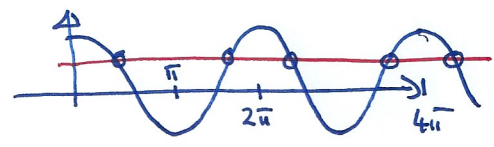
$$\lambda = \alpha [1 - \gamma e^{-\lambda}]$$

vary  $\alpha$   $\lambda = i\theta$

$$i\theta = \alpha [1 - \gamma e^{-i\theta}]$$

$$0 = 1 - \gamma \cos \theta$$

$$\theta = \arcsin \frac{\alpha \gamma}{\gamma}$$



$$\theta = \cos^{-1} \frac{1}{\gamma} \text{ for } \gamma > 1$$

or with  $\phi = \cos^{-1} \frac{1}{\gamma} \in (0, \pi/2)$

$$\theta = 2n\pi \pm \phi \quad n=0, 1, \dots$$

$$\alpha = \frac{\theta}{\gamma \sin \theta}$$

gives sequence of increasing  $\alpha$  values

$$\alpha_n = \frac{2n\pi + \phi}{\gamma \sin \phi} = \frac{2n\pi + \phi}{(\gamma^2 - 1)^{1/2}}$$

$$\text{first is } \alpha_0 = \frac{\cos^{-1} \frac{1}{\gamma}}{\sqrt{\gamma^2 - 1}}$$

with  $\gamma = 1.5$

$$\alpha_0 = 0.75$$

Transversality  $\lambda(\alpha)$

$$\lambda' = 1 - \gamma e^{-\lambda} + \alpha \gamma e^{-\lambda} \lambda'$$
$$= \frac{\lambda}{\alpha} + (\alpha - \lambda) \lambda'$$

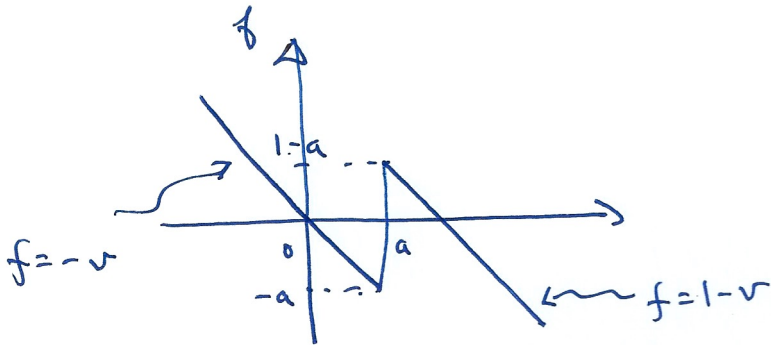
$$\text{so } \lambda' = \frac{\lambda}{\alpha(1 - \alpha + \lambda)} \text{, at } \lambda = i\theta \text{, } \lambda' = \frac{i\theta [1 - \alpha - i\theta]}{\alpha [(1 - \alpha)^2 + \theta^2]}$$

$\Rightarrow \text{Re} \lambda' = \frac{\theta^2}{\alpha [(1 - \alpha)^2 + \theta^2]} > 0$  so Hopf as  $\alpha$  increases through

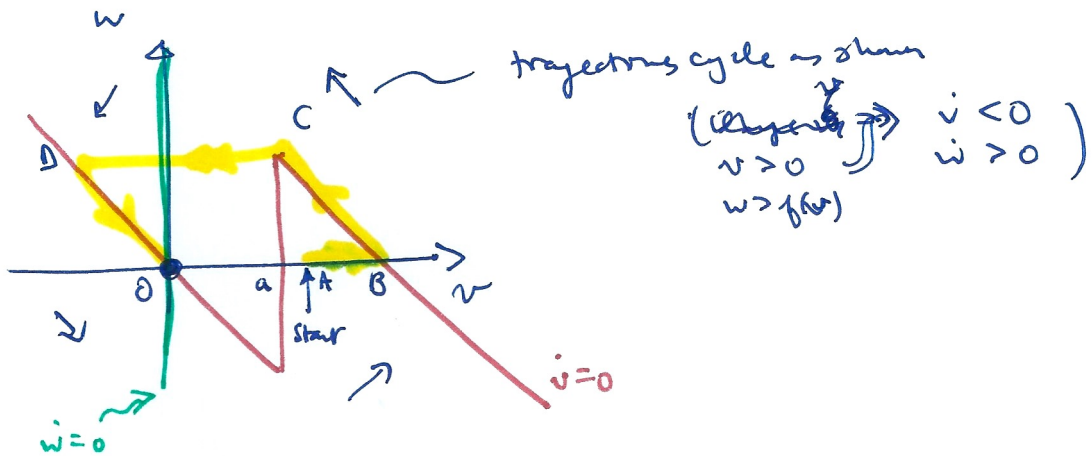
$$\cos^{-1} \frac{1}{\gamma} = 0.75$$
$$\sqrt{\gamma^2 - 1} \text{ not } \rightarrow \alpha \downarrow$$

CS.12 Math Physics 2015 Q1 answer.

1, (a)  $\epsilon \dot{v} = f(v) - w$   
 $\dot{w} = v$



(i)  $v$  electrical potential etc  
 $w$  gate variable etc



$(0,0)$  unique equilibrium

Near  $(0,0)$   $\begin{pmatrix} \dot{v} \\ \dot{w} \end{pmatrix} \approx \underbrace{\begin{pmatrix} -\frac{1}{\epsilon} & -1 \\ 1 & 0 \end{pmatrix}}_M \begin{pmatrix} v \\ w \end{pmatrix}$  det

$\det M = 1$   
 $\text{tr } M = -\frac{1}{\epsilon}$   
 $\Rightarrow$  stable

Starting at A  $(v^k, 0)$   $v^k > a$  trajectory is as

- shown: ABCDO : AB fast to  $v$  will be as  $\epsilon \ll 1$
- BC slow
- CD fast
- DO slow

$\Rightarrow$  steady state is excitable

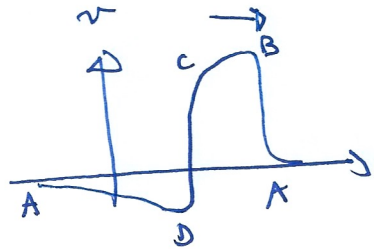
(4b)

$$\epsilon v_t = \epsilon^2 v_{xx} + f(v) - w$$

$$w_t = v$$

$$y = x - ct, \quad c > 0$$

$$v = v(y), \quad w = w(y)$$



(i)

$$-\epsilon c v' = \epsilon^2 v'' + f(v) - w$$

$$-c w' = v$$

(ii)

$$y = \epsilon \eta \Rightarrow -c v' = v'' + f(v) - w$$

in front AB

$$w' = \epsilon v$$

$$\Rightarrow w' \approx 0 \Rightarrow w \approx 0 \quad (w \rightarrow 0 \text{ as } \eta \rightarrow \infty)$$

$$\Rightarrow v'' + c v' + f(v) = 0$$

bc  $v \rightarrow 0$  as  $\eta \rightarrow \infty$

$v \rightarrow 1$  (only <sup>other</sup> physically stable steady state) as  $\eta \rightarrow -\infty$

iii

we have to get from  $v=1$  at  $y=-\infty$   
to  $v=0$  at  $y=+\infty$

$$\text{for } v > a \quad v'' + cv' + 1 - v = 0$$

$$f = 1 - v$$

solutions exponential

$$f = 1 - v \propto e^{\lambda y}$$

$$-\lambda^2 - c\lambda + 1 = 0$$

$$\lambda^2 + c\lambda - 1 = 0$$

$$\lambda = \frac{1}{2} [c \pm \{c^2 + 4\}^{1/2}] = \lambda_{\pm} \quad \begin{array}{l} \lambda_+ > 0 \\ \lambda_- < 0 \end{array}$$

we need  $\lambda > 0$  so  $1 - v \rightarrow 0$  as  $y \rightarrow -\infty$

$$\Rightarrow 1 - v = e^{\lambda_+ y} \quad (\text{coeff} = 1 \text{ wlog as just fixes origin})$$

$$\text{At } v = a \text{ at } y = \frac{1}{\lambda_+} \ln(1 - a) = y_a$$

$$\hookrightarrow v' = -\lambda_+ e^{\lambda_+ y} a = -\lambda_+ (1 - a)$$

for  $v < a$   $v'' + cv' - v = 0$  solutions  $e^{\lambda_{\pm} y}$  as before

~~obvious~~ we need  $\lambda_-$  so  $v \rightarrow 0$  as  $y \rightarrow \infty$   
thus require  $v = a e^{\lambda_- (y - y_a)}$

$$\hookrightarrow v' \text{ cts so } \lambda_- a = -\lambda_+ (1 - a)$$

$$\text{or } \frac{1}{2} [c + (c^2 + 4)^{1/2}] a = \frac{1}{2} [-c + (c^2 + 4)^{1/2}] (1 - a)$$

$$\text{So } ca + c(1-a) = -(c^2+4)^{\frac{1}{2}}a + (c^2+4)^{\frac{1}{2}}(1-a)$$

(4)

~~$$c(2-a) = (c^2+4)^{\frac{1}{2}}a$$~~

$$\Rightarrow c = (c^2+4)^{\frac{1}{2}}(1-2a) \quad \text{requires } a < \frac{1}{2} \text{ for } c > 0$$

$$\Rightarrow c^2 = (c^2+4)(1-2a)^2$$

~~$$= c^2(1-2a)^2 + 4(1-2a)^2$$~~

~~$$c^2 = \frac{4(1-2a)^2}{1 - (1-2a)^2}$$~~

$$c^2 [1 - (1-2a)^2] = 4(1-2a)^2$$

$$c^2 [4a - 4a^2]$$

$$\text{So } c = \frac{1-2a}{[a(1-a)]^{\frac{1}{2}}}$$

(iv) well come as you already told us  $c$  was true

anyway what he wants is

$$v'' + cv' + f(v) = 0$$

$$\frac{1}{2}v'^2 \Big|_{-a}^{\infty} + c \int_{-a}^{\infty} v' \, dy + \int_1^0 f(v) \, dv = 0$$

$$\text{ie } c = \frac{\int_0^1 f(v) \, dv}{\int_{-\infty}^{\infty} v' \, dy}$$

$$\geq 0 \text{ if } \int_0^1 f(v) \, dv \geq 0$$

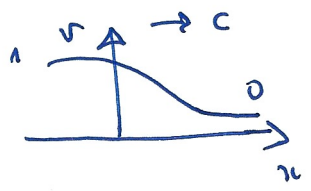
evidently if  $a \leq \frac{1}{2}$

(this sign is wrong)



2/

$$\epsilon v_t = \epsilon^2 \nabla^2 v + f(v), \quad A = Av(v-a)(1-v)$$



(a)  $\underline{x} = \underline{x}(\underline{X}, t)$  Jacobian  $\frac{\partial \underline{x}}{\partial \underline{X}} = \underline{J}$ ,  $J_{ij} = \frac{\partial x_i}{\partial X_j}$

inverse is  $\underline{X} = \underline{X}(\underline{x}, t)$  Jacobian  $(=J^{-1}) = \underline{K}$ ,  $K_{ij} = \frac{\partial X_i}{\partial x_j}$

note  $\underline{JK} = \underline{I}$ .

$$\underline{e}_i = \frac{\partial \underline{x}}{\partial X_i}$$

(i) Since  $X_2$  &  $X_3$  define local cartesian coordinates in the interface, if we assume  $\underline{X}$  is an orthogonal system, then  $X_1$  is normal to the interface, so at  $X_1 = 0$  (in the interface)  $\underline{e}_1$  is normal to the interface.

(ii) we have  $\frac{\partial v}{\partial t} \Big|_{\underline{x}} = \frac{\partial v}{\partial t} \Big|_{\underline{X}} + \frac{\partial x_i}{\partial t} \Big|_{\underline{X}} \frac{\partial v}{\partial x_i}$  ( $v(\underline{x}, t) = v[\underline{x}(\underline{X}, t), t]$ )  
 ( $\dots v(\underline{X}, t)$ )

Also  $\frac{\partial}{\partial x_i} = \frac{\partial X_j}{\partial x_i} \frac{\partial}{\partial X_j} = K_{ji} \frac{\partial}{\partial X_j}$  (use summation convention)

so  $\frac{\partial v}{\partial x_i} = K_{ji} \frac{\partial v}{\partial X_j}$   
 $\nabla^2 v = \frac{\partial^2 v}{\partial x_i \partial x_i} = \frac{\partial}{\partial x_i} \left[ K_{ji} \frac{\partial v}{\partial X_j} \right] = K_{ki} \frac{\partial}{\partial X_k} \left[ K_{ji} \frac{\partial v}{\partial X_j} \right]$

$$= K_{ki} K_{ji} \frac{\partial^2 v}{\partial X_j \partial X_k} + K_{ki} \frac{\partial K_{ji}}{\partial X_k} \frac{\partial v}{\partial X_j}$$

So the equation is  $(v = v(\underline{x}, t))$ ,  $\frac{\partial v}{\partial x_i} = k_{ji} \frac{\partial v}{\partial x_j}$

$$\epsilon v_t = \epsilon \frac{\partial x_i}{\partial t} \Big|_{\underline{x}} \frac{\partial v}{\partial x_j} + \epsilon^2 \left[ k_{ki} k_{ji} \frac{\partial^2 v}{\partial x_j \partial x_k} + k_{ki} \frac{\partial k_{ji}}{\partial x_k} \frac{\partial v}{\partial x_j} \right]$$

Note  $k_{ki} \frac{\partial k_{ji}}{\partial x_k} = \frac{\partial x_k}{\partial x_i} \frac{\partial k_{ji}}{\partial x_k} = \frac{\partial k_{ji}}{\partial x_i}$

in particular  $\frac{\partial k_{ii}}{\partial x_i} = \frac{\partial}{\partial x_i} \left[ \frac{\partial x_1}{\partial x_i} \right]$

note also  $\underline{\nabla} \cdot \underline{x}_1$  is the normal to the interface

thus  $\frac{\partial k_{ii}}{\partial x_i} = \underline{\nabla} \cdot [\underline{\nabla} x_1]$

we can assume (otherwise rescale  $x_1$ ) that in fact  $\underline{\nabla} \cdot \underline{x}_1 = \underline{n}$  (unit normal)

then  $n_i = k_{ii}$  and  $\underline{k}_{ii} \underline{k}_{ii} = 1$

$$\text{So } \epsilon v_t = \epsilon \frac{\partial x_i}{\partial t} \Big|_{\underline{x}} k_{ji} \frac{\partial v}{\partial x_j} + \epsilon^2 k_{ki} k_{ji} \frac{\partial^2 v}{\partial x_j \partial x_k} + \epsilon \frac{\partial k_{ji}}{\partial x_i} \frac{\partial v}{\partial x_j}$$

Next we assume  $v$  changes rapidly with  $x_1$ ,  $x_1 = \epsilon \xi$

then to leading order

$$0 = \frac{\partial x_i}{\partial t} \Big|_{\underline{x}} \underbrace{k_{ii}}_{=1} \frac{\partial v}{\partial \xi} + \underbrace{k_{ii} k_{ii}}_{=1} \frac{\partial^2 v}{\partial \xi^2} + \epsilon \underbrace{\frac{\partial k_{ii}}{\partial x_i}}_{\underline{\nabla} \cdot \underline{n}} \frac{\partial v}{\partial \xi} + f(v)$$

$$\Rightarrow 0 = v_{\xi\xi} + \left[ \underbrace{\frac{\partial x_i}{\partial t} \Big|_{\underline{x}}}_{u_n} + \epsilon \underline{\nabla} \cdot \underline{n} \right] v_{\xi} + f(v)$$

*u<sub>n</sub> normal velocity of front*

and we know that the solution of this is  $V(\frac{r}{\epsilon})$  satisfying

$$V'' + cV' + f(V) = 0$$

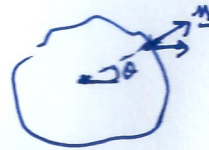
Therefore

$$\underbrace{\eta \cdot \frac{\partial \eta}{\partial t}}_{u_n} + \epsilon \nabla \cdot \eta = c$$

(i)  $\eta \cdot \frac{\partial \eta}{\partial t}$  is wave front speed  
 $\nabla \cdot \eta$  is curvature

(b) the wave front is at  $r = R(t, \theta)$

$$\begin{aligned} \text{So } x &= R \cos \theta \\ y &= R \sin \theta \end{aligned}$$



$$\underline{n} \propto (dy, -dx)$$

$$\propto (R' \sin \theta + R \cos \theta, -R' \cos \theta + R \sin \theta)$$

$$\text{So } \underline{n} = \frac{(R' \sin \theta + R \cos \theta, -R' \cos \theta + R \sin \theta)}{\sqrt{(R'^2 + R^2)^{3/2}}}$$

$$[R'^2 \sin^2 \theta + R^2 \cos^2 \theta + 2RR' \sin \theta \cos \theta + R'^2 \cos^2 \theta + R^2 \sin^2 \theta + 2RR' \sin \theta \cos \theta]$$

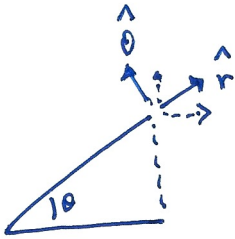
$$= \frac{(R' \sin \theta + R \cos \theta, -R' \cos \theta + R \sin \theta)}{(R'^2 + R^2)^{3/2}}$$

$$(R'^2 + R^2)^{3/2}$$

$$\frac{\partial x}{\partial t} = R_t (\cos \theta, \sin \theta)$$

$$\text{So } \eta \cdot \frac{\partial \eta}{\partial t} = \frac{R_t [R' \sin \theta \cos \theta + R \cos^2 \theta - R' \sin \theta \cos \theta + R \sin^2 \theta]}{(R'^2 + R^2)^{3/2}}$$

$$= \frac{RR_t}{(R'^2 + R^2)^{3/2}}$$



In Cartesian coordinates

$$\underline{n} = \frac{(R' \sin \theta + R \cos \theta, -R' \cos \theta + R \sin \theta)}{(R^2 + R'^2)^{3/2}}$$

we want this in cylindrical polars

$$\text{note } \hat{r} = i \cos \theta + j \sin \theta$$

$$\hat{\theta} = -i \sin \theta + j \cos \theta$$

$$\text{so } i = \hat{r} \cos \theta - \hat{\theta} \sin \theta$$

$$j = \hat{r} \sin \theta + \hat{\theta} \cos \theta$$

$$\underline{n} = \frac{1}{(R^2 + R'^2)^{3/2}} \left[ (R' \sin \theta + R \cos \theta) \cos \theta + (-R' \cos \theta + R \sin \theta) \sin \theta, \right. \\ \left. -(R' \sin \theta + R \cos \theta) \sin \theta + (-R' \cos \theta + R \sin \theta) \cos \theta \right]$$

$$= \frac{1}{(R^2 + R'^2)^{3/2}} [R, -R']$$

$$\nabla \cdot \underline{n} = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{R}{(R^2 + R'^2)^{3/2}} \right) + \frac{1}{r} \frac{\partial}{\partial \theta} \left[ \frac{-R'}{(R^2 + R'^2)^{3/2}} \right]$$

$$\text{or } r=R, = \frac{1}{R} \left[ \frac{R}{(R^2 + R'^2)^{3/2}} - \frac{R''}{(R^2 + R'^2)^{3/2}} + \frac{R'(RA' + R'R'')}{(R^2 + R'^2)^{3/2}} \right]$$

$$= \frac{1}{R(R^2 + R'^2)^{3/2}} \left[ R(R^2 + R'^2) - R''(R^2 + R'^2) + RR' + R'R'' \right]$$

$$= \frac{1}{R(R^2 + R'^2)^{3/2}} [R^3 + 2RR'^2 - R^2R'']$$

$$= \frac{R^2 + 2R'^2 - RR''}{(R^2 + R'^2)^{3/2}}$$

show

(5)

$$\text{So } c = \frac{RR_f}{(R^2 + R'^2)^{3/2}} + \frac{\epsilon (R^2 + 2R'^2 - RR'')}{(R^2 + R'^2)^{3/2}}$$

$$\text{or } R_f = \frac{c(R^2 + R'^2)^{3/2}}{R} - \frac{\epsilon (R^2 + 2R'^2 - RR'')}{R(R^2 + R'^2)}$$

( $\epsilon' = R'(0)$   
 $\rightarrow \frac{\partial R}{\partial t}$ )

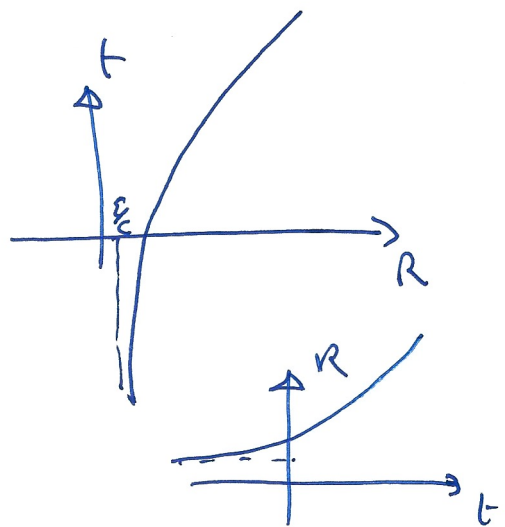
!!!

$$(ii) \quad R = R(t) \quad \Rightarrow \quad \dot{R} = c - \frac{\epsilon}{R} = \frac{cR - \epsilon}{R}$$

$$\text{So } \frac{R\dot{R}}{cR - \epsilon} = 1$$

$$= \frac{R - \frac{\epsilon}{c} + \frac{\epsilon}{c}}{c(R - \frac{\epsilon}{c})}$$

$$\Rightarrow ct = R + \frac{\epsilon}{c} \ln\left(R - \frac{\epsilon}{c}\right)$$



So I suppose curvature blocking refers to the fact that it doesn't work for small  $R$  (curvature too large)

ii) seems a bit long...

$$r = R(t) + p \quad p(0, t) \text{ small}$$

$$\text{so } \dot{R} + \dot{p}_t = \frac{c(R^2 + 2Rp \dots)^k}{(R+p)} + \frac{\epsilon [Rp_{00} \dots - R^2 - 2Rp \dots]}{(R+p)(R^2 + 2Rp \dots)}$$

x by R+p

$$R\dot{R} + Rp_t + R\dot{p} \dots = cR(1 + \frac{2p}{R} \dots)^k - \epsilon + \frac{\epsilon}{R} p_{00} \dots$$

O(1) cancel so  $(R\dot{R} = cR - \epsilon)$

$$Rp_t + R\dot{p} = \frac{\epsilon}{R} p_{00} + \dots$$

$$\& R\dot{R} = c - \frac{\epsilon}{R} \quad \text{so } R\dot{p} = \frac{\epsilon}{R}(p + p_{00})$$

$$\& \text{ solutions are } p = \sum_m e^{im\theta} p_m(t)$$

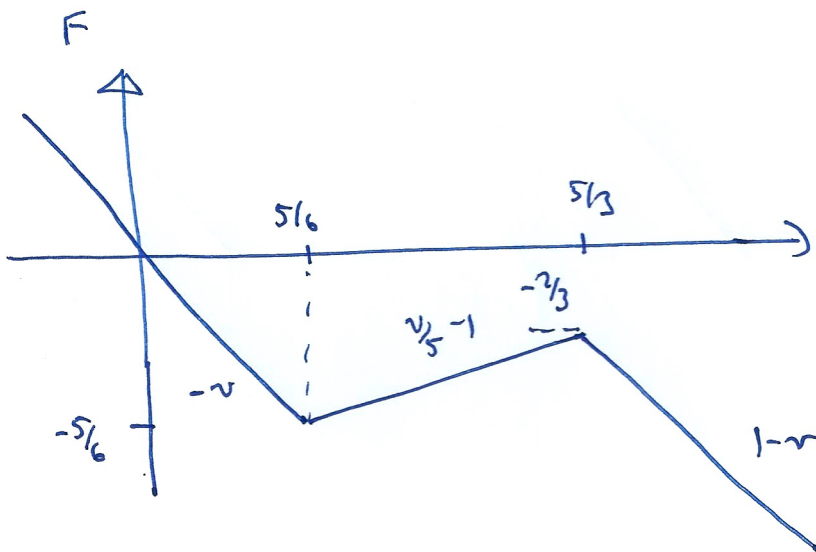
( $m \neq 0$  as we can take mean of  $p$  to be 0 w.l.o.g.)

$$\Rightarrow R\dot{p}_m = \frac{\epsilon}{R}(p_m - m^2 p_m) = -\frac{\epsilon}{R}(m^2 - 1)p_m$$

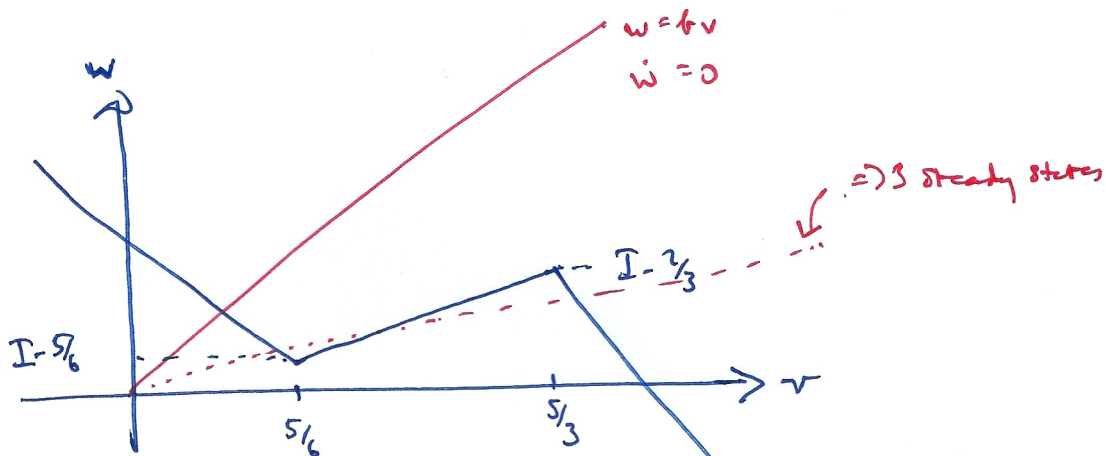
so  $|m| > 1$  decay  
 $|m| = 1$  neutrally stable apparently

(modulo algebra)

(a)  $\Sigma v = I + f(v) - w$   
 $\dot{w} = -w + bv$   $I > 5/6$



- i v intracellular electric potential
- w gate variable for channel conductance
- I applied current

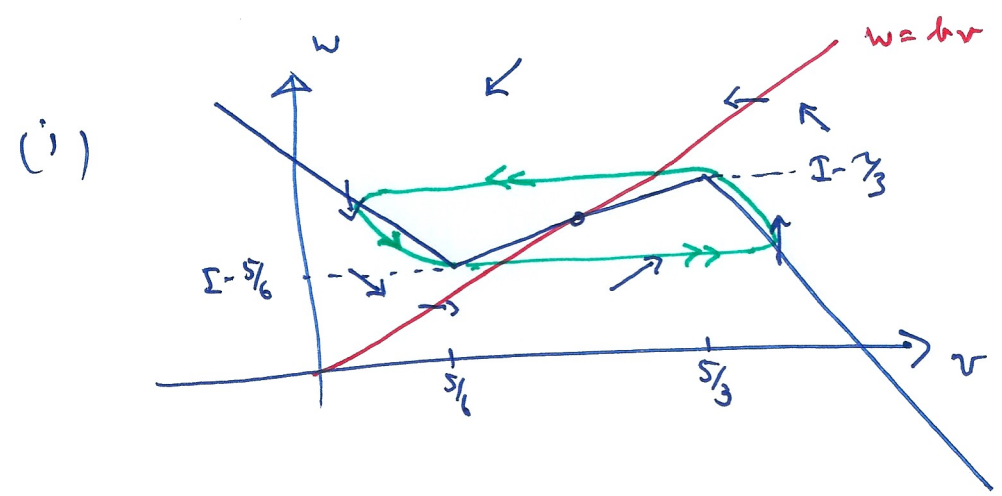


The dotted line indicates 3 steady states if  $b < 1/5$  and

$\frac{5}{6}b > I - \frac{5}{6}$  and  $\frac{5}{3}b < I - \frac{2}{3}$   
 $\frac{5b+12}{3} < I < \frac{5b+5}{6}$  (which requires  $b < 1/5$ )

$w = I + f(v) - w$   
 $\dot{v} = 0$

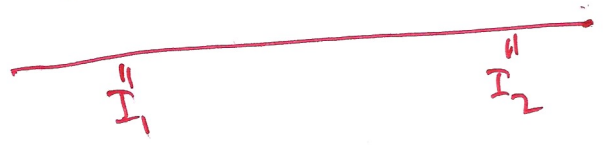
(b) | steady state  $\frac{5}{6} < v^* < \frac{5}{3}$  requires



steady exists for

$$\frac{5}{6}b < I - \frac{5}{6} < \frac{5}{3}b > I - \frac{7}{3}$$

or  $\frac{5}{6}(b+1) < I < \frac{5b+2}{3}$  (note  $b > \frac{1}{3}$ )



At large w  $v < 0$   $\dot{w} < 0$  so trajectory directed as for arrows above in diagram

$\Rightarrow$  fixed point is node or spiral.

$\epsilon \ll 1 \Rightarrow$  relaxation oscillates as indicated in green above

$\Rightarrow$  steady state is unstable

(but to do it formally, unstable if  $\text{tr} M = T > 0$ )

( $\det M > 0$  as not a saddle)

$$M = \begin{pmatrix} F'_{1/2} - 1/2 \\ b - 1 \end{pmatrix} \quad \text{tr} M = \frac{F'}{\epsilon} - 1 > 0 \text{ as } \epsilon \ll 1 \ \&F' > 0.$$

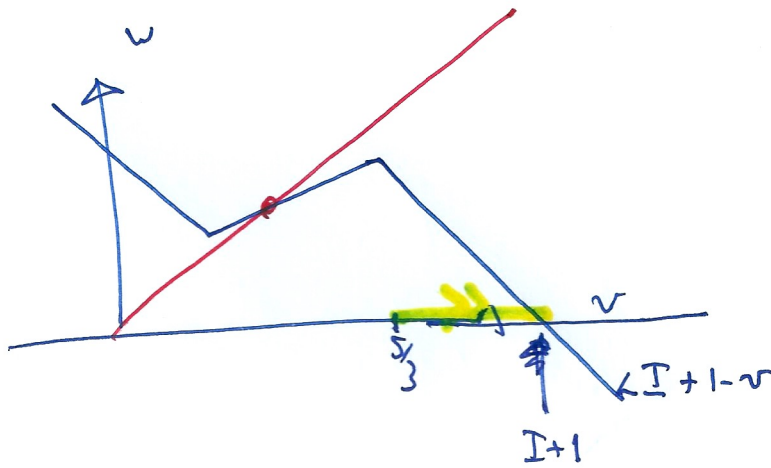


Depends on  $\varepsilon f(b)$ ? This is a bit vague as we are told  $\varepsilon \ll 1$ . (3)

$$T = \frac{1}{\varepsilon} \frac{1}{\varepsilon - 1} \text{ so unstable for } \varepsilon < 0.2.$$

only depends on  $b$  if steady state not on middle branch.

iii



Start at  $(\frac{5}{3}, 0)$  in yellow

$$t = \varepsilon \tau \quad v' = I + f(v) - w$$

$$w' = \varepsilon [-w + b]$$

$$\Rightarrow w \approx 0, \quad v' \approx I + f(v) = I + 1 - v$$

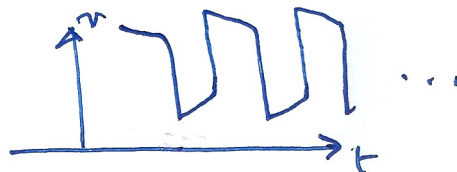
$$v \rightarrow \underline{I+1}$$

iv Already done in (i) :  $v$  relaxes to  $v$  will die rapidly

$w$  tracks slowly as  $v$  will die towards red

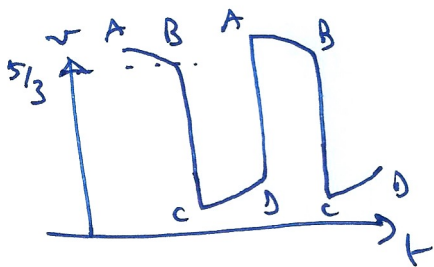
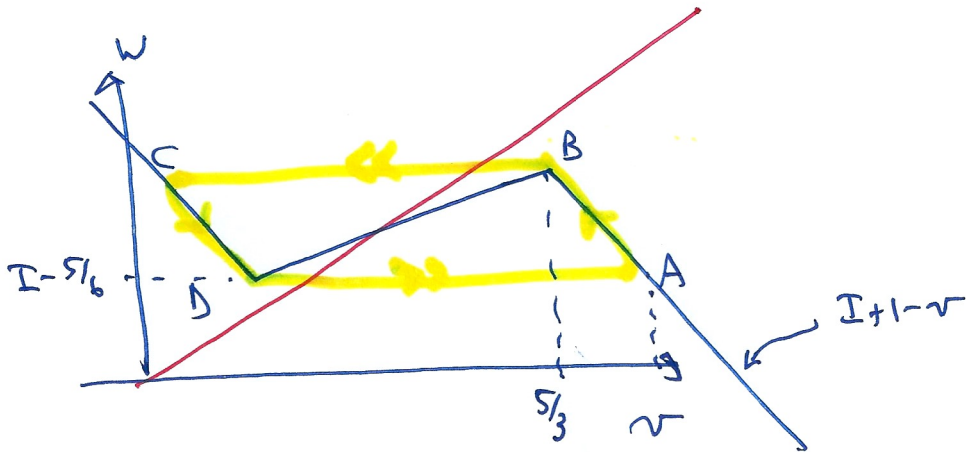
$w$  will die but can't stay as  $v$  will die so hops rapidly

to other branch



(4) 254

$T = \text{length of time } v > 5/3 \text{ in orbit:}$



$$T = \int_A^B dt = \int_A^B \frac{dw}{\dot{w}} = \int_A^B \frac{dw}{-w + b + v}$$

and  $w = I + 1 - v$

$$\text{so } T = \int_A^B \frac{-dv}{bv + v - (I+1)}$$

At A  $I + 1 - v = I - 5/6 \Rightarrow v = 11/6$

At B  $v = 5/3$

$$\Rightarrow T = \int_{11/6}^{5/3} \frac{-dv}{(b+1)v - (I+1)}$$

$$= \frac{1}{b+1} \ln \left[ (b+1)v - (I+1) \right]_{5/3}^{11/6}$$

$$= \frac{1}{b+1} \ln \left[ \frac{\frac{11}{6}(b+1) - I - 1}{\frac{5}{3}(b+1) - I - 1} \right] = \frac{1}{b+1} \ln \left[ \frac{11b + 5 - 6I}{2(5b + 2 - 3I)} \right]$$

C5-12

Math Physiol 2016 Q2

(1)

2,

$$u_t + \gamma v_t = 1 - u + \epsilon u_{xx}$$

$$\epsilon v_t = -v + g(u)$$



(a)  $v$  is the  $Ca^{2+}$ -sensitive store in the cell (sarcoplasmic reticulum)

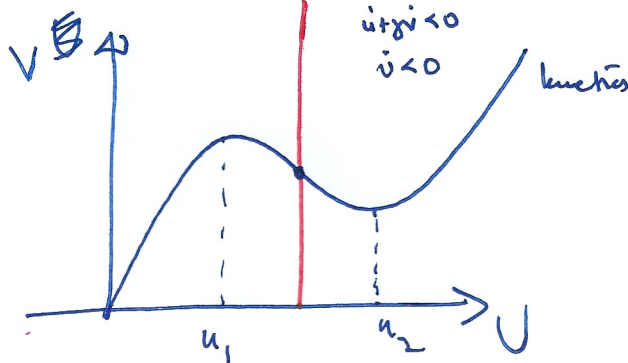
$u$  is the cytosolic  $Ca^{2+}$  concentration in the cell.

(b)  $u = U(\xi) \quad v = V(\xi) \quad \xi = x + st$

$$\Rightarrow s(U' + \gamma V') = 1 - U + \epsilon U''$$

$$\epsilon s V' = -V + g(U)$$

$(U, V)$  phase plane



Question a bit imprecise - periodic travelling waves?

solitary travelling waves?

~~periodic travelling waves~~

kines:

$$u_t + \gamma v_t = 1 - u$$

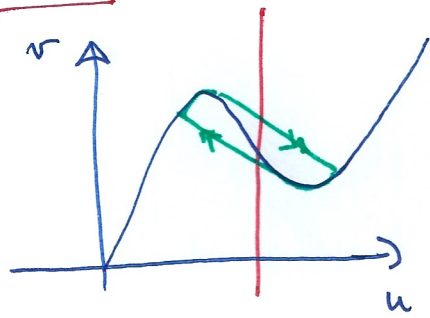
$$\epsilon v_t = -v + g(u)$$

sa

See below (p3) for wave trajectory

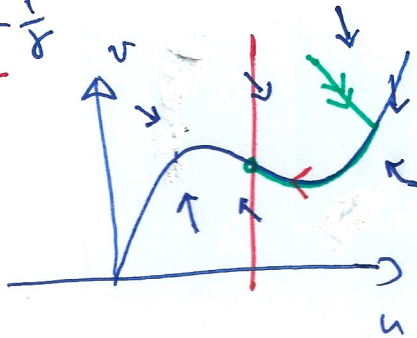
Discussion: whether the steady state is stable or unstable (2)  
 probably depends on whether  $g' \geq -\frac{1}{\delta}$  at the fixed point

if  $g' < -\frac{1}{\delta}$  ( $-g' \geq \frac{1}{\delta}$ )



we get oscillations

if  $g' > -\frac{1}{\delta}$



fixed point is stable

[Warning: see p2A for phase plane discussion]

Linearization  $\dot{u} = 1 - u - \frac{\delta}{\epsilon} [-v + g(u)]$

$\dot{v} = \frac{1}{\epsilon} [-v + g(u)]$

Near fixed pt community matrix is  $M = \begin{pmatrix} -1 - \frac{\delta g'}{\epsilon} & \frac{\delta}{\epsilon} \\ \frac{g'}{\epsilon} & -\frac{1}{\epsilon} \end{pmatrix}$

Phase plane indicates not saddle

fixed pt unstable iff  $\text{tr} M > 0$

$\Rightarrow -\frac{\delta g'}{\epsilon} - \frac{1}{\epsilon} \geq 0$

$\Rightarrow -g' \geq \frac{1}{\delta}$

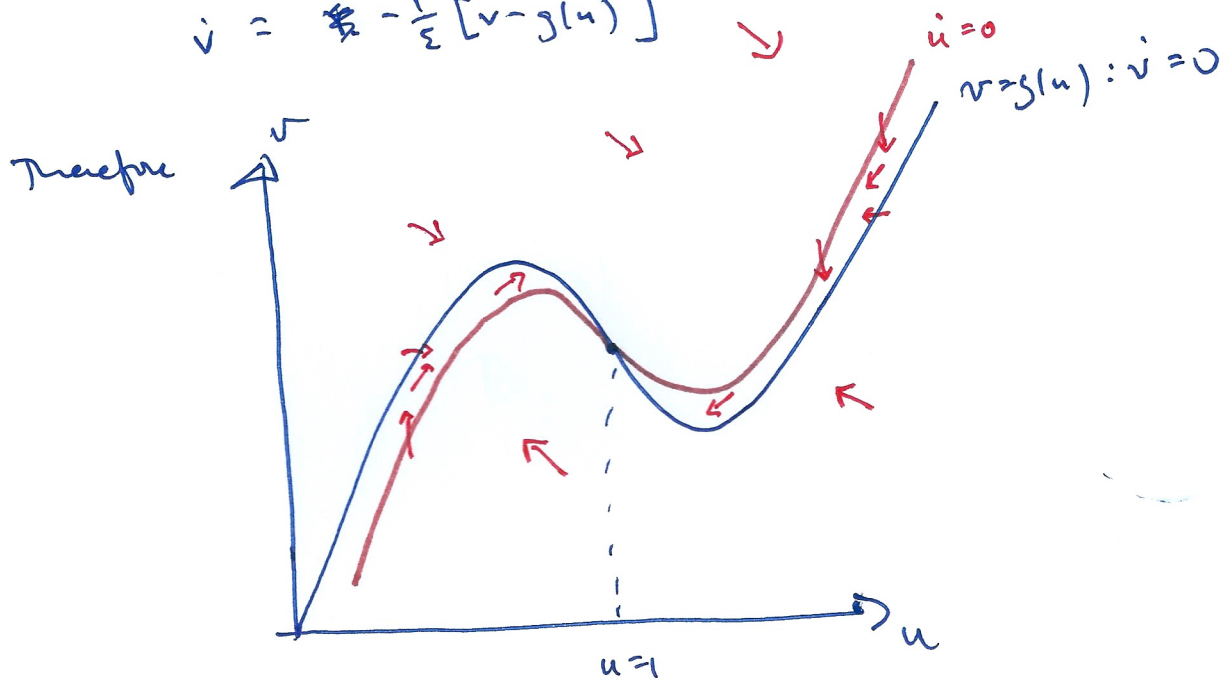
[ Further discussion and salutary warning:

if you look at the trajectory directions in  $\mathbb{R}^2$   
it looks as if  $\dot{u} = 0$  on  $v = g(u)$  instead of  $\dot{v} = 0$  !?

In more detail:

$$\dot{u} = 1 - u + \frac{\gamma}{\varepsilon} [v - g(u)]$$

$$\dot{v} = \frac{\gamma}{\varepsilon} - \frac{1}{\varepsilon} [v - g(u)]$$



actual nullclines for  $u$  &  $v$  are

$$\dot{v} = 0 \quad v = g(u) \quad (\text{blue})$$

$$\dot{u} = 0 \quad v = g(u) + \frac{\varepsilon}{\gamma}(u-1) \quad (\text{brown})$$

and trajectory directions as shown in red

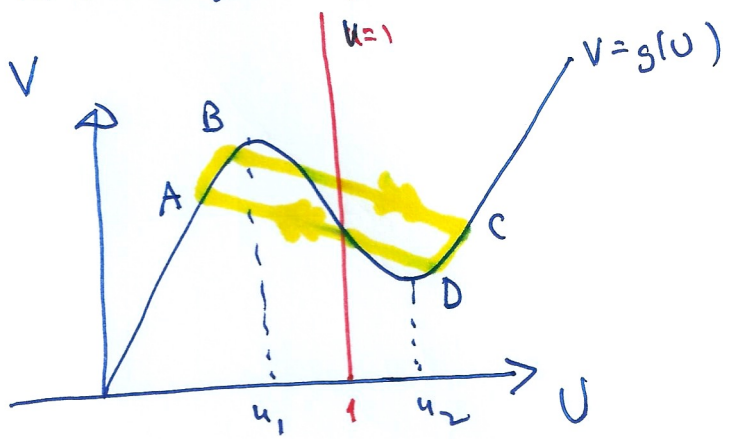
Warning: do not be overly simplistic with phase plane  
- rely on  $\varepsilon \ll 1$

]

The diagram in the question is terrible!

but appears to indicate a solitary wave - but the system is not excitable & so let us assume periodic travelling waves

Then ( $\sim$  Fitzhugh-Nagumo) I guess



(BC & AD not necessarily straight)

we don't know <sup>what</sup> where  $U_B \approx U_A$  are

(c) Fast:  $\xi = \epsilon X$

$$\Rightarrow s(U' + \gamma V') = \epsilon [1 - U] + U''$$

$$sV' = -V + g(U)$$

~~$$\Rightarrow s(U' + \gamma[-V + g(U)]) = U''$$~~

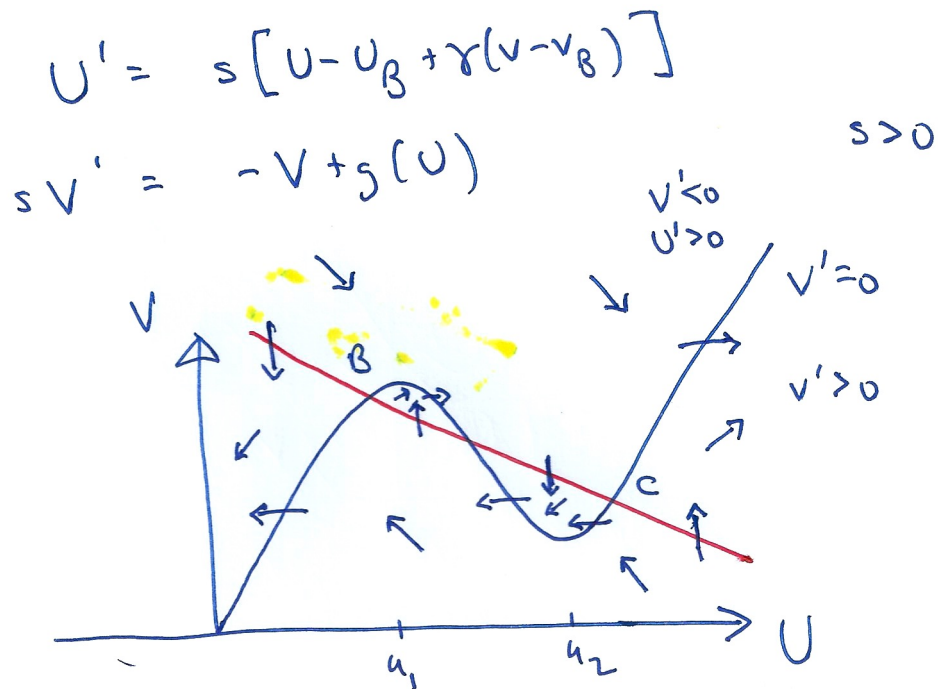
or is  $s(U' + \gamma V') \approx U''$

$$\Rightarrow s[U - U_B + \gamma(V - V_B)] \approx U'$$

( $U \rightarrow U_B, V \rightarrow V_B$   
 $\text{as } X \rightarrow -\infty$ )

~~is not~~ as required

(i) Suitable choice of  $\gamma$  !! We already need to know this! It is  $g'(1) < -\frac{1}{f}$  (so oscillatory kinetics)



Phase portrait: nullclines, directions (above)  
(above)

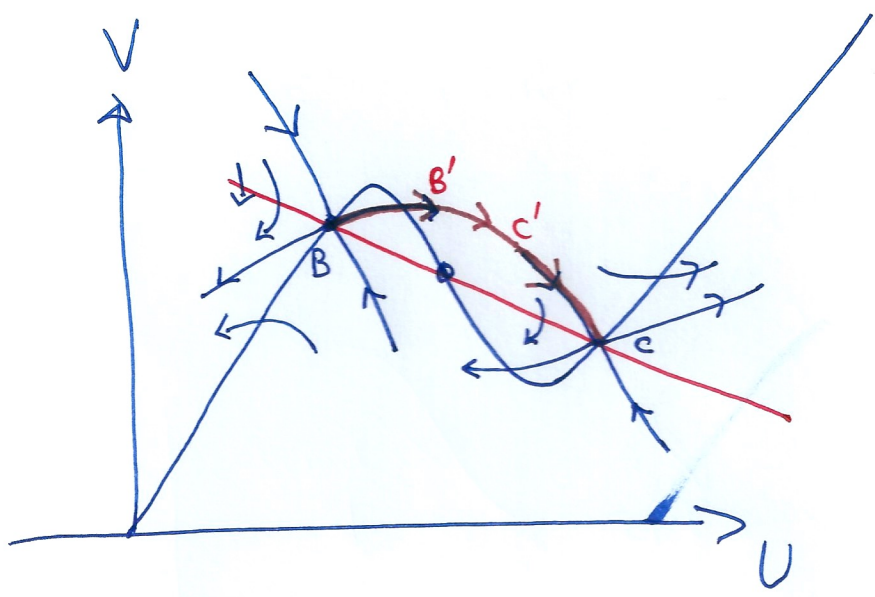
Where it is clear that B & C are saddles

§ Intermediate fixed point is node or spiral  
stability depends on  $\text{tr} M$ ,  $M = \begin{pmatrix} s & \gamma s \\ s' & -1 \end{pmatrix}$

$$\text{tr} M = s - 1$$

unstable if  $s > 1$

stable if  $s < 1$

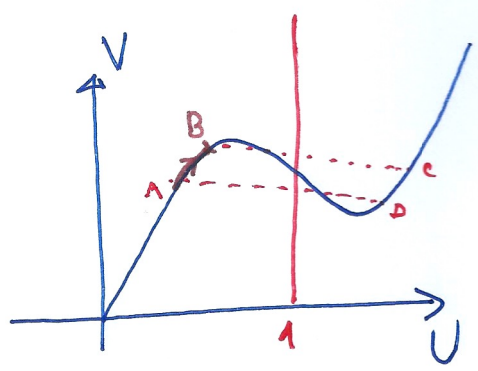


ii) To get from B to C the unstable separatrix BB' from B must join to the stable separatrix c'c to C.

In general this will not occur. Given B, we choose s to make it happen.

(d) Back to  $\xi$  :  $s(U' + \gamma V') = 1 - U + \epsilon U''$   
 $\epsilon s V' = -V + g(U)$

$\Rightarrow V = g(U)$   
 $s(U' + \gamma V') = 1 - U$   
 $\Rightarrow s[1 + \gamma g'(U)]U' = 1 - U$



"Hence show..." - unprecise. I think what is meant is that at B,  $U_B < 1$ ,  $U' > 0$ ,

$\Rightarrow 1 + \gamma g'(U_B) > 0$  so  $U_B$  is less than the value it obtains in the limit cycle (which has  $\gamma g' = -1$ )

[Note:  $U_B$  is not constrained: given  $U_B$ , choose s; in the way back, select D to connect D to A. So there is a one-parameter family of periodic travelling waves]



3/  $\dot{E} = F(E_\tau) - \gamma E$

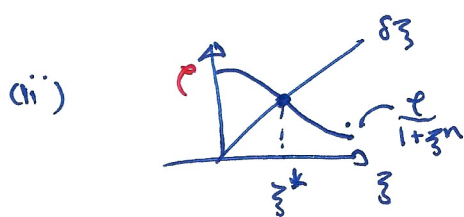
(a) E circulating erythrocytes,  $\gamma$  loss rate (life time  $\sim 100$  d)  
 F production from Pluripotential stem cells with a delay  $\tau$   
 due to maturation time

(b)  $F(E) = \frac{F_0 \theta^n}{E^n + \theta^n}$

(i)  $E = \theta \xi \quad t = \tau T$

$\Rightarrow \frac{\theta}{\tau} \dot{\xi} = \frac{F_0}{1 + \xi^n} - \gamma \theta \xi$

$\Rightarrow \dot{\xi} = \frac{\rho}{1 + \xi^n} - \delta \xi \quad \rho = \frac{F_0 \tau}{\theta}, \quad \delta = \gamma \tau$



clearly unique steady state

(iii) linearize: write  $h = \frac{\rho}{1 + \xi^n}$

$\xi = \xi^* + \eta$

$\dot{\eta} = h'(\xi^*) \eta - \delta \eta$

Define  $\alpha = -h'(\xi^*) = \frac{\rho \cdot n \xi^{n-1}}{(1 + \xi^n)^2}$  note  $1 + \xi^n = \frac{\rho}{\delta \xi}$

$\alpha = \frac{\rho \delta^2 \xi^{2n-2} \cdot n \xi^{n-1}}{\rho^2} = \frac{\delta^2}{\rho} \xi \left( \frac{\rho}{\delta \xi} - 1 \right)$   
 $= \delta n \left[ 1 - \frac{\delta \xi^*}{\rho} \right] > 0$

$$\dot{y} = -\alpha y_1 - \delta y$$

(2)

$$y = e^{\sigma t}$$

$$\underline{\sigma = -\delta - \alpha e^{-\sigma}}$$

Question does not define  $\omega$  !!

If  $\alpha$  is small  $\text{Re } \sigma < 0$  (necessity of  $\alpha < \delta$ )

Fix  $\delta$ ,  $\sigma(\alpha)$  has derivative

$$\sigma' = -e^{-\sigma} + \alpha e^{-\sigma} \sigma'$$

$$\Rightarrow \sigma' = \frac{e^{-\sigma}}{\alpha e^{-\sigma} - 1}, \quad \alpha e^{-\sigma} = -\sigma - \delta$$

$$\text{so } \sigma' = \frac{1}{\alpha} \left[ \frac{-\sigma - \delta}{-\sigma - \delta - 1} \right] = \frac{\sigma + \delta}{\alpha(\sigma + \delta + 1)}$$

Suppose  $\sigma = i\theta$  at some ~~fixed~~ value of  $\alpha$

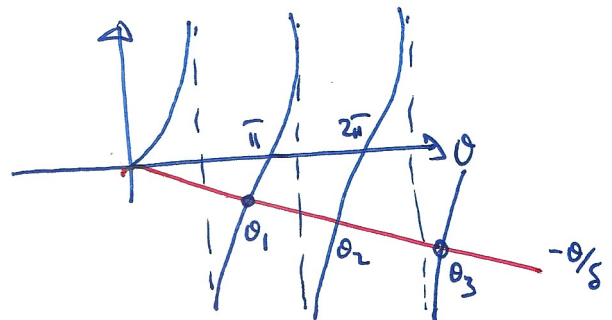
$$\text{then } i\theta = -\delta - \alpha e^{-i\theta}$$

$$\Rightarrow 0 = -\delta - \alpha \cos \theta$$

$$\begin{cases} \theta = \alpha \sin \theta \\ -\delta = \alpha \cos \theta \end{cases}$$

$$\Rightarrow \tan \theta = -\frac{\delta}{\delta}$$

$$\alpha = \frac{\theta}{\sin \theta}$$



These are roots  $\theta_i$  as shown

with  $\theta_1 \in (\frac{\pi}{2}, \pi)$ ,  $\theta_3 \in (\frac{5\pi}{2}, 3\pi)$  etc

A corresponding positive  $\alpha_1 = \frac{\theta_1}{\sin \theta_1}$ ,  $\alpha_3 = \frac{\theta_3}{\sin \theta_3}$  etc

$$\alpha_1 < \alpha_3 < \dots$$

[the latter because also  $\alpha = -\frac{\delta}{\cos \theta}$  & from the graph we

see that  $\theta_r = r\pi - \phi_r$  where  $\phi \in (0, \pi/2)$  is increasing with  $r$

$$\text{So } \theta_{2n-1} = (2n-1)\pi - \phi_{2n-1}$$

$$\alpha = \frac{-\delta}{\cos \theta_{2n-1}} = \frac{\delta}{\cos \phi_{2n-1}}$$

$\phi \uparrow \Rightarrow \cos \phi \downarrow \Rightarrow \frac{\delta}{\cos \phi} \uparrow$  ]

Transversality:  $\sigma' \Big|_{i0} = \frac{\delta + i\theta}{\alpha(1 + \delta + i\theta)} = \frac{(\delta + i\theta)(1 + \delta - i\theta)}{\alpha[(1 + \delta)^2 + \theta^2]}$   
 $= \frac{\delta + i\theta + \delta^2 + \theta^2}{\alpha[(1 + \delta)^2 + \theta^2]}$

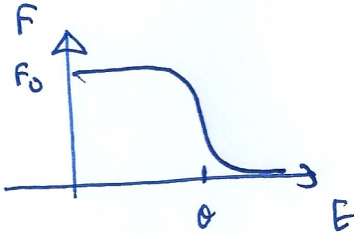
$$\text{So } \text{Re } \sigma' \Big|_{\sigma=i0} > 0$$

Therefore at  $\alpha_1 = \frac{-\delta}{\cos \theta_1}$   
So I suppose  $\theta_1 = \omega^*$

instability occurs for  $\alpha > \alpha_1$

not sure what  $A$  is about. - seems to be upside down

(c)  $n \rightarrow \infty$ .



$$F = \frac{F_0}{1 + \left(\frac{E}{\theta}\right)^n}$$

$E < 0 \quad F \rightarrow F_0$   
 $E > 0 \quad F \rightarrow 0$

oops question has  $\leq 0$  &  
 $\leq E_c$   
 should be <

$t \geq 0 \quad E = E_0 > 0, \quad E > 0 \quad -\tau \leq t \leq 0$

method of steps

$$\dot{E} = F - \gamma E$$

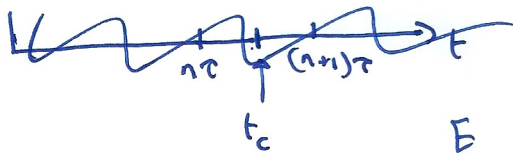
$F = 0 \quad \text{if } E_c > 0$   
 $F = F_0 \quad \text{if } E_c < 0$

(i)  $0 < t < \tau: \quad \dot{E} = -\gamma E \Rightarrow E = E_0 e^{-\gamma t}$

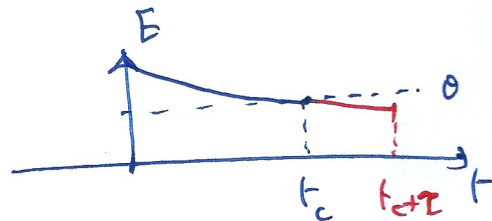
As long as  $E_0 e^{-\gamma t} > 0$  this solution carries on

Suppose  $E_0 e^{-\gamma t}$  At  $t = t_c = \frac{1}{\gamma} \ln \frac{E_0}{\theta}$

$$E = E_0 e^{-\gamma t} = \theta$$



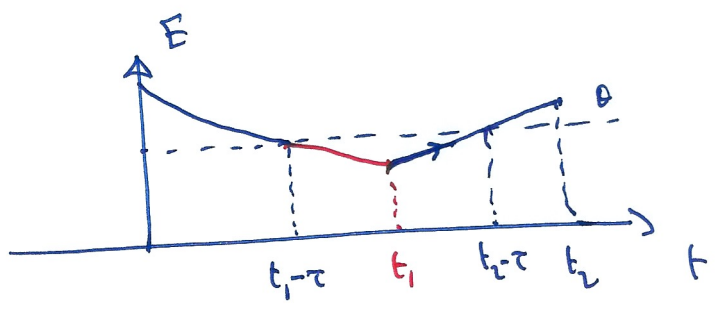
~~If  $t_c < (n+1)\tau$~~



for  $t_c < t < t_c + \tau$  we still have  $E_c > 0$

so  $E = E_0 e^{-\gamma t}$  till  $t = t_c + \tau = \tau + \frac{1}{\gamma} \ln \frac{E_0}{\theta} = t_1$

$E_1 = \theta e^{-\gamma \tau}$



Now for  $t > t_1$ ,  $E_t < \theta$  so  $F = F_0$

$$\dot{E} = F_0 - \gamma E \quad E = E_1 \text{ at } t = t_1$$

$$E - \frac{F_0}{\gamma} = (E_1 - \frac{F_0}{\gamma}) e^{-\gamma(t-t_1)}$$

and this will carry on till  $t = t_2$

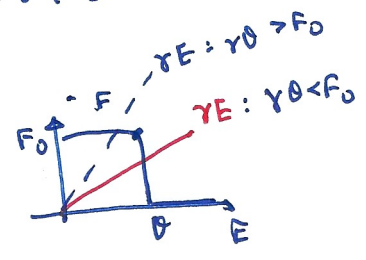
where  $E(t_2 - \tau) = \theta$

$$\theta - \frac{F_0}{\gamma} = (E_1 - \frac{F_0}{\gamma}) e^{-\gamma[t_2 - t_1 - \tau]}$$

$$\Rightarrow \frac{\gamma\theta - F_0}{\gamma E_1 - F_0} = e^{-\gamma(t_2 - t_1 - \tau)}$$

so ...

[note:



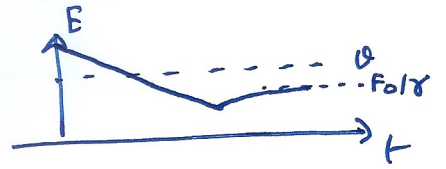
looking back at stability  
result - oscillations if  
 $\alpha = -d'$  large enough  
 $\Rightarrow$  oscillations for  $\gamma < \frac{F_0}{\theta}$   
stable if  $\gamma > \frac{F_0}{\theta}$

$$t_2 = t_1 + \tau + \frac{1}{\gamma} \ln \left[ \frac{\gamma E_1 - F_0}{\gamma\theta - F_0} \right]$$

The sketch above (ie  $E$  becomes  $> \theta$  again)

only applies if  $\frac{F_0}{\gamma}$  (where  $E$  is heading) is  $> \theta$

ie if  $\gamma < \frac{F_0}{\theta}$  if  $\gamma < \frac{F_0}{\theta}$  then



Answer

In fact for  $t > t_1$ ,  $\dot{E} = F_0 - \gamma E$

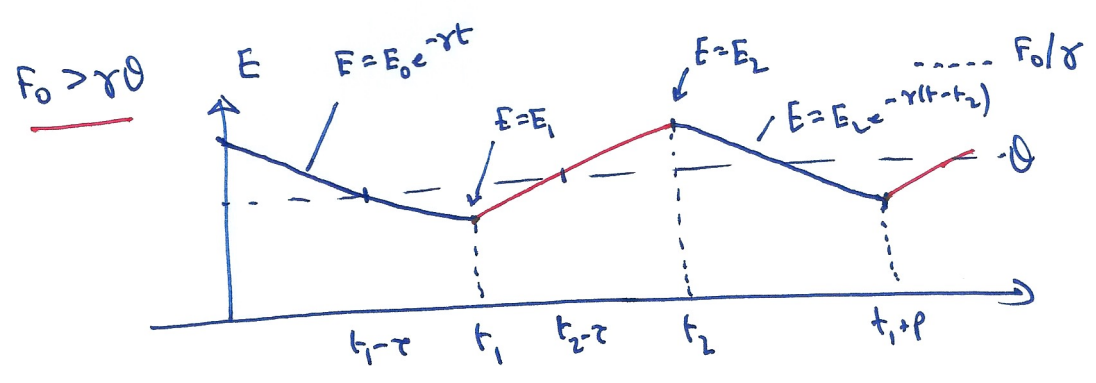
↳ if  $\gamma E_1 > F_0$  solution will continue to decrease & will approach  $\frac{F_0}{\gamma}$  monotonically

↳  $\gamma \theta e^{-\gamma t} > F_0$  solution decreases for ever

↳  $F_0 < \gamma \theta e^{-\gamma t}$  decreases for ever,  $t_1 = \infty$  ( $\Leftrightarrow E \rightarrow \frac{F_0}{\gamma}$ )

$\gamma \theta e^{-\gamma t} < F_0 < \gamma \theta$  decreases till  $t_1$ , increases for ever after  $t_2 = \alpha$  ( $\Leftrightarrow \frac{F_0}{\gamma}$ )

↳ if  $F_0 > \gamma \theta$  oscillations.  $\frac{F_0}{\gamma}$ . [I think]



At  $t_2$ ,  $E = E_2 = \frac{F_0}{\gamma} + (E_1 - \frac{F_0}{\gamma}) \left( \frac{\gamma F_0 - \gamma \theta}{F_0 - \gamma E_1} \right) e^{-\gamma t_2}$

thereafter  $E = E_2 e^{-\gamma(t-t_2)}$  and the solution is periodic with period  $P$

where  $E_2 e^{-\gamma(t_1+p-t_2)} = E_1$  so, note  $e^{-\gamma(t_1+p-t_2)} = e^{\gamma t \left( \frac{F_0 - \gamma E_1}{F_0 - \gamma \theta} \right)}$

so  $e^{\gamma p} = \frac{E_2}{E_1} e^{\gamma t \left( \frac{F_0 - \gamma E_1}{F_0 - \gamma \theta} \right)} = \frac{1}{E_1} \left[ \frac{F_0}{\gamma} \left( \frac{F_0 - \gamma E_1}{F_0 - \gamma \theta} \right) e^{\gamma t} + E_1 - \frac{F_0}{\gamma} \right]$

$\Rightarrow p \dots$

question needed to state that  $F_0 > \gamma \theta$ .

1. 
$$\Sigma \dot{v} = I^* + f(v) - w$$

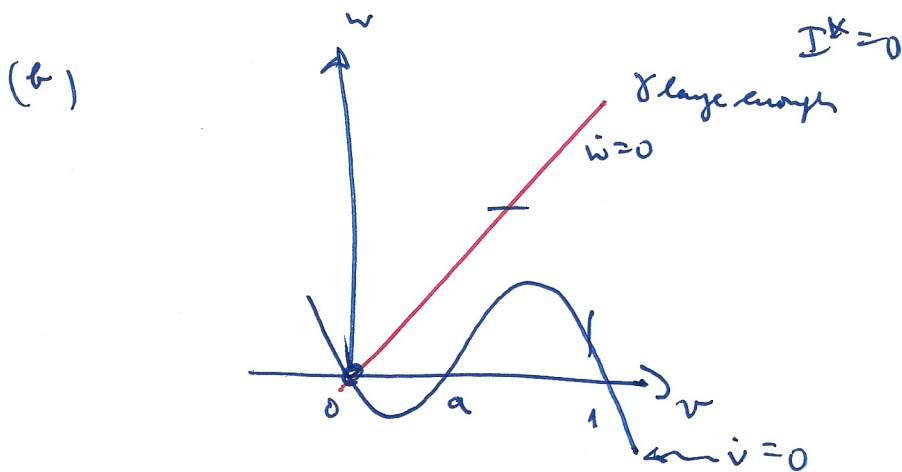
$$\dot{w} = \gamma v - w$$

$$f = -v(a-v)(1-v) \quad 0 < a < 1$$

- (a)  $v$  intracellular electric potential  
 $w$  gate variable  
 $I^*$  applied current

$-f(v) + v$  ionic current at

Start with Hodgkin-Huxley, 3 gate variables <sup>m, h, n</sup> & telegraph equation for potential (via  $I_H$  &  $I_L$ ):  $\tau_m \ll 1 \Rightarrow$  in equilibrium,  $n+h = \text{constant}$ .  
 $\Rightarrow$  FN reduction ...



Endstate are equilibria  $(0,0)$  for  $\delta$  layer

Linearize 
$$\begin{pmatrix} \dot{v} \\ \dot{w} \end{pmatrix} \approx \underbrace{\begin{pmatrix} \frac{f'}{\Sigma} & -\frac{1}{\Sigma} \\ \gamma & -1 \end{pmatrix}}_M \begin{pmatrix} v \\ w \end{pmatrix}$$

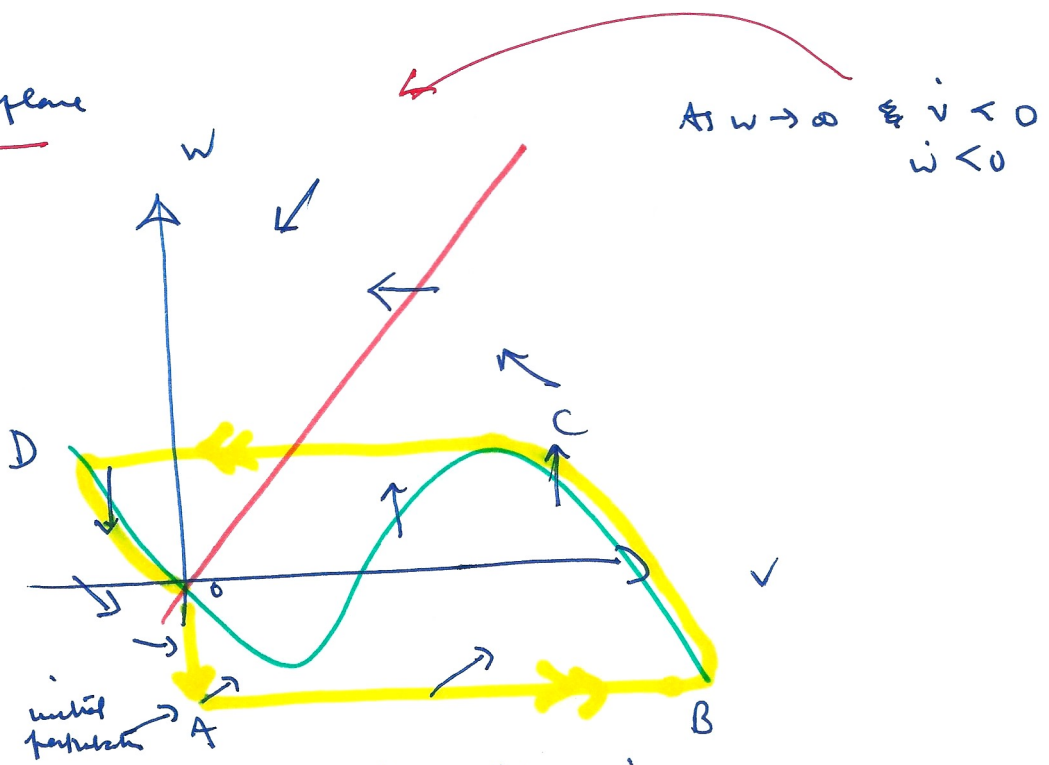
$\text{tr } M = \frac{f'}{\Sigma} - 1 < 0$  at  $(0,0)$ ,  $\det M = -\frac{f'}{\Sigma} + \gamma > 0 \Rightarrow$  stable

$t \sim 1$  :  $w \approx f(v)$

$\dot{w} = f(v) - w$

$t \sim \epsilon$ ,  $t = \epsilon T$      $v' = f(v) - w$   
 $w' = 0$

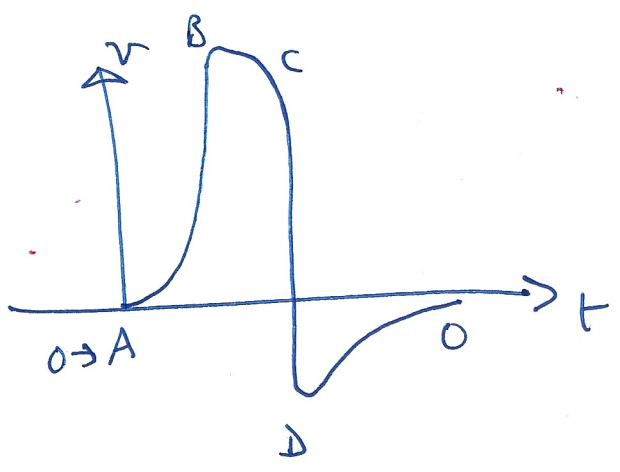
phase plane



trajectories cycle round stable origin

threshold : as  $v$  approaches  $v^*$   $I^* > 0$  for short time  $\leftrightarrow$  lower

$w \Rightarrow$  trajectory as shown : fast phases with  $\rightarrow$

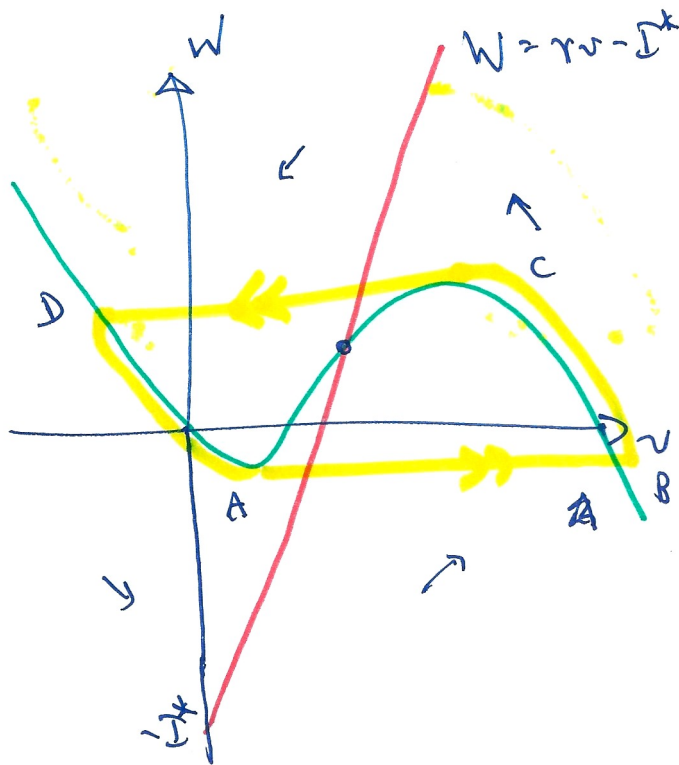




$$(e) \quad \dot{I}^* = 0, \quad W = w - \dot{I}^*$$

$$\dot{v} = f(v) - W$$

$$\dot{W} = r v - \dot{I}^* - W$$



$$P \approx \int_B^C dt + \int_D^A dt$$

$$\approx \int_B^C \frac{dw}{\dot{w}} + \int_D^A \frac{dw}{\dot{w}} \quad \text{along } W = f(v)$$

$$= \int_B^C \frac{dw}{rv - \dot{I}^* - W} + \int_D^A \frac{dw}{rv - \dot{I}^* - W}$$

$$= \int_B^C \frac{f'(v) dv}{rv - \dot{I}^* - f(v)} + \int_D^A \frac{f(v) dv}{rv - \dot{I}^* - W}$$

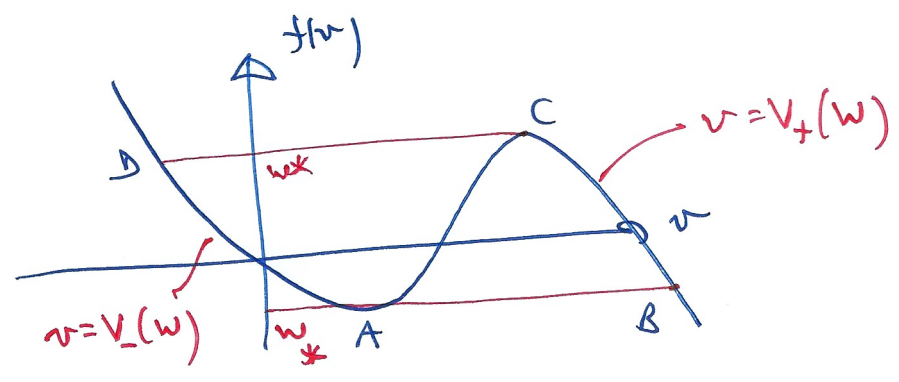
From the question leaves: as  $W$ , how did

$$P \approx \int_{w_B}^{w_C} \frac{dw}{\gamma r - \mathcal{I}^* - w} + \int_{w_D}^{w_A} \frac{dw}{\gamma r - \mathcal{I}^* - w}$$

On BC  $w < \gamma r - \mathcal{I}^* - w$ , denote  $v = V_+(w)$  on BC  
 on DA  $w > \gamma r - \mathcal{I}^* - w$  denote  $v = V_-(w)$  on AD

(see figure)

Also let  $w = f(v) = w_*$  at A & B  
 $w = w^*$  at C & D



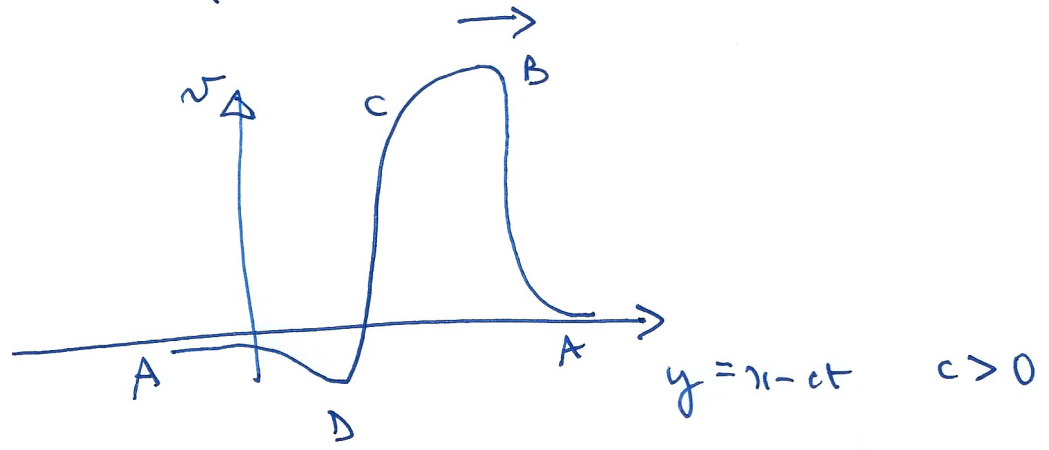
$$\begin{aligned} \text{So } P &\approx \int_{w_*}^{w^*} \frac{dw}{\gamma V_+(w) - \mathcal{I}^* - w} + \int_{w^*}^{w_*} \frac{dw}{\gamma V_-(w) - \mathcal{I}^* - w} \\ &= \int_{w_*}^{w^*} \left[ \frac{1}{\gamma V_+(w) - \mathcal{I}^* - w} - \frac{1}{\gamma V_-(w) - \mathcal{I}^* - w} \right] dw \end{aligned}$$

note this is  $> 0$

(d)

$$\varepsilon v_F = f(v) - w + \varepsilon^2 v_{xxx}$$

$$w_F = \gamma v - w$$



(i) 
$$-\varepsilon c v' = f(v) - w + \varepsilon^2 v''$$

$$-c w' = \gamma v - w$$

$v(\eta), w(\eta)$   
 bc's  $v, w \rightarrow 0$  at  $\pm \infty$ .

(ii) AB part where  $y = \varepsilon \eta$

$$\Rightarrow -c v' = f(v) - w + v''$$

$$-c w' = \varepsilon(\gamma v - w) \Rightarrow w \approx 0$$

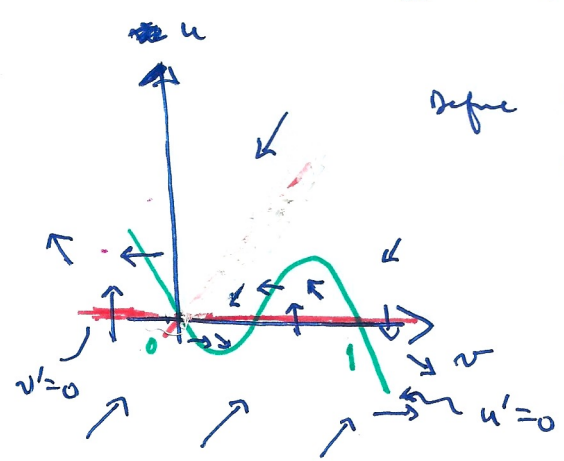
$$\Rightarrow v'' + c v' + f(v) = 0 \quad w \approx AB$$

$$\eta \rightarrow \infty \quad v \rightarrow 0$$

$$\eta \rightarrow -\infty \quad v \rightarrow v_B \quad (\text{where } f(v_B) = 0 \text{ and } v_B = 1)$$

ii  $v \rightarrow 1$  (as a).

(iii)



define  $u' = -u$   
 then  $u' = f(v) - cu$

At large  $u$   $v' < 0$   $u' < 0$

$\Rightarrow$  trajectories as shown

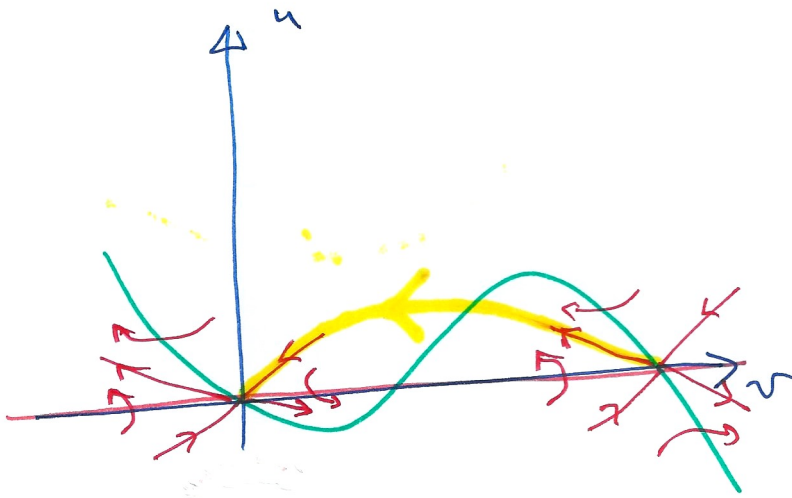
6

Clearly  $(0,0)$  &  $(1,0)$  are saddles,  $(\frac{1}{2},0)$  a node or spiral

To connect  $(1,0)$  ( $\gamma \rightarrow -\infty$ ) to  $(0,0)$  ( $\gamma \rightarrow \infty$ ) we

need to connect the unstable separatrix from  $(1,0)$  in  $v < 1$  to

the stable separatrix  $\rightarrow$  to  $(0,0)$  in  $v > 0$ :



this requires a choice of  $c$  to make them join.

$$v'' + cv' + f(v) = 0$$

So  $(xv')$   $\frac{1}{2}v'^2 \Big|_{-\infty}^{\infty} + c \int_{-\infty}^{\infty} v'^2 dv + \int_1^0 f(v) dv = 0$

$$\Rightarrow c = \frac{\int_0^1 f(v) dv}{\int_{-\infty}^{\infty} v'^2 dv}$$

---

which requires  $\int_0^1 f(v) dv > 0$   
 $v \geq \frac{1}{2}$

$$\dot{p} = -\gamma p + \beta(N)N - e^{-\gamma\tau} \beta(N_\tau)N_\tau$$

$$\dot{N} = -\beta(N)N - \kappa N + 2e^{-\gamma\tau} \beta(N_\tau)N_\tau$$

(a)  $\gamma$  apoptosis (cell death) rate

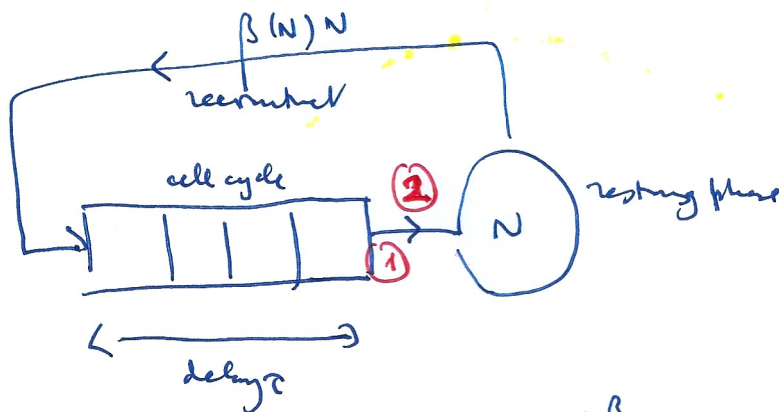
$\kappa$  loss to maturation stage

(i)  $e^{-\gamma\tau} \beta(N_\tau)N_\tau$  (1) loss of cells from proliferative phase after cell cycle

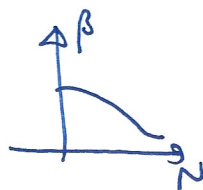
(ii)  $2e^{-\gamma\tau} \beta(N_\tau)N_\tau$  (2) supply to resting phase  $N$  after mitosis (factor of 2)

(iii)  $\beta$  decreasing to exert control on production of  $N$  (high  $N$

causes less recruitment to proliferative phase)



(\*)  $\beta(N) = \beta_0 \text{sech}\left(\frac{N}{\beta_1}\right)$



let  $N = \beta_1 n$ ,  $t \sim \tau$

$$\Rightarrow \frac{\beta_1}{\tau} \dot{n} = -\beta_0 \beta_1 n \text{sech} n - \kappa \beta_1 n + 2e^{-\gamma\tau} \beta_0 \beta_1 n_1 \text{sech} n_1$$

$$\Rightarrow \dot{n} = \beta_0 \tau [n_1 \text{sech} n_1 - n \text{sech} n] - \kappa \tau n + [2e^{-\gamma\tau} - 1] \beta_0 \tau n_1 \text{sech} n_1$$

If we define  $g = \tau n \text{sech} n$  then,  $\tau = \beta_0 \tau$

$$\dot{n} = g(n_1) - g(n) + [2e^{-\gamma\tau} - 1] g(n_1) - \kappa \tau n$$

Thus

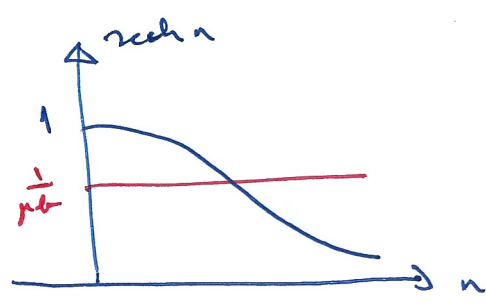
$$\dot{n} = g(n_1) - g(n) + \varepsilon [\mu g(n_1) - n]$$

$\varepsilon = \kappa \tau$ ,  $\mu = \frac{2e^{-\kappa \tau} - 1}{\kappa \tau}$   $b = \beta_0 \tau$

(i) equilibrium

$$n = \mu g(n)$$

equilibrium  
 $= \mu b n$



So  $n=0$  or  $n = \frac{1}{\mu b}$  if  $\mu b > 1$

linear  $n = n^* + m$

$$\Rightarrow \dot{m} = g'(n_1) - g'(n) + \varepsilon [\mu g'(n_1) - m]$$

$$g' = g'(n^*)$$

$$m = e^{\lambda t} \Rightarrow \lambda = g' e^{-\lambda} - g' + \varepsilon \mu g' e^{-\lambda} - \varepsilon$$

$\lambda = -\alpha - \delta e^{-\lambda}$

where  $\alpha = \varepsilon + g'$

$\delta = -(1 + \varepsilon \mu) g' > 0$

If  $\alpha, \delta > 0$  then  $\lambda < 0$  if real.

(ii)

Define  $\tau = \varepsilon t$ ,  $n = n(\tau) \Rightarrow n_1 = n(\tau - \varepsilon)$

$\Rightarrow$  Taylor expand  $n_1 = n - \varepsilon n' \dots$   
 $\Rightarrow g(n_1) \approx g(n) - \varepsilon n' g'(n) \dots$

~~$\varepsilon n'$~~

$\varepsilon n' \approx g(n) - \varepsilon n' g'(n) - g(n)$

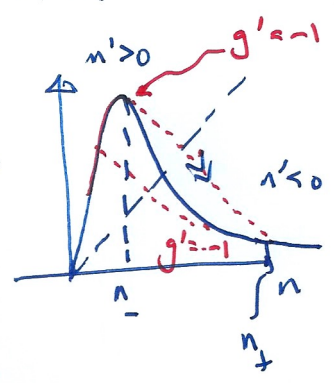
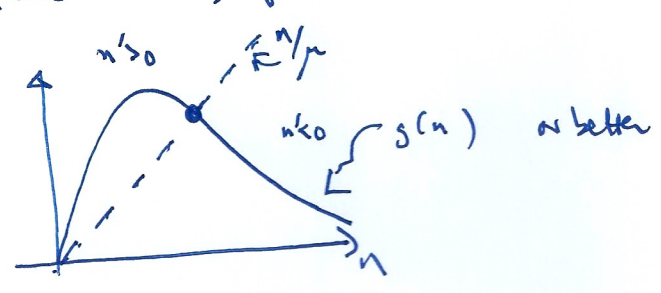
$+ \varepsilon [\mu \{ g(n) - \varepsilon n' g'(n) \} - n]$

$\Rightarrow n' \approx -n' g'(n) + \mu g(n) - n$

$\Rightarrow n' \approx \frac{\mu g(n) - n}{1 + g'(n)}$

but for  $t \sim 1$   $\dot{n} \approx g(n_1) - g(n)$

The oscillations are actually of relaxation time, as on the slow time scale



slow phase finishes at  $g' = -1$

$\Rightarrow$  fast phase  $\dot{n}$  where  $n \rightarrow n_+ \approx t \rightarrow \infty$ ,  $n \rightarrow n_- \approx t \rightarrow -\infty$

$n(t_+) - n(t_-) = \int_{t_-}^{t_+} g(n_1) dt - \int_{t_-}^{t_+} g(n) dt$   
 $= \int_{t_-}^{t_+} g(n) dt - \int_{t_-}^{t_+} g(n) dt = \int_{t_-}^{t_+} g dt - \int_{t_+}^{t_-} g dt$

$\Rightarrow n_+ - n_- \approx g(n_-) - g(n_+)$  so jump  $n_-$  to  $n_+$  along  $n + g(n) = \text{constant}$  - red lines above

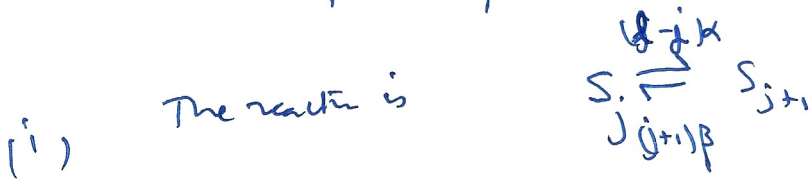
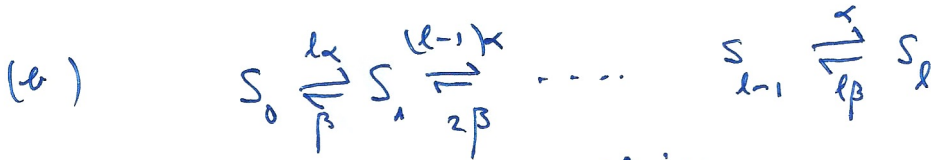


3/ (a)  $C \xrightleftharpoons[\beta]{\alpha} O$  ← fraction

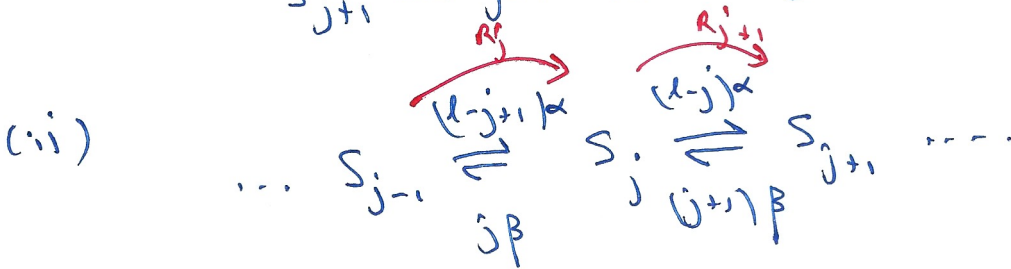
$$n = \alpha(1-n) + \beta n$$

$$= \tau n = n_0 - n \quad \tau = \frac{1}{\alpha + \beta}, \quad n_0 = \frac{\alpha}{\alpha + \beta}$$

$\tau_n$  relaxation time  
no equilibrium



became  $S_j$  has  $j$  open ports,  $l-j$  closed so  $(l-j)$  chances of opening  
 $S_{j+1}$  has  $j+1$  so  $(j+1)$  chances of closing



$x_j =$  fraction of open  $S_j$  channels

~~$x_j = \frac{(l-j+1)\alpha}{j\beta} x_{j-1}$~~

write  $R_j = (l-j+1)\alpha x_{j-1} - j\beta x_j \quad j = 1, \dots, l$

then  $x_j = R_j - R_{j+1} \quad j = 1, \dots, l-1$



Also

$$x_0 = -R_1$$

$$x_l = R_l$$

(iii) To show a solution is  $x_j = \binom{l}{j} n^j (1-n)^{l-j}$

a cute way is then  $\sum_0^l x_j s^j = \sum_0^l \binom{l}{j} (ns)^j (1-n)^{l-j} = (1-n+ns)^l$

So define  $\phi(s,t) = \sum_0^l x_j s^j$

$$\begin{aligned} \text{then } \phi_t &= \sum_0^l \dot{x}_j s^j \\ &= \sum_0^l [R_j - R_{j+1}] s^j \\ &= \sum_0^l R_j s^j - \frac{1}{s} \sum_0^l R_{j+1} s^{j+1} \\ &= \sum_0^l R_j s^j - \frac{1}{s} \sum_0^{l-1} R_{j+1} s^{j+1} \\ &= \sum_0^l R_j s^j - \frac{1}{s} \sum_1^l R_k s^k \\ &= \left(1 - \frac{1}{s}\right) \sum_0^l R_j s^j \end{aligned}$$

provided we define  $R_0 = R_{l+1} = 0$

$$\begin{aligned} \text{Also } \sum_0^l R_j s^j &= \sum_0^{l-1} (l-j+1) \alpha x_{j-1} s^j - \sum_1^l \beta j x_j s^j \\ &= \sum_0^{l-1} (l-k) \alpha x_k s^{k+1} - \beta s \sum_1^l j x_j s^{j-1} \\ (l-l=0): &= \sum_0^l (l-k) \alpha x_k s^{k+1} - \beta s \sum_0^l j x_j s^{j-1} \quad (0=0) \\ &= \sum_0^l \alpha l s x_k s^k - \sum_0^l \alpha s^2 k x_k s^{k-1} - \beta s \sum_0^l j x_j s^{j-1} \\ &= \alpha l s \phi - \alpha s^2 \phi_{s'} - \beta s \phi_s \end{aligned}$$

Hence

$$\begin{aligned} \phi_f &= \left(1 - \frac{1}{s}\right) \left[ \alpha s \phi - (\alpha s^2 + \beta s) \phi_s \right] \\ &= (s-1) \left[ \alpha \phi - (\alpha s + \beta) \phi_s \right] \end{aligned}$$

Let us put  $\phi = (1-n+ns)^l$

$$\phi_f = l(1-n+ns)^{l-1} (s-1)n$$

$$\phi_s = l(1-n+ns)^{l-1} n$$

∴ this solves the pde ( + thus the  $x_j = e^{j^2}$  ) ✓

$$\phi_f = l(1-n+ns)^{l-1} (s-1)n$$

$$= (s-1) \left[ \alpha \phi - (\alpha s + \beta) \phi_s \right]$$

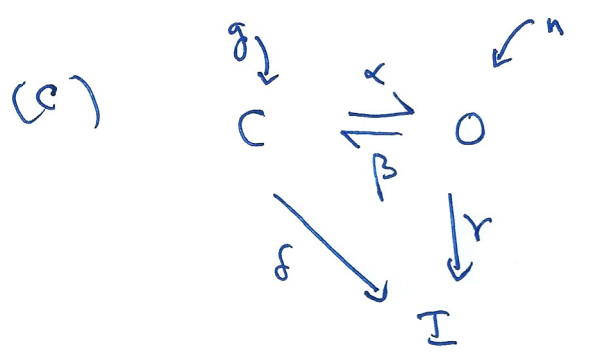
$$= (s-1) \left[ \alpha l(1-n+ns)^{l-1} - (\alpha s + \beta) l(1-n+ns)^{l-1} n \right]$$

i.e.  $\left[ \div \text{ by } l(1-n+ns)^{l-1} (s-1) \right]$

$$n = \alpha(1-n+ns) - (\alpha s + \beta)n$$

$$= \alpha(1-n) - \beta n$$

∴



(i)  $1 - n - g$

(ii)  $\dot{n} = \alpha g - \beta n - \gamma n$

$\dot{g} = -\alpha g + \beta n - \delta g$

(iii)  $t \rightarrow 0 \quad n = 1 \quad g = 0 \quad \text{all open}$

$$\begin{pmatrix} \dot{n} \\ \dot{g} \end{pmatrix} = \begin{pmatrix} -(\beta + \gamma) & \alpha \\ \beta & -(\alpha + \delta) \end{pmatrix} \begin{pmatrix} n \\ g \end{pmatrix}$$

$$\Rightarrow \begin{pmatrix} n \\ g \end{pmatrix} = \underline{c_1} e^{\lambda_1 t} + \underline{c_2} e^{\lambda_2 t}$$

$$(\lambda + \beta + \gamma)(\lambda + \alpha + \delta) - \alpha\beta = 0 \Rightarrow \lambda_1, \lambda_2$$

$$\Rightarrow g = a(e^{\lambda_1 t} - e^{\lambda_2 t}) \quad (\lambda_1 > \lambda_2) \quad \text{for } g = 0 \text{ at } t = 0$$

~~then (5e1)  $n = \frac{1}{\beta} [g + (\alpha + \delta)g]$~~

then (5e1)  $n = \frac{1}{\beta} [g + (\alpha + \delta)g]$

for  $t = 0 \quad n = 1 = \frac{1}{\beta} [g|_0] = \frac{a}{\beta} (\lambda_1 - \lambda_2)$

$$\Rightarrow a = \frac{\beta}{\lambda_1 - \lambda_2}$$

characteristic equation:  $(\lambda + \beta + \gamma)(\lambda + \alpha + \delta) - \alpha\beta = 0$

$$\Rightarrow \lambda^2 + (\alpha + \beta + \gamma + \delta)\lambda + (\alpha\delta + \beta\delta + \gamma\alpha) - \alpha\beta = 0$$

$$\lambda_{1,2} = \frac{1}{2} [T \pm (T^2 - 4D)^{1/2}]$$

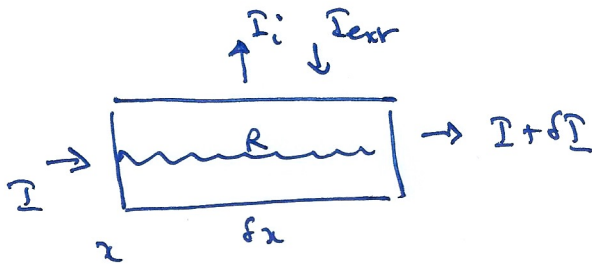
$$\Rightarrow \lambda_1, -\lambda_2 = (T^2 - 4D)^{1/2} = [(\alpha + \beta + \gamma + \delta)^2 - 4(\alpha\delta + \beta\delta + \gamma\alpha - \alpha\beta)]^{1/2}$$

CS-12

Math Physiol 2018 21

C

(a)



Conservation of charge (density)  $Q = CV$

$$\frac{\partial}{\partial t} Q \Delta x = I \Big|_x^{x+\Delta x} + (I_{\text{ext}} - I_i) \Delta x$$

$$\Rightarrow \frac{\partial}{\partial t} C \frac{\partial V}{\partial x} = - \frac{\partial I}{\partial x} \Delta x + I_{\text{ext}} - I_i$$

Also Ohm's law with Resistance  $R$  / unit length

$$-\Delta V = R \Delta x I$$

$$\Rightarrow \frac{-\Delta V}{\Delta x} = R I$$

$C$  capacitance (unit length)

$R$  resistance (unit length)

$$(b) \quad I_i = g_1(V - V_1)n + g_2(V - V_2)(1-n)m \quad V_1 < V_2$$

$$I_i \approx \dot{q} = n_0(V) - n$$

(i) steady state  $I_i = 0 \Rightarrow V = V_0, n = n_0(V_0) = n_0$  say

$$\Rightarrow 0 = g_1(V_0 - V_1)n_0 + g_2(V_0 - V_2)(1 - n_0)m \quad \text{or } n = n(V_0)?$$

$$\Rightarrow V_0 = \frac{g_1 n_0 V_1 + g_2 (1 - n_0) m V_2}{g_1 n_0 + g_2 (1 - n_0) m} \in (V_1, V_2)$$

since  $g_1 n_0 > 0$   
 $g_2 (1 - n_0) m > 0$

ii

(2)

non-d f ~ c x ~ d  $V = V_0 + V^* v$

$$CV_t = \frac{1}{R} V_{t+1} + \bar{I}_{ext} - \bar{I}_i$$

$$\begin{aligned} \dagger \bar{I}_i &= g_1 [V_0 - V_1 + V^* v] n + g_2 [V_0 - V_2 + V^* v] (1-n) m \\ &= g_1 V^* \left[ \frac{V_0 - V_1}{V^*} + v \right] n + g_2 V^* \left[ v - \frac{V_2 - V_0}{V^*} \right] (1-n) m \end{aligned}$$

$$= g_2 V^* \bar{I}_i^*$$

$$\bar{I}_i^* = \frac{g_1}{g_2} \left[ \frac{V_0 - V_1}{V^*} + v \right] n + \left[ v - \frac{V_2 - V_0}{V^*} \right] (1-n) m$$

choose  $V^* \geq V_2 - V_0 > 0$

$$\Rightarrow \bar{I}_i^* = \gamma (v + v_1) n + (v - 1) (1-n) m$$

$$\gamma = \frac{g_1}{g_2}, \quad v_1 = \frac{V_0 - V_1}{V_2 - V_0} > 0$$

and  $\frac{CV^*}{\tau} v_t = \frac{V^*}{Rl^2} v_{t+1} + g_2 V^* (\bar{I}_{ext}^* - \bar{I}_i^*)$

where also  $\bar{I}_{ext}^* = g_2 V^* \bar{I}_{ext}^*$

$$\Delta \quad \underline{n = n_0 - n}$$

thus define  $\varepsilon = \frac{CV^*}{\tau g_2 V^*} = \frac{C}{\tau g_2}$

$$\dagger \varepsilon^2 = \frac{1}{g_2 R l^2} \quad \text{if } l = \frac{\tau g_2}{C \sqrt{g_2 R}} = \frac{\tau}{C} \sqrt{\frac{g_2}{R}}$$

(e)  $\Sigma V_f = \Sigma_{\text{extr}}^k - \Sigma_i^k + \varepsilon^{-1} v_{\text{ext}}$

$n_f = n_a - n$

$\Sigma_i^k = g(n, v) = \gamma(v+v_1)^n + (v-1)(1-n)m$

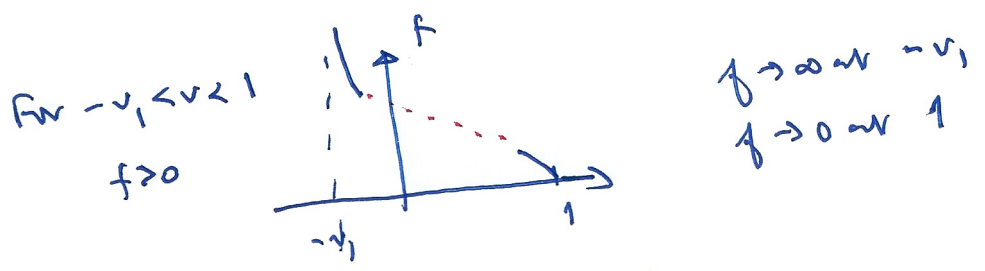
$n = h(v) \iff g(n, v) = 0$

explicitly  $[\gamma(v+v_1) - (v-1)m]^n + (v-1)m = 0$

$n = \frac{(v-1)m(v)}{(v-1)m(v) - \gamma(v+v_1)} = h(v) \quad m > 0, m' > 0$

equilibrium:  $v=0, n=n_0(0)$

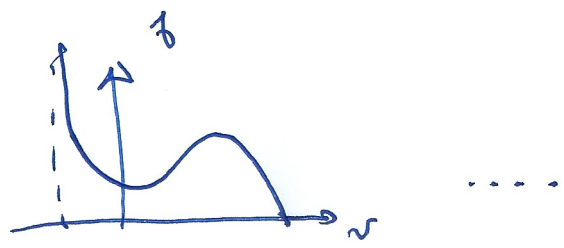
Consider the function  $f(v) = \frac{(1-v)}{\gamma(v+v_1)} \quad (20 \text{ is } \frac{1}{f+1})$



so monotonically decreasing is possible

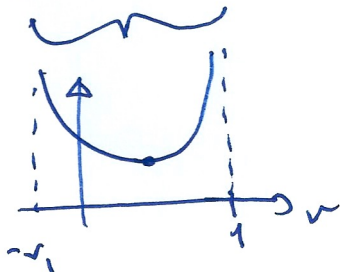
but clearly  $f$  will not be non-monotonic if

$m'$  is large enough

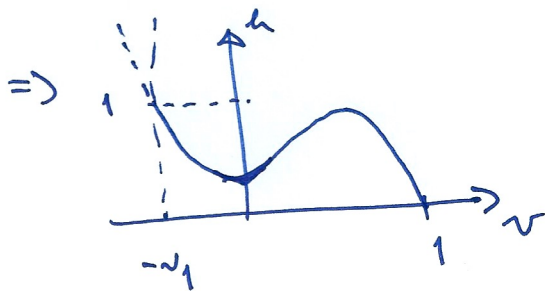
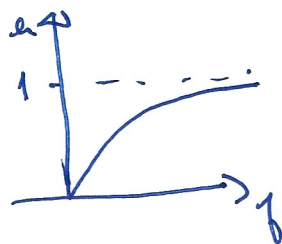
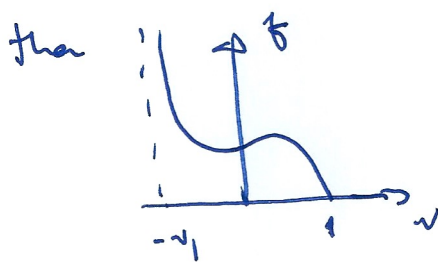


Explicitly  $\frac{f'p'}{f} = \frac{-1}{1-v} + \frac{m'}{m} - \frac{1}{v+v_1}$

$$= \frac{m'}{m} - \left[ \frac{1}{1-v} + \frac{1}{v+v_1} \right]$$



$> 0$  if  $\frac{m'}{m}$  larger than  $\min_{-v_1 < v < 1} \left[ \frac{1}{1-v} + \frac{1}{v+v_1} \right]$



(ii) obvious (clearly done)  $\cdot$   $h'(v) = h'(g) f'(v)$

$$= \frac{f}{(f+1)^2} \left[ \frac{m'}{m} - \left\{ \frac{1}{1-v} + \frac{1}{v+v_1} \right\} \right]$$

$\rightarrow -\infty$  as  $v \rightarrow 1$   
 $f < 0$  as  $v \rightarrow v_1$   
 $f \rightarrow \infty$

$$\left( h' = \frac{1}{f} \cdot -\frac{1}{(v+v_1)} \right)$$

$$\approx -\frac{\gamma}{(1+v_1)^2 m(-v_1)}$$

$$m = \exp[k(v-1)]$$

$$= \frac{m'}{m} = k$$

non-monotonic if  $k > \min \left[ \frac{1}{1-v} + \frac{1}{v+v_1} \right]$

which is at  $\frac{1}{(1-v)^2} = \frac{1}{(v+v_1)^2}$

or  $1-v = v+v_1$

$$v = \frac{1-v_1}{2}$$

$$\text{min is } \left[ \frac{1}{1 - \left(\frac{1-v_1}{2}\right)} + \frac{1}{\frac{1-v_1}{2} + v_1} \right]$$

$$= \frac{4}{1+v_1}$$

So if  $k > \frac{4}{1+v_1}$

(iii)  $n_\infty(v)$  increasing

~~At  $v=0$ ,  $f = \frac{n(0)}{f+1}$~~

$$k'(v) = \frac{f}{(f+1)^2} \left[ k - \left\{ \frac{1}{1-v} + \frac{1}{v+v_1} \right\} \right]$$

$$k'(0) > 0 \quad \text{if } [k(0) > 0] \text{ or } n(0) > 0$$

$$k > 1 + \frac{1}{v_1}$$



[Note: question suggests  $h'(0) > 0$  or below. Scope for  $h'(0) < 0$ ]

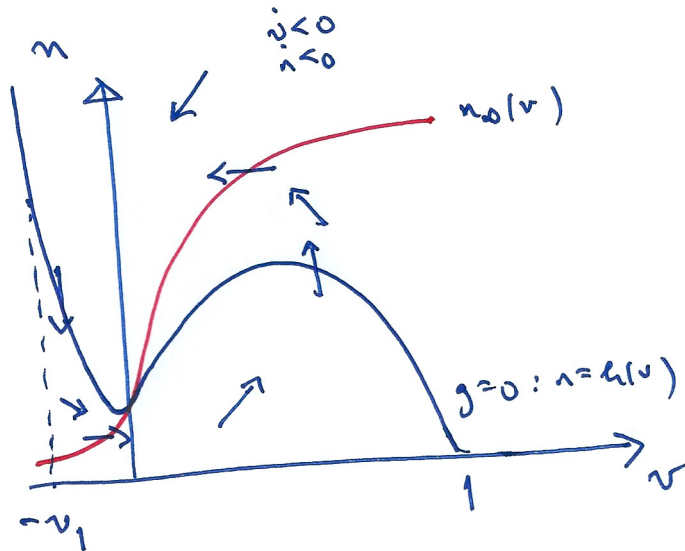
$$\epsilon \dot{v} = -g(n, v)$$

$$\dot{n} = n_0 - n$$

Note for  $-v_1 < v < 1, n > 0$

$$g \rightarrow \infty \text{ as } n \rightarrow \infty$$

$$\Rightarrow \dot{v} < 0 \text{ for } n > h(v)$$



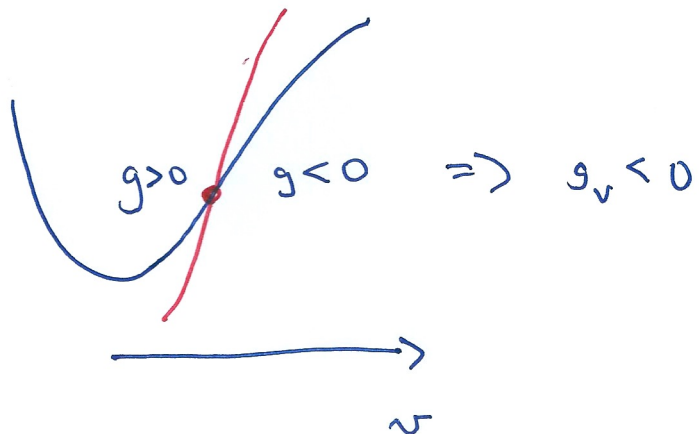
↓  
trajectory direction  
as shown  
⇒ fixed point  
is node or spiral

⇒ stable if  $\text{tr} M < 0$  where  $M = \begin{pmatrix} -\frac{1}{\epsilon} g_v & \frac{1}{\epsilon} g_n \\ n_0' & -1 \end{pmatrix}$

$$\text{tr} M = -\frac{1}{\epsilon} g_v - 1$$

$$< 0 \text{ if } g_v > -\epsilon$$

Now need  $h'(0) > 0$



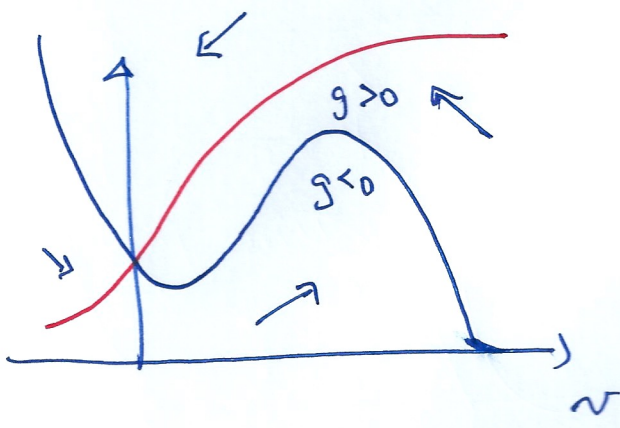
and the steady state is unstable !?

[The question is not specific, but the implication to me is that we should have  $h'(0) < 0$ ]

[ I think the question ought to read:

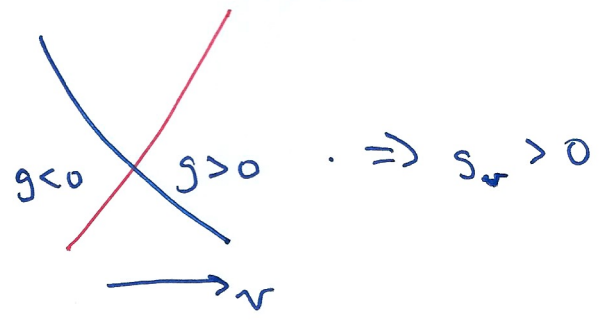
determine the conditions such that  $h'(v_0) < 0$ . Assuming this,

we... ]

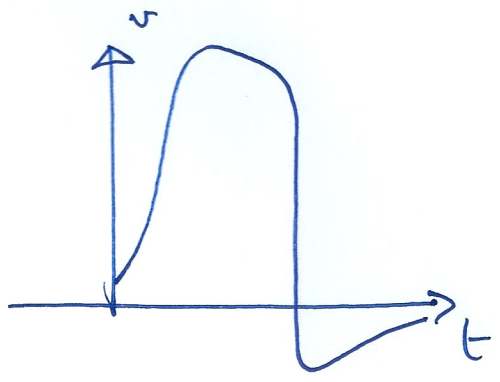
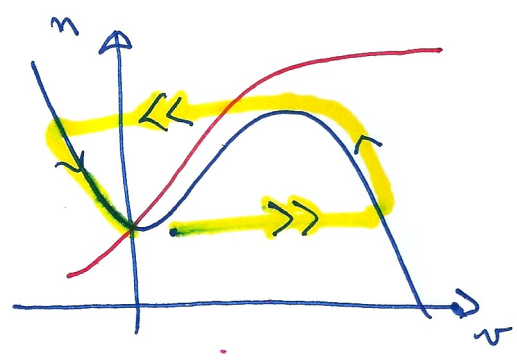


Steady state is stable if  $g_v > -\epsilon$

Always i.e. if  $g_v \geq 0$  ( $\epsilon < 1$ )



Threshold phenomenon: increase v





$$\dot{c} = r - lc - [J_+ - J_- - lc_s c_s]$$

$$\dot{c}_s = J_+ - J_- - lc_s c_s$$

(a)  $r$  : production of cytoplasmic  $Ca^{2+}$  by stimulation of the  $IP_3$  sensitive store

$lc$  leakage of cytoplasmic  $Ca^{2+}$  through cell

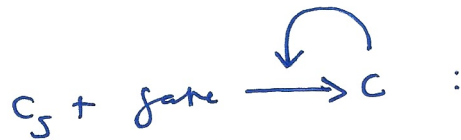
$lc_s$  leakage of  $Ca^{2+}$  sensitive store to cytoplasm

(b) 
$$J_- = \frac{V c_s^m}{K_i^m + c_s^m} \cdot \frac{c^p}{K_v^p + c^p}$$

This is the product of two Hill functions (analogous to <sup>cooperative</sup> enzyme production) : the release ~~is~~ ~~depends~~ increases with  $c_s$

(as for example  $c_s + \text{gate} \rightarrow c$ )

but is also stimulated by  $c$  (CICR) thus



the cytoplasmic  $Ca^{2+}$  facilitates the release of the stored  $Ca^{2+}$ .

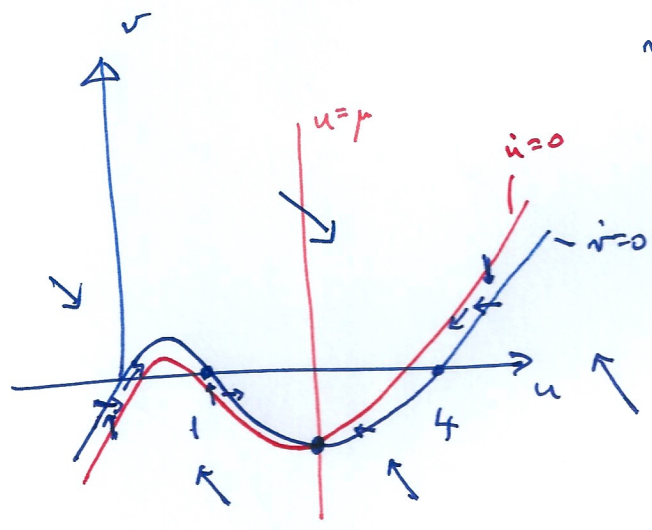
(c)

$$\dot{u} = \mu - u - \frac{\epsilon}{5} f(u, v)$$

$$\dot{v} = \frac{1}{\epsilon} f(u, v)$$

$$f = u[u^2 - 4u + 5] - v \approx g(u) - v$$

(i)



v nullcline  $f=0$ :

$$v = u(u-4)(u-1)$$

$\dot{u}=0$  [ not sure if the actual nullclines is required - would have depended how the lecturer presented it - I'll do the actual nullcline ]

is (with  $g(u) = u(u-4)(u-1)$ )

$$\frac{\epsilon}{5}(\mu - u) = f = g - v \Rightarrow v = g(u) - \frac{\epsilon}{5}(\mu - u)$$

example above uses  $1 < \mu < 4$ .

Large  $v$ :  $\dot{v} < 0$   $\Rightarrow$  other trajectories as shown

Note unique steady state at  $u = \mu, v = g(\mu)$

Carrying on formally, linearise at steady state

(3)

$$\begin{aligned} u &= \mu + U \\ v &= g(\mu) + V \end{aligned} \Rightarrow \text{linearise} \begin{pmatrix} \dot{U} \\ \dot{V} \end{pmatrix} \approx M \begin{pmatrix} U \\ V \end{pmatrix}$$

$$M = \begin{pmatrix} -1 - \frac{5}{\epsilon} f_u & -\frac{5}{\epsilon} f_v \\ \frac{1}{\epsilon} f_u & \frac{1}{\epsilon} f_v \end{pmatrix}$$

$$\text{So } \det M = -\frac{1}{\epsilon} f_v$$

$$\text{tr} M = -1 - \frac{5}{\epsilon} f_u + \frac{1}{\epsilon} f_v$$

$$f = g(u) - v \quad \text{So } \det M > 0 \quad \text{never null}$$

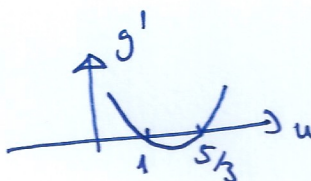
$$\text{tr} M = -1 + \frac{1}{\epsilon} [-1 - 5g']$$

So ( $\epsilon \ll 1$ ) steady state is stable if  $g' \geq -1 - 5g' \leq 0$

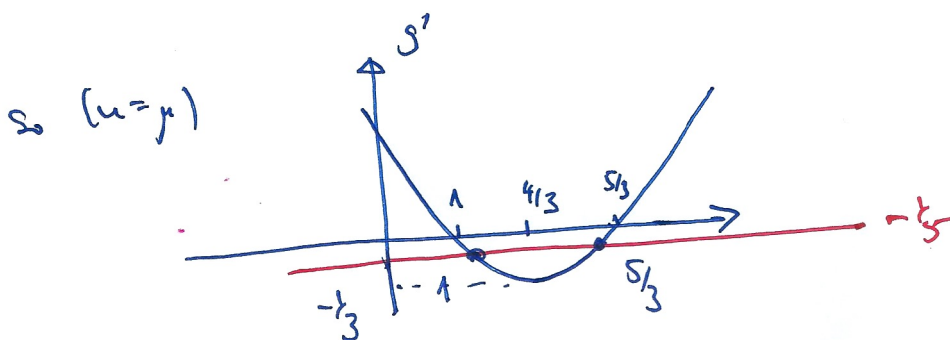
$$\text{ie } g' \geq -\frac{1}{5}$$

$$g' = [u^3 - 4u^2 + 5u]' = 3u^2 - 8u + 5$$

$$\begin{aligned} & \cancel{3u^2 - 8u + 5} \\ & = (u-1)(3u-5) \end{aligned}$$



$$\text{min } g' \text{ is at } u = \frac{4}{3}, \quad \text{min } g' = 3 \cdot \frac{16}{9} - \frac{32}{3} + 5 = \frac{15-16}{3} = -\frac{1}{3}$$



values of  $u$  where  $g' = -\frac{1}{5}$  :

$$3u^2 - 8u + 5 = -\frac{1}{5}$$

are  $3u^2 - 8u + \frac{26}{5} = 0$

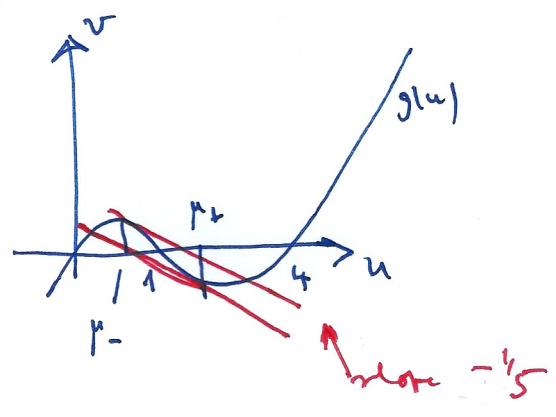
$$u = \frac{1}{6} \left[ 8 \pm \sqrt{64 - \frac{12 \cdot 26}{5}} \right]$$

$$= \frac{1}{6} \left[ 8 \pm \sqrt{\frac{320 - 312}{5}} \right]$$

$$= \frac{4}{3} \pm \frac{1}{3} \sqrt{\frac{8}{5}} = \mu_{\pm}$$

so for  $\mu_- \leq \mu \leq \mu_+$  steady state is unstable. ]

Back directly (perhaps all that is required)

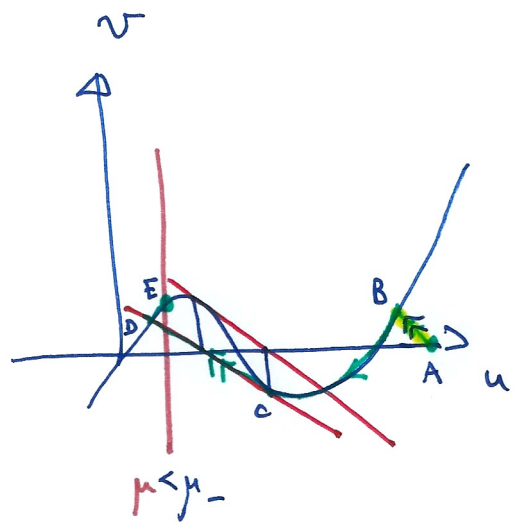


$$\dot{v} = f(u, v) = g(u) - v$$

$$(u + 5v) = \mu - u$$

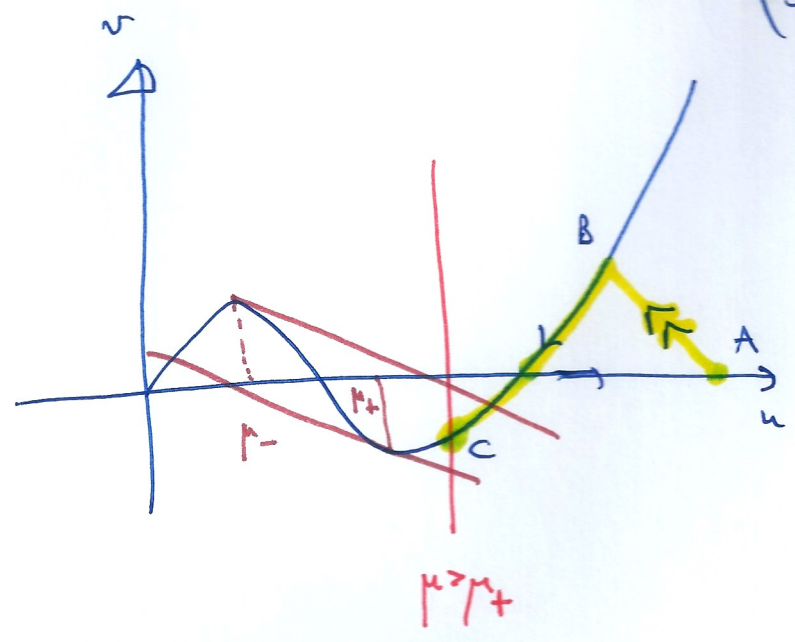
If we define  $\mu_{\pm}$  to be where  $g'(u) = -\frac{1}{5}$  (then as above)

then we will get relaxation oscillations for  $\mu_- < \mu < \mu_+$  :



$\mu < \mu_-$

trajectory follows  
ABCDE



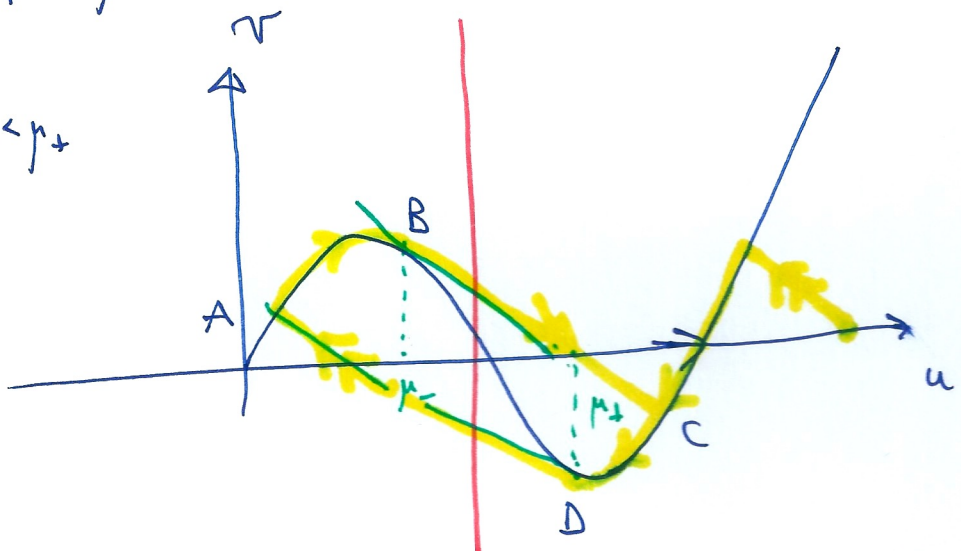
$\mu > \mu_+$

follows ABC

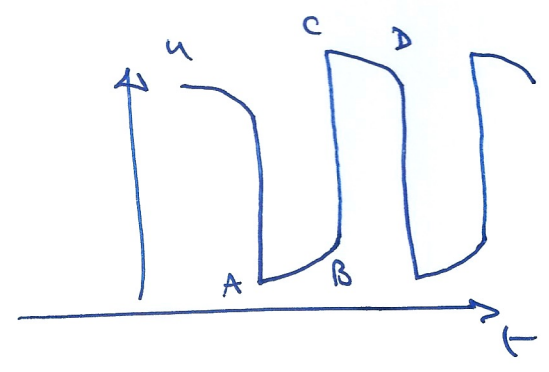
↑ fast ↓ slow

(ii)  $\mu_-, \mu_+$  close above

$\mu_- < \mu < \mu_+$

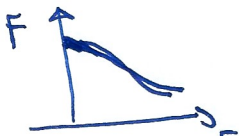


relaxation oscillation is ABCD



$$3) \dot{E} = F(E_\tau) - \gamma E$$

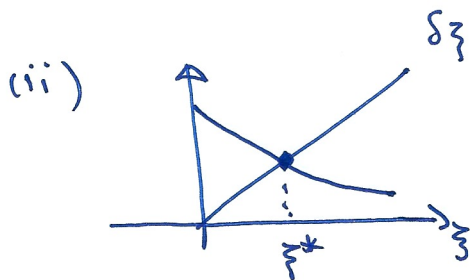
(a)  $E$ : erythrocytes produced at rate  $F$  which depends on  $E$  via feedback (eg. via Epo) to stem cells which take time  $\tau$  to mature:  $\gamma$  represents death rate of blood cells in circulation

(\*)  production is reduced  $\sim E$  increases which acts to control numbers

(c) (i)  $t \gg \tau$   $E = \theta \xi$ ,  $F = \frac{F_0 \theta^n}{(E_\tau + \theta)^n}$

$$\Rightarrow \frac{d}{dt} \xi = \frac{F_0}{(1 + \xi_1)^n} - \gamma \theta \xi$$

$$\Rightarrow \dot{\xi} = \frac{p}{(1 + \xi_1)^n} - \delta \xi \quad \left\{ \begin{array}{l} p = \frac{F_0 \tau}{\theta} \\ \delta = \gamma \tau \end{array} \right.$$

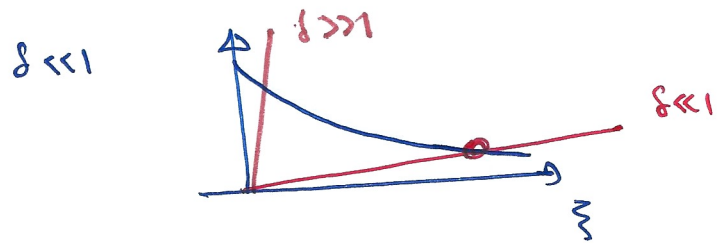


steady  $\frac{p}{(1 + \xi_1)^n} = \delta \xi$   
 $\uparrow$  decreasing  $\uparrow$  increasing  
 $\Rightarrow$  unique steady state



$$f(\xi) = \frac{1}{(1+\xi)^n}$$

$$\text{so } \xi = p f(\xi_1) - \delta \xi$$



$\xi^*$  is large

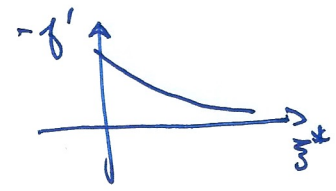
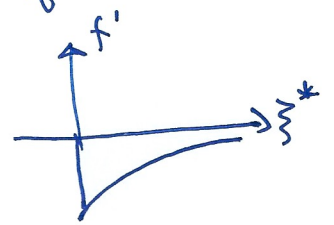
$$\frac{p}{(1+\xi)^n} = \delta \xi \Rightarrow \xi^* \approx \left(\frac{p}{\delta}\right)^{\frac{1}{n+1}} \quad \delta \ll 1$$

if  $\delta \gg 1, \xi \ll 1, \xi^* \approx \frac{p}{\delta} \quad \delta \gg 1$

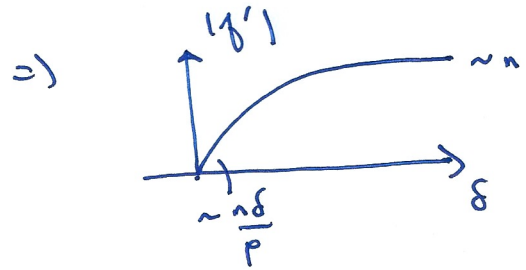
$$\text{so } f' = \left(\frac{1}{(1+\xi)^n}\right)' = \frac{-n}{(1+\xi)^{n+1}} \approx \frac{-n\delta}{p} \quad \delta \ll 1$$

$$\approx -n \quad \delta \gg 1$$

clearly  $f'$  is monotonic in  $\xi$



$\xi^*$  increases monotonically as  $\delta$  decreases  
 $\Rightarrow |f'|$  increases with  $\delta$



(iii)  $\delta \ll 1$ 

for further steady state  $\xi \approx \xi^* + X$

$$\Rightarrow \dot{X} = -p f'(\xi^*) X - \delta X$$

$$X = e^{\sigma t} \quad \sigma = -p f' e^{-\sigma} - \delta \quad \leftarrow \text{note this is fine}$$

$$\delta \ll 1, \quad p f' \approx n \delta$$

$$\Rightarrow \sigma \approx -\delta n e^{-\sigma} - \delta$$

Clearly for  $n < 1$  all roots have  $\text{Re } \sigma < 0$

$\sigma$  varies smoothly with  $n$

If instability occurs then  $\sigma = i\theta$  for some  $n$

$$\Rightarrow i\theta = -\delta n [\cos \theta - i \sin \theta] - \delta$$

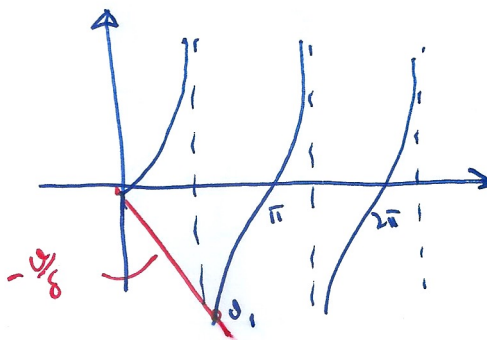
$$\Rightarrow \theta = \delta n \sin \theta$$

$$\delta n \cos \theta + 1 = 0$$

$$\text{or } -1 = n \cos \theta$$

$$\Rightarrow -\frac{\theta}{\delta} = \tan \theta$$

$$\text{then } n = \frac{-1}{\cos \theta}$$



Note when  $\delta \ll 1$

roots are  $\theta_1 = \frac{\pi}{2} + \phi_1 \quad \phi_1 \ll 1$

$\theta_2 = \frac{3\pi}{2} + \phi_2 \quad \phi_2 \ll 1$

:

$\theta_m = (m - \frac{1}{2})\pi + \phi_m \quad \phi_m \text{ decreases with } m$

so  $-\frac{1}{\cos \theta_m} = \frac{-1}{(-1)^m \cos(-\frac{1}{2}\pi + \phi_m)}$

$= \frac{(-1)^{m+1}}{\sin \phi_m}$

only interested in  $m$  odd

consequently  $n_m = \frac{1}{\sin \phi_m} \quad m \text{ odd}$

$\phi_m$  decreases with  $m$

so does  $\sin \phi_m (\approx \phi_m)$

so  $n_m$  increases with  $m$

so  $\min_{m \text{ odd}} n_m = n_1$

we have  $-\frac{\theta}{\delta} \approx \tan \theta \quad \theta_1 = \frac{\pi}{2} + \phi_1$

$-\frac{\pi}{2\delta} \approx \frac{\cos \phi_1}{-\sin \phi_1} \approx -\frac{1}{\phi_1} \Rightarrow \phi_1 \approx \frac{2\delta}{\pi}$

$\Rightarrow n_1 \approx \frac{-1}{\cos \theta_1} = \frac{1}{\sin \phi_1} \approx \frac{\pi}{2\delta}$

So the steady state is unstable for  $n \geq \frac{1}{2\delta}$

(5)

(assuming some approximate works).

Transversality  $\sigma(n)$

$$\sigma = -\delta n e^{-\sigma} - \delta$$

$$\sigma' = -\delta e^{-\sigma} + \delta n e^{-\sigma} \sigma'$$

$$= \frac{\sigma + \delta}{n} - (\sigma + \delta) \sigma'$$

$$\Rightarrow \sigma' = \frac{1}{n} \left[ \frac{\sigma + \delta}{\sigma + \delta + 1} \right]$$

$$\text{at } \sigma = i0 \quad \sigma' = \frac{1}{n} \left[ \frac{(1+\delta-i0)(\delta+i0)}{(1+\delta)^2 + 0^2} \right]$$

$$= \frac{1}{n} \left[ \frac{\delta + i0 + \delta^2 + 0^2}{(1+\delta)^2 + 0^2} \right]$$

$\Rightarrow \text{Re } \sigma' > 0$  transversality.

[ Actually the part ii is a bit off-putting. Linear stability

is  $\sigma = -p|f'| e^{-\sigma} - \delta = -\beta e^{-\sigma} - \delta$  say in any case  
 so all the above, replacing  $\delta_n$  by  $p|f'| = \beta$  still works, so the

condition is  $p|f'| \geq \frac{1}{2}$  - independently of whether the

approximation for  $f'$  still works. In fact if you put  $p|f'| = \frac{1}{2}$

you find  $\sigma^* = \frac{1}{2\beta - 1}$  which is 0(1) if  $\beta = 0(1)$  so (ii) seems irrelevant ]

# Mathematical Physiology Feb 2018-2019

C

## Answers

B = bookwork

V = variant of <sup>or similar to</sup> material seen before (e.g. on problem sheet)

N = new

1. (a)

$S$  = concentration of ion

so  $-D \nabla S$  is diffusive flux

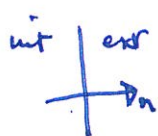
$V$  = electrical potential

drives current  $\propto -\nabla V$

At each ion moves in the direction of  $-\nabla V$  at a rate  $u$  (if positively charged) or  $-u$  (if negatively charged), i.e. at rate  $u z q n z$ ,  $z$  = valency, and thus the ionic flux due to  $V$  is  $-u z q n z S \nabla V$

Total flux is  $\underline{J} = -D \nabla S - u z q n z S \nabla V$

In equilibrium  $\underline{J} = 0$  & across a membrane this gives



$$-D \frac{\partial S}{\partial n} - u z q n z S \frac{\partial V}{\partial n} = 0$$

$$\text{i.e. } -\frac{\partial V}{\partial n} = \frac{D}{u z q n z} \frac{1}{S} \frac{\partial S}{\partial n}$$

$$\Rightarrow -[V]_i^e = \frac{D}{u z q n z} [\ln S]_i^e$$

with  $u = \frac{|z| F D}{RT}$

$$\frac{D}{u z q n z} = \frac{D}{|z| z q n z F D} = \frac{RT}{F z}$$

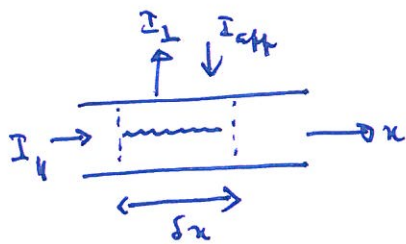
$$V = [V]_e^i = \frac{RT}{zF} \ln \frac{S_e}{S_i}$$

(5)

(B)

(b)

(2)



If  $V$  is the <sup>(internal)</sup> potential then  $CV \delta x$  is the charge in the segment  $(x, x + \delta x)$ ,  $C =$  capacitance per unit length

So conservation of charge gives

$$\frac{\partial}{\partial t} CV \delta x = -I_r \delta x + I_t \delta x + I_{||}|_x - I_{||}|_{x+\delta x}$$

$$\text{Hence } \underline{C \frac{\partial V}{\partial t} = -I_r + I_t - \frac{\partial I_{||}}{\partial x}}$$

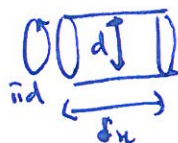
The axial current is given by Ohm's law:

$$V|_x - V|_{x+\delta x} = I_{||} R \delta x \quad \text{where } R = \text{resistance per unit length,}$$

$$\therefore I_{||} = -\frac{1}{R} \frac{\partial V}{\partial x}$$

$$\Delta \quad \underline{C V_t = -I_r + I_t + \frac{1}{R} V_{xx}}$$

(5) (B)



If  $C_m$  is the capacitance per unit area, then  $\bar{u} d \delta x C_m = \delta x C$

$$\text{i.e. } \underline{C = \bar{u} d C_m}$$

(c)

$$I_i = g_{Na} m^3 h (V - V_{Na}) + g_K n^4 (V - V_K) + g_L (V - V_L)$$

is current per unit area. Thus  $\pi dx I_i = I_{\perp}$ , i.e.  $I_{\perp} = \pi dx I_i$

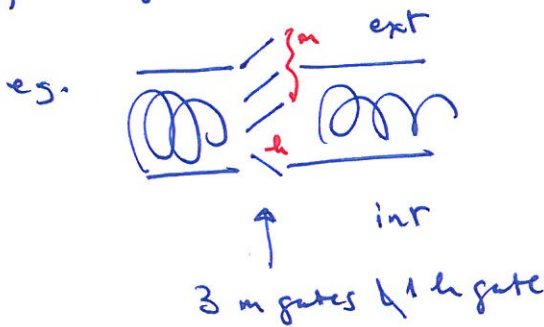
Each term is an ionic flux due to sodium (Na),

potassium (K) and leakage (L) - (mostly) chloride <sup>e.g.</sup>

$g_{Na}$  etc are conductances

$V_{Na}$  etc are Nernst potentials

$m, h, n$  are gate variables



$m^3 h$  is the proportion of open channels with 3 m gates & 1 h gate.

Gate equations:  $\tau_k \dot{h} = h_{\infty}(V) - h$

for  $h = m, n, l$ .

$$\tau_m \dot{m} = m_{\infty} - m$$

$$\tau_n \dot{n} = n_{\infty} - n$$

$$\tau_h \dot{h} = h_{\infty} - h$$

$\tau_m \ll \tau_n, \tau_h \Rightarrow m \rightarrow m_{\infty}$  rapidly  $\Rightarrow m \approx m_{\infty}(V)$

$\tau_n = \tau_h, m_{\infty} + h_{\infty} = \bar{h} \Rightarrow \tau_n(n+h) = \bar{h} - (n+h)$

$\Rightarrow n+h \rightarrow \bar{h}$  so that  $n+h = \bar{h}$

(6) (B)

(d)

$$V - V_{eq} = (V_{Na} - V_{eq})v \quad t \sim \tau_n \quad v \sim 1$$

$$\Rightarrow V - V_{Na} = V_{eq} - V_{Na} + (V_{Na} - V_{eq})v$$

$$\text{write } \Delta V = V_{Na} - V_{eq}$$

$$\Rightarrow V - V_{Na} = \Delta V (v - 1)$$

$$V - V_K = V_{eq} - V_K + \Delta V v$$

$$V - V_L = V_{eq} - V_L + \Delta V v$$

$$\text{Define } \begin{aligned} V_{eq} - V_K &= \Delta V_K = 12 \text{ mV} \\ V_L - V_{eq} &= \Delta V_L = 10.6 \text{ mV} \\ \Delta V &= 115 \text{ mV} \end{aligned}$$

$$\text{so } V - V_{Na} = \Delta V (v - 1)$$

$$V - V_K = \Delta V \left( v + \frac{\Delta V_K}{\Delta V} \right)$$

$$V - V_L = \Delta V \left( v - \frac{\Delta V_L}{\Delta V} \right)$$

$$\text{Define } \begin{aligned} v_K^* &= \frac{\Delta V_K}{\Delta V} = \frac{12}{115} \sim 0.1 \\ v_L^* &= \frac{\Delta V_L}{\Delta V} = \frac{10.6}{115} \sim 0.09 \end{aligned} \quad \left. \vphantom{\begin{aligned} v_K^* \\ v_L^* \end{aligned}} \right\}$$

$$\begin{aligned} \text{Then } I_i &= g_{Na} m^3 h \Delta V (v - 1) + g_K n^4 \Delta V (v + v_K^*) + g_L \Delta V (v - v_L^*) \\ &= g_{Na} \Delta V \left[ -(1 - v) m^3 h + \gamma_K n^4 (v + v_K^*) + \gamma_L (v - v_L^*) \right] \end{aligned}$$

$$\gamma_K = \frac{g_K}{g_{Na}} = \frac{36}{120} = 0.3$$

$$\gamma_L = \frac{g_L}{g_{Na}} = \frac{0.3}{120} = \frac{3 \times 10^{-1}}{1.2 \times 10^2} = 2.5 \times 10^{-3}$$



Thus, with  $I_i = g_{Na} \Delta V I_i^*$

(5)

$$I_i^* = -(1-\nu)m^3 k + \gamma k^{n+1} (\nu + \nu k^*) + \gamma_L (\nu - \nu_L^*)$$

The cable equation is (max-d)

$$\frac{C}{\tau_n} \Delta V \nu_t = I_{app} - \pi d g_{Na} \Delta V I_i^* + \frac{1}{R} \frac{\Delta V}{l^2} \nu_{xx}$$

Thus with  $I_i^* = \frac{I_{app}}{\pi d g_{Na} \Delta V}$ , this is

$$\frac{C}{\pi d \tau_n g_{Na}} \nu_t = I_i^* - \frac{I_i^*}{\tau_n} + \frac{1}{\pi d R l^2 g_{Na}} \nu_{xx}$$

So we define  $(C = \pi d C_m)$

$$\Sigma = \frac{C_m}{\tau_n g_{Na}} = \frac{10^{-6}}{5 \cdot 10^{-3} \cdot 120 \cdot 10^{-3}} \frac{F \text{ cm}^2}{\text{cm}^2 \text{ s S}}$$

$$= \frac{1}{600} = \frac{1}{6 \times 10^2} \sim 0.16 \times 10^{-2}$$

and  $\frac{1}{\pi d R l^2 g_{Na}} = \Sigma^2 = \frac{C_m^2}{(\tau_n g_{Na})^2}$

$$\Rightarrow l = \frac{1}{\sqrt{\pi d R g_{Na}}} \frac{\tau_n g_{Na}}{C_m} = \frac{\tau_n}{C_m} \sqrt{\frac{g_{Na}}{\pi d R}}$$

$$= \frac{5 \cdot 10^{-3}}{10^{-6}} \left( \frac{0.12 \cdot 10^{-4}}{3.14 \times 5 \times 10^{-2} \cdot 1.5 \text{ cm}^2 \text{ cm}^{-2} \text{ s}^{-1}} \right)^{1/2} \frac{\text{s cm}^2}{F}$$

$$= 5 \times 10^3 \left( \frac{12}{15.7} \right)^{1/2} \frac{\text{s}}{\text{cm}} \frac{\text{s cm}^2}{F}$$

$$\sim 50 \times \frac{\sqrt{3}}{2} \text{ cm} \sim 43 \text{ cm}$$

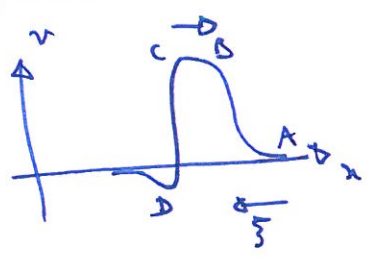
(5) (V)

(e)  $\mathcal{D}^* = 0$

$$\epsilon v_f = -g(v, n) + \epsilon^2 v_{xx}$$

$$n_f = n_0 - n$$

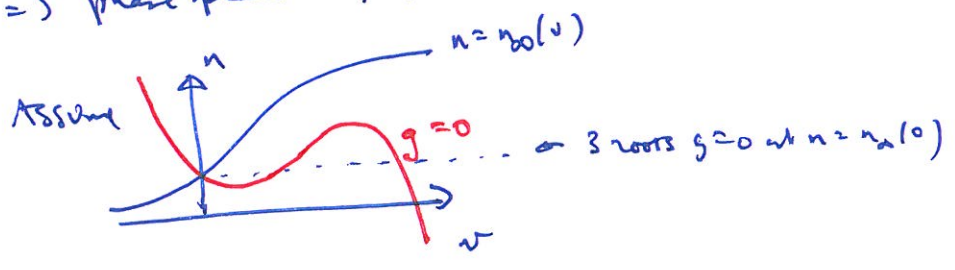
travelling wave  $n, v$  function of  $\xi = \text{const } ct - x, c > 0$



$$\Rightarrow \epsilon c v' = -g + \epsilon^2 v''$$

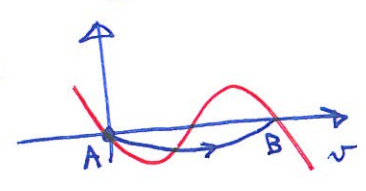
$$c n' = n_0 - n$$

$\Rightarrow$  phase plane  $n, v, v'$



Fast phase  $\xi = \epsilon X : c v' = -g + v''$ ,  $n \approx \text{constant}$

phase plane

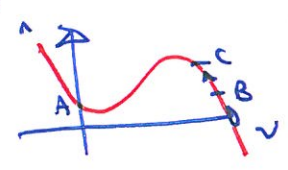


$$v' = -w$$

$$w' = cw - g$$

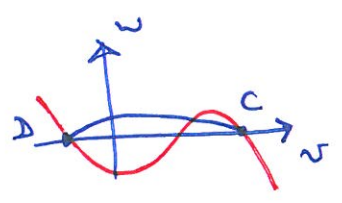
pick C so  $A \rightarrow B$

Slow phase  $g \geq 0$   $c n' = n_0 - n$

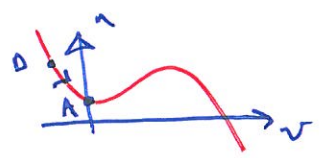


$B \rightarrow C, n = n^*$  to be found

fast phase: pick  $n^* \Rightarrow C \rightarrow D$



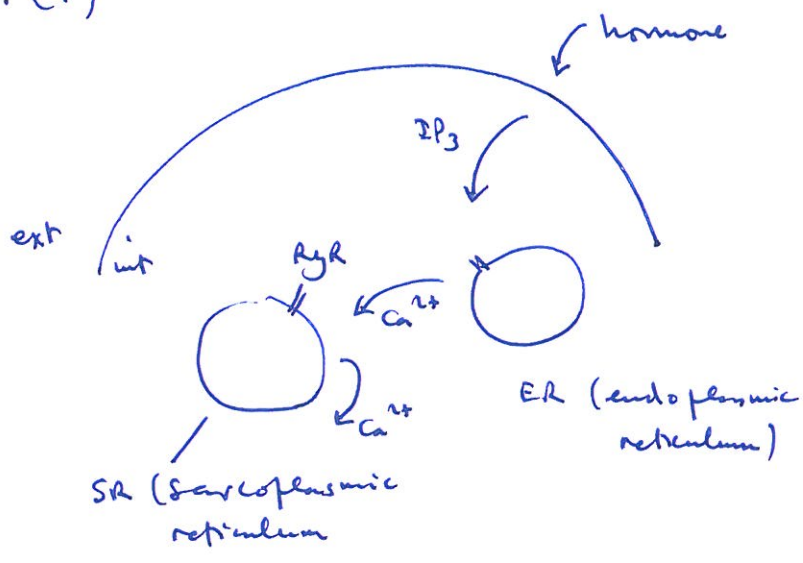
Slow phase  $D \rightarrow A$



4

5

2. (a)



Stimulation of a cell by an agonist causes release of IP<sub>3</sub> to the ER, which releases Ca<sup>2+</sup> to the SR which releases stored Ca<sup>2+</sup>.

Model

$$\dot{c} = r - kc - [J_+ - J_- - k_5 c_s]$$

$$\dot{c}_s = J_+ - J_- - k_5 c_s = J, \text{ say}$$

$$J_+ = \frac{V_1 c^n}{K_1^n + c^n} \quad J_- = \frac{V_2 c_s^m}{K_2^m + c_s^m} \cdot \frac{c^p}{K_3^p + c^p}$$

$$J = \frac{V_1 c^n}{K_1^n + c^n} - \frac{V_2 c_s^m}{K_2^m + c_s^m} \cdot \frac{c^p}{K_3^p + c^p} - k_5 c_s$$

Balances as shown: scale  $t \sim \frac{1}{k}$ ,  $c = K_1 u$ ,  $c_s = k_2 v$

$$J = V_2 f$$

then  $k_1 u = r - k_1 u - V_2 f$

$k_2 v = V_2 f$

$V_2 f = V_1 \frac{u^n}{1+u^n} - \frac{V_2 v^m}{1+v^m} \cdot \frac{u^p}{(\frac{k_3 v}{K_1}) + u^p} - k_3 k_2 v$

Thus  $\dot{u} = \mu - u - \gamma v$

$\dot{v} = f$

$f = F(u) - \frac{G(u)v^m}{1+v^m} - \delta v, \quad F = \frac{\beta u^n}{1+u^n}, \quad G = \frac{\alpha u^p}{\alpha p + u^p}$

$\mu = \frac{r}{k_1}, \quad \frac{\gamma}{\epsilon} = \frac{V_2}{k_1}, \quad \epsilon = \frac{k_2 k_2}{V_2} \Rightarrow \gamma = \frac{k_2}{K_1}$

$\beta = \frac{V_1}{V_2}, \quad \alpha = \frac{K_3}{K_1}, \quad \delta = \frac{k_3 k_2}{V_2}$

10 B

(b)  $\alpha = \frac{K_3}{K_1} = 0.9, \quad \beta = \frac{65}{500} = 0.13, \quad \gamma = 2, \quad \delta = \frac{1 \times 2 \text{ s}^{-1} \mu\text{M}}{500 \mu\text{M s}^{-1}} = 0.004$   
 $\epsilon = \frac{10 \times 2}{500} \frac{\text{s}^{-1} \mu\text{M}}{\mu\text{M s}^{-1}} = 0.04$

2 B

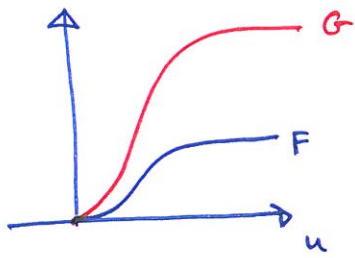
(c) Since  $\delta \ll 1, f \approx 0$  if  $\frac{v^m}{1+v^m} = \frac{F(u)}{G(u)}$

↳ this is  $v = V(u)$ ,  $V$  has same shape as  $F/G$

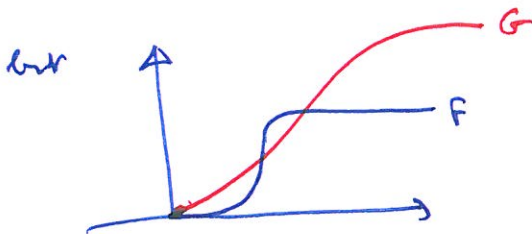
as  $\frac{v^m}{1+v^m}$  is monotonically increasing ( $A < 1$ , but this is ok if  $F/G < 1$ )

~~1/11~~)  $m=2, n=4, p=2$

so  $f = F(u) = \frac{\alpha(u)u^2}{1+u^2} - \delta u$ ,  $F = \frac{\beta u^4}{1+u^4}$ ,  $G = \frac{u^2}{\alpha^2+u^2}$



possible:  $F < G$  initially & finally  
(& then  $F < G$ )



is possible if  $F=G$  has 2 true roots

In the latter case  $\frac{\beta u^4}{1+u^4} = \frac{u^2}{\alpha^2+u^2}$

$$\Rightarrow \beta u^2(\alpha^2+u^2) = 1+u^4$$

$$\Rightarrow (1-\beta)u^4 - \beta\alpha^2 u^2 + 1 = 0$$

$$\Rightarrow u^2 = \frac{1}{2(1-\beta)} \left[ \beta\alpha^2 \pm \left\{ \beta^2\alpha^4 - 4(1-\beta) \right\}^{1/2} \right]$$

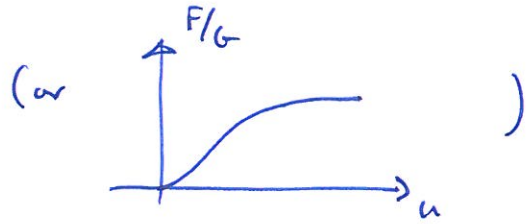
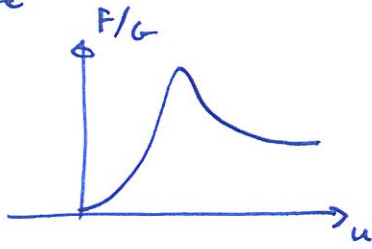
has 2 true roots iff  $\beta^2\alpha^4 > 4(1-\beta)$

$$\text{i.e. } \alpha^2 > \frac{2}{\beta}(1-\beta)^{1/2}$$

$$\sim \alpha > \sqrt{\frac{2}{\beta}}(1-\beta)^{1/4}$$

so  $F < G$  (1st picture) if  $\alpha < \sqrt{\frac{2}{\beta}}(1-\beta)^{1/4}$

In that case



to show  $F/G$  has a maximum, show  $(F/G)' = 0$  has a true root

$$\text{i.e. } F'G - FG' = 0$$

do these derivatives wrt  $\xi = u^2$ ,  $F = \frac{\beta \xi^2}{1 + \xi^2}$ ,  $G = \frac{\alpha}{\alpha^2 + \xi}$

$$\Rightarrow F' = \frac{2\beta\xi}{1 + \xi^2} - \frac{2\beta\xi^3}{(1 + \xi^2)^2} = \frac{2\beta\xi}{(1 + \xi^2)^2}$$

$$G' = \frac{1}{\alpha^2 + \xi} - \frac{\xi}{(\alpha^2 + \xi)^2} = \frac{\alpha^2}{(\alpha^2 + \xi)^2}$$

no need  $\frac{\beta \xi^2}{1 + \xi^2} \cdot \frac{\alpha^2}{(\alpha^2 + \xi)^2} = \frac{2\beta\xi}{(1 + \xi^2)^2} \cdot \frac{\xi}{\alpha^2 + \xi}$

$F \quad G' \quad = \quad F' \quad G$

$$\div \beta \xi^2 \quad \text{i.e.} \quad \frac{\alpha^2}{\xi} (1 + \xi^2) = 2(\alpha^2 + \xi)$$

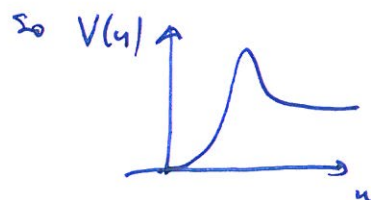
$$\text{i.e. } \alpha^2 \xi^{-1} - 2\xi - \alpha^2 = 0$$

$$\Rightarrow \xi = \frac{1}{\alpha^2} \left[ 1 \pm \sqrt{1 + \alpha^2} \right]^{1/2}$$

$$= u^2$$

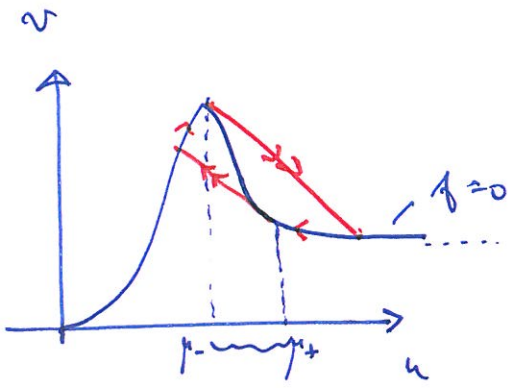
$$\text{So } u = \frac{1}{\alpha} \left[ 1 + (1 + \alpha^2)^{1/2} \right]^{1/2} \quad \text{there is always a maximum}$$

10  $V/N$



Small  
max  $f/g < 1$

(d)



$$u + \gamma v = \mu - u$$

$$\gamma v = \gamma$$

$v$  rapidly  $\rightarrow f=0$  along  $u + \gamma v = \text{constant}$

A few oscillations as shown by  $\mu - \gamma < \mu < \mu + \gamma$

$v_{\text{max}}$  needs to be large enough so that lines  $\frac{dv}{du} = -\frac{1}{\gamma}$  can

reverse  $f=0$  as shown.

3  $v/N$

3/ (a)

$$\sigma = -\beta - \gamma e^{-\sigma}$$

Consider the function  $(\sigma + \beta)e^{\sigma} = f(\sigma)$

This has an essential singularity at  $\infty$

$$f = 0 \text{ at } \sigma = -\beta$$

Therefore in any neighborhood of  $\infty$   $f = -\gamma$  has a root

$\Rightarrow \exists \infty$  roots of  $\sigma = -\beta - \gamma e^{-\sigma}$  as  $\sigma \rightarrow \infty$

As  $\sigma \rightarrow \infty$ , we must have  $e^{-\sigma} \rightarrow 0 \Rightarrow \text{Re } \sigma \rightarrow -\infty$

Actually  $\sigma(\gamma)$  is analytic,

$$\sigma' = -e^{-\sigma} + \gamma e^{-\sigma} \sigma' \Rightarrow \sigma' = \frac{-e^{-\sigma}}{1 - \gamma e^{-\sigma}} = \frac{1}{\gamma - e^{\sigma}}$$

Evidently there are singularities (branch points) when  $\gamma e^{-\sigma} = 1$ , but at such values  $\sigma = -\beta - 1$  is real (4-ve), so the complex roots vary analytically with  $\gamma$ .

If  $\gamma$  is small, then  $\sigma = -\beta + O(\gamma)$ ,  $\text{Re } \sigma < 0$ , unless

$e^{-\sigma}$  is large - which requires  $\text{Re } \sigma < 0$ ;

so  $\text{Re } \sigma < 0 \forall$  small  $\gamma$ .

$$\text{From above, if } \sigma = i\omega, \text{Re } \frac{d\sigma}{d\gamma} = \frac{d \text{Re } \sigma}{d\gamma} = \text{Re} \left[ \frac{1}{\gamma - e^{\sigma}} \right] = \text{Re} \left[ \frac{1}{\gamma + \frac{\gamma}{\sigma + \beta}} \right] \\ = \text{Re} \left[ \frac{i\omega + \beta}{i\gamma\omega + \gamma(1+\beta)} \right] = \text{Re} \left[ \frac{(i\omega + \beta)\{-i\gamma\omega + \gamma(1+\beta)\}}{\gamma^2(1+\beta)^2 + \gamma^2\omega^2} \right] = \frac{\beta\gamma(1+\beta) + \gamma\omega^2}{\gamma^2(1+\beta)^2 + \gamma^2\omega^2} > 0$$



Hence  $\text{Re } \sigma > 0$  for  $\gamma > \gamma_c$

where  $\gamma_c$  is smallest root of  $i\omega = -\beta - \gamma e^{-i\omega}$

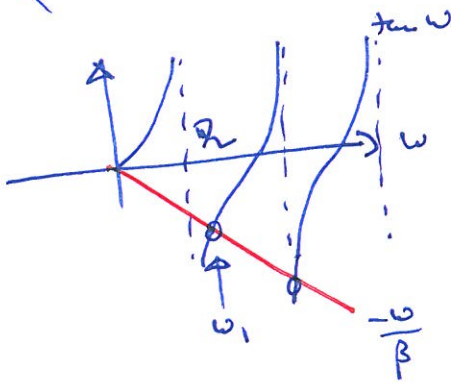
i.e.  $\omega = \gamma \sin \omega$ ,  $0 = -\beta - \gamma \cos \omega$   
 $\Rightarrow -\beta = \gamma \cos \omega$

thus  $-\frac{\omega}{\beta} = \tan \omega$  determines  $\omega$  given  $\beta$

(then  $\gamma = \frac{\omega}{\sin \omega}$ )



so  $\gamma$  increases as  $\omega$  increases (can elaborate...)



gives a sequence  $\omega_1 < \omega_2 < \dots$  (corresponding  $\gamma_1 < \gamma_2 < \dots$ )

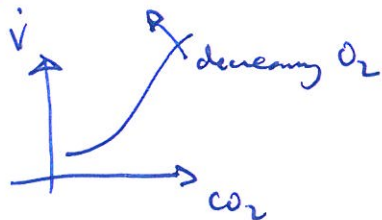
As  $\beta \rightarrow 0$ ,  $\omega_1 \rightarrow \frac{\pi}{2} \Rightarrow \gamma_1 = \gamma_c = \frac{\pi}{2}$

10 B/V


(b) minute ventilation: volume of air inspired in a minute,  $\dot{V}$

central chemoreceptor responds (via  $H^+$ ) to  $CO_2$

peripheral chemoreceptor responds to  $O_2$ , modulated by  $CO_2$



4 B

Cheyne-Stokes: periodic with apnea  
lung volume 

(5)

$$\dot{p} = M - p G [p_\tau - p_0]$$

M metabolic CO<sub>2</sub> production rate

K compartment (tissue) volume

G gain of controller

$$p_\tau = p_{CO_2}(t - \tau)$$

Steady  $M = p G (p - p_0)$  (as  $p > p_0$ )

$$\frac{M}{G p_0^2} = \frac{p}{p_0} \left( \frac{p}{p_0} - 1 \right) \text{ is small,}$$

$$\text{so } \frac{p}{p_0} = 1 + \frac{M}{G p_0^2} \cdot \frac{p_0}{p}$$

$$\frac{p}{p_0} \approx 1 \text{ so } \frac{p}{p_0} \approx 1 + \frac{M}{G p_0^2}, \quad \underline{p \approx p_0 + \frac{M}{G p_0} = p^*}$$

6 B/v

(d)  $p = p^* + P$ , linear ...

$$\dot{p} = M - p^* G p_\tau - P G (p^* - p_0)$$

$$P = e^{\sigma t / \tau} \Rightarrow \frac{K \sigma}{\tau} = -p^* G e^{-\sigma} - G (p^* - p_0)$$

$$\text{or } \sigma = -\frac{p^* G \tau}{K} e^{-\sigma} - \frac{G \tau}{K} (p^* - p_0)$$

$$= -\beta - \gamma e^{-\sigma} \quad \underline{\gamma = \frac{p^* G \tau}{K}}, \quad \underline{\beta = \frac{G \tau}{K} (p^* - p_0)}$$

If  $M \ll G \rho_0^2$ , then

$$\gamma \approx \frac{\rho_0 G \tau}{K}, \quad \beta \approx \frac{G \tau}{K} \frac{M}{G \rho_0} = \frac{M \tau}{K \rho_0}$$

note that  $\frac{\beta}{\gamma} = \frac{M \tau}{K \rho_0} \cdot \frac{K}{\rho_0 G \tau} = \frac{M}{G \rho_0^2} \ll 1$

so  $\beta \ll \gamma$ .

Assuming  $\beta \ll 1$  then instability occurs if  $\gamma \geq \frac{1}{2}$

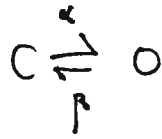
Since  $\gamma = O(1)$  at this value, then indeed  $\beta \ll 1$ .

This criterion is  $\frac{\rho_0 G \tau}{K} \geq \frac{1}{2}$  i.e.  $\tau \geq \frac{K}{2 \rho_0 G}$

(5) (v/N)

B = broodwork  
 V = variant / homework  
 N = new

1(a)



n open gates so  $n = \alpha(1-n) - \beta n$   
 $= \alpha - (\alpha + \beta)n$

4 B

$n \rightarrow n_{\infty} = \frac{\alpha}{\alpha + \beta} \rightarrow t \rightarrow \infty$

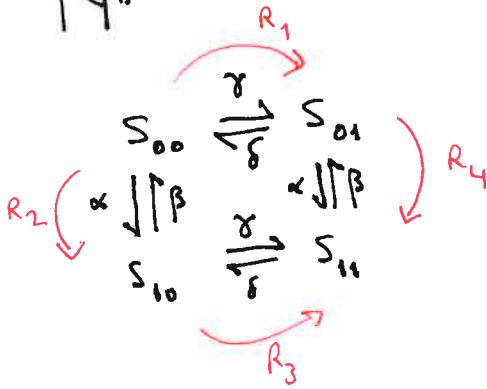
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(b)



$S_{ij}$  : i open H gates  
 j open H gates (fraction)

Reaction scheme



Overall reaction rates

$$R_1 = \gamma S_{00} - \delta S_{01}$$

$$R_2 = \alpha S_{00} - \beta S_{10}$$

$$R_3 = \gamma S_{10} - \delta S_{11}$$

$$R_4 = \alpha S_{01} - \beta S_{11}$$

rate equations

$$\dot{S}_{00} = -R_1 - R_2$$

$$\dot{S}_{01} = R_1 - R_4$$

$$\dot{S}_{10} = R_2 - R_3$$

$$\dot{S}_{11} = R_3 + R_4$$

Adding, we see  $\sum S_{ij} = \text{constant} = 1$

$$h = S_{01} + S_{11}$$

$$m = S_{10} + S_{11}$$

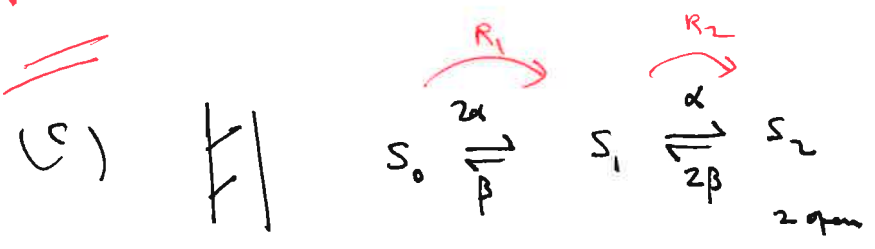
$$\Rightarrow 1-h = S_{10} + S_{00}$$

$$1-m = S_{01} + S_{00}$$

$$\begin{aligned} \Rightarrow \dot{h} &= \dot{S}_{01} + \dot{S}_{11} = R_1 - R_4 + R_3 + R_4 = R_1 + R_3 \\ &= \gamma(S_{00} + S_{10}) - \delta(S_{01} + S_{11}) \\ &= \gamma(1-h) - \delta h \end{aligned}$$

$$\begin{aligned} \Delta \dot{m} &= \dot{S}_{10} + \dot{S}_{11} = R_2 + R_4 = \alpha(S_{00} + S_{01}) - \beta(S_{10} + S_{11}) \\ &= \alpha(1-m) - \beta m \end{aligned}$$

8 ✓



$$\begin{aligned} R_1 &= 2\alpha S_0 - \beta S_1 \\ R_2 &= \alpha S_1 - 2\beta S_2 \end{aligned}$$

$$\begin{aligned} \dot{S}_0 &= -R_1 \\ \dot{S}_1 &= R_1 - R_2 \\ \dot{S}_2 &= R_2 \end{aligned}$$

$$S = S_0 + S_1 x + S_2 x^2$$

$$\Rightarrow S_f = -R_1 + (R_1 - R_2)x + R_2 x^2 = (x-1)[R_1 + R_2 x]$$

$$\Delta S_2 = S_1 + 2S_2 x$$

~~$$\begin{aligned} S &= -2\alpha S_0 + \beta S_1 + 2\alpha S_0 x - \beta S_1 x + \alpha S_1 x + 2\beta S_2 x + \alpha S_1 x^2 - 2\beta S_2 x^2 \\ &= 2\alpha S_0(x-1) - \beta S_1(x-1) + \alpha S_1 x(x-1) - 2\beta S_2 x(x-1) \\ &= (x-1) [2\alpha S_0 - \beta S_1 + \alpha S_1 x - 2\beta S_2 x] \\ &= (x-1) [2\alpha S_0 + 2\alpha S_1 x + 2\alpha S_2 x^2 - \alpha S_1 x - \beta S_1 + 2\beta S_2 x - 2\alpha S_2 x^2] \\ &= (x-1) [2\alpha S - \alpha x(S_1 + 2S_2 x)] \end{aligned}$$~~

$$S_0 \quad S_t = (x-1) \left[ (2\alpha S_0 + \beta S_1) + (\alpha S_1 - 2\beta S_2)x \right]$$

$$= (x-1) \left[ 2\alpha S_0 + 2\alpha S_1 x + 2\alpha S_2 x^2 - 2\alpha S_1 x - 2\alpha S_2 x^2 - \beta S_1 + \alpha S_1 x - 2\beta S_2 x \right]$$

$$= (x-1) \left[ 2\alpha S_0 + S_1 [-\beta - \alpha x] - 2S_2 x (\beta + \alpha x) \right]$$

$$= (x-1) \left[ 2\alpha S_0 - (\beta + \alpha x)(S_1 + 2S_2 x) \right]$$

$$= (x-1) \left[ 2\alpha S_0 - (\beta + \alpha x) S_x \right]$$

$$\text{Try } S = [1-g(t)+s(t)x]^2$$

$$\Rightarrow S_t = 2[1-g+sx](x-1)\dot{g}$$

$$S_x = 2[1-g+sx]g$$

$$\text{So we require } 2(1-g+sx)(x-1)\dot{g} = (x-1) \left[ 2\alpha \{1-g+sx\}^2 - (\beta + \alpha x) \cdot 2\{1-g+sx\}g \right]$$

$$\text{Use } \dot{g} = \alpha(1-g+sx) - (\beta + \alpha x)g \\ = \alpha(1-g) - \beta g$$

$$\text{For this solution } S = (1-g)^2 + 2g(1-g)x + g^2 x^2$$

$$\Rightarrow \underline{S_2 = g^2}$$

8 B/N  
==

(d)

$$\text{If } S = [1 - g + gx]^2 + u(x, t)$$

$$S(1, t) = 1 + u(1, t) = S_0 + S_1 + S_2 = 1 \Rightarrow u(1, t) = 0$$

We have

$$S_t + (\lambda - 1)(\alpha x + \beta) S_x = 2\alpha(\lambda - 1)S$$

$$S = (1 - g + gx)^2 \text{ is a solution of } g = \alpha(1 - g) - \beta g$$

Eq is linear so

$$u_t + (\lambda - 1)(\alpha x + \beta) u_x = 2\alpha(\lambda - 1)u$$

$$\text{Characteristics } \dot{x} = (\lambda - 1)(\alpha x + \beta)$$

$$\dot{u} = 2\alpha(\lambda - 1)u$$

$$\text{B.c. } x=1, t=0, u=0$$

$$u = u_0(x) \text{ at } t=0$$

$$u = u_0(\sigma), x = \sigma, t = 0$$

$$\frac{dx}{\alpha x + \beta} \left[ \frac{1}{x-1} - \frac{\alpha}{\alpha x + \beta} \right] = dt$$

$$\ln \left( \frac{x-1}{\alpha x + \beta} \right) = \ln \left( \frac{\sigma-1}{\alpha \sigma + \beta} \right) + (\alpha + \beta)t$$

$$\Rightarrow \frac{x-1}{\alpha x + \beta} = \frac{\sigma-1}{\alpha \sigma + \beta} e^{(\alpha + \beta)t}$$

$$\text{Then } \frac{du}{dx} = \frac{2\alpha u}{\alpha x + \beta} \Rightarrow \ln u = 2 \ln(\alpha x + \beta) + \dots$$

$$\Rightarrow u = u_0(\sigma) \left( \frac{\alpha x + \beta}{\alpha \sigma + \beta} \right)^2$$

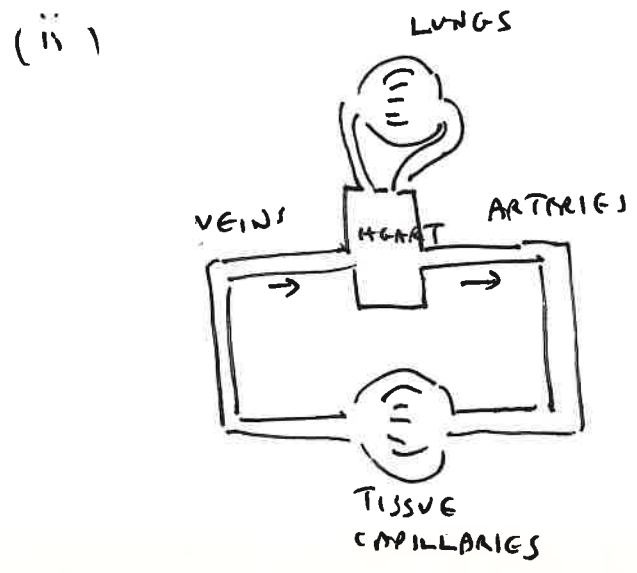
Note when  $x=1, \sigma=1, u=0 \Rightarrow u_0(1)=0$  (or just  $u(1, t)=0$  at  $t=0$ )

As  $t \rightarrow \infty, \sigma \rightarrow 1 \Rightarrow u \rightarrow 0. \square$

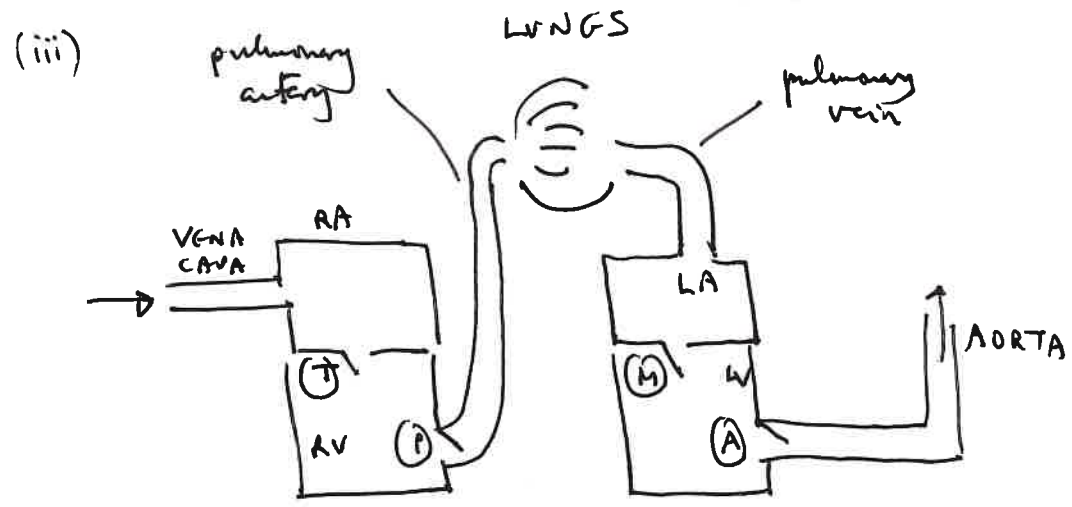
(5) N



(i) Periodic action potentials occur in the sinoatrial node and the resultant signal is propagated through the myocardium causing contraction of the heart muscle cells



Contracting of the heart causes blood to flow from the heart to the lungs where it collects oxygen, back to the heart, where it is expelled to the arteries, then tissues & back to the heart via the veins.

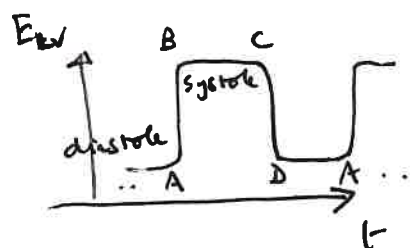


- vals:
- |              |                    |
|--------------|--------------------|
| T: tricuspid | RA: right atrium   |
| P pulmonary  | RV right ventricle |
| M mitral     | LA left atrium     |
| A aortic     | LV left ventricle  |

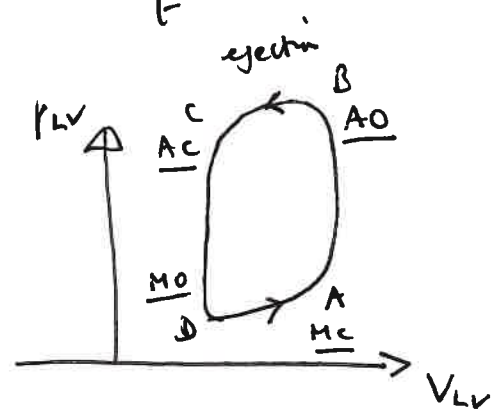
6 B



(b) Compliance : volume / pressure (looseness)  
 Elastance : Compliance<sup>-1</sup> (pressure / volume) (stiffness)  
 resistance : pressure drop / flow rate



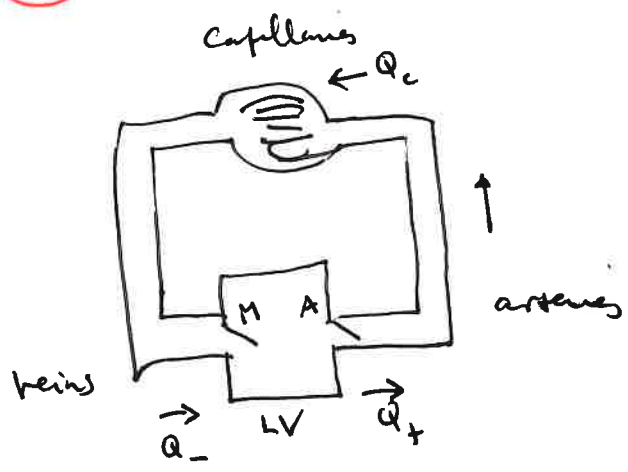
$$P_{LV} = E_{LV}(V_{LV} - V_{LV0})$$



Left ventricular values  
 A (aortic) outlet  
 M (mitral) inlet  
 AO A opens  
 AC A closes  
 MO M opens  
 MC M closes

7 B

(c)



$V_a$  aortic volume  
 $V_v$  venous volume  
 $V_{LV}$  left ventricular volume  
 $Q_+$  flow from LV  
 $Q_-$  flow to LV  
 $Q_c$  flow through capillaries

mass conservation  $\Rightarrow$

$$\dot{V}_a = Q_+ - Q_c$$

$$\dot{V}_v = Q_c - Q_-$$

$$\dot{V}_{LV} = Q_- - Q_+$$

$P_a, v, LV$  pressure in  
 aorta, veins,  
 left ventricle

$$Q_c = \frac{P_c - P_v}{R_c} \quad Q_+ = \frac{[P_{LV} - P_c]_+}{R_a} \quad Q_- = \frac{[P_v - P_{LV}]_+}{R_v}$$

resistances R  
 compliances C

$V_a = V_{a0} + C_a P_a, V_v = V_{v0} + C_v P_v$  : capillary volume is zero.

6 B

Ejection: aortic valve open  
mitral valve closed

$$\Rightarrow P_{LV} > P_a, P_v \Rightarrow Q_+ = \frac{P_{LV} - P_a}{R_a} \quad Q_- = 0$$

$$\Rightarrow C_a \dot{P}_a = \frac{P_{LV} - P_a}{R_a} - \frac{(P_a - P_v)}{R_c}$$

$$C_v \dot{P}_v = \frac{P_a - P_v}{R_c}$$

$$\frac{1}{E_s} \dot{P}_{LV} = - \frac{(P_{LV} - P_a)}{R_a}$$

$$\text{or } \begin{aligned} 0.095 \cdot R_a C_a \dot{P}_a &= P_{LV} - P_a - \frac{R_a}{R_c} (P_a - P_v) \\ 60.5 \cdot R_c C_v \dot{P}_v &= P_a - P_v \\ 0.025 \cdot \frac{R_a}{E_s} \dot{P}_{LV} &= P_a - P_{LV} \end{aligned} \quad (\text{note } E_s = \frac{1}{C_s})$$

Based on the values given above, during systole (0.3s)

$$P_a \approx P_{LV} \text{ due to } \frac{R_a}{E_s} \sim 0.025 \ll 0.35$$

$$\text{thus } P_a - P_{LV} = R_a C_s \dot{P}_{LV} \approx R_a C_s \dot{P}_a$$

$$P_v \approx \text{constant as } 60.5 \gg 0.35$$

$$P_a \text{ eqn} \Rightarrow R_a (C_a + C_s) \dot{P}_a = - \frac{R_a}{R_c} (P_a - P_v)$$

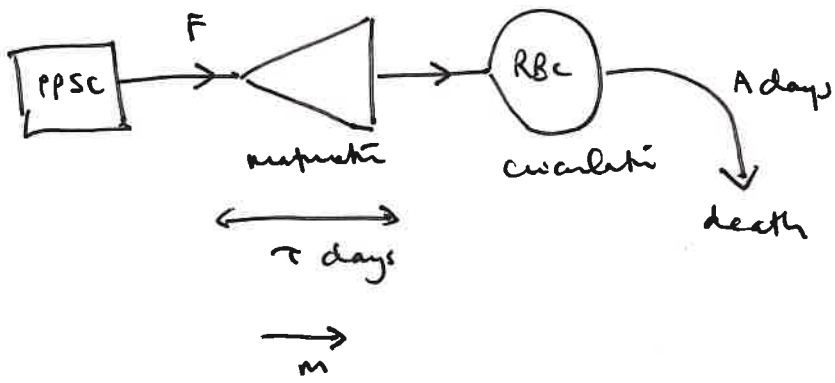
$$\Rightarrow \dot{P}_a \approx - \frac{(P_a - P_v)}{R_c (C_a + C_s)} \Rightarrow P_a - P_v \propto \exp \left[ - \frac{t}{\tau} \right],$$
  
$$\tau = R_c (C_a + C_s)$$

6 N

$$\text{Value is } R_c C_a + \frac{R_c C_a \cdot R_c C_s}{R_a C_a} = 1.8 + \frac{1.8}{0.09} \cdot 0.02 = 2.25$$

3/a) red blood cells, white blood cells (of many types)

produced by migration of pluripotential stem cells in the bone marrow + released to the blood circulation from there.



The maturing cell concentration  $c$  satisfies the characteristic equation

$$\frac{dc}{dt} = -\delta c \quad \Rightarrow \quad c_f + c_m = -\delta c \quad \delta = \text{cell death rate}$$

$$\frac{dm}{dt} = 1$$

Similarly  $\gamma$  RBC population  $r$  has age  $a$ ,

$$r_f + r_a = -\gamma r \quad \gamma = \text{RBC death rate}$$

Evidently  $r(t,0) = c(t,\tau)$ :

$$\text{Also } \frac{d}{dt} \int_0^\tau c \, da = \int_0^\tau \frac{dc}{dt} \, da = -\delta \int_0^\tau c \, da - c|_{a=\tau} + c|_{a=0}$$

death rate
loss to RBC
source from PPSC

$$\text{So } c|_{a=0} = f(t)$$

5) B/V

(f)

$$\begin{aligned} \dot{c} &= -\delta c & m &= 0 \\ \dot{m} &= 1 & t &= s > 0 \\ & & c &= F(s) \end{aligned}$$

$$\Rightarrow c = F(s) e^{-\delta(t-s)}, \quad m = t-s$$

$$\Rightarrow c = F(t-m) e^{-\delta m}$$

$$\Rightarrow c(t, \tau) = F(t-\tau) e^{-\delta \tau} \quad \forall t > \tau \quad (\text{so } s > 0)$$

$$\Rightarrow r(t, 0) = F(t-\tau) e^{-\delta \tau}$$

$$\text{so } \begin{aligned} \dot{r} &= -\gamma r & a &= 0 \\ \dot{a} &= 1 & t &= \eta > 0 \\ & & r &= F(\eta-\tau) e^{-\delta \tau} \end{aligned}$$

$$\Rightarrow a = t - \eta$$

$$r = F(\eta - \tau) e^{-\delta \tau} e^{-\gamma(t-\eta)}$$

$$\Rightarrow r = F(t-a-\tau) e^{-\delta \tau - \gamma a}$$

$$= F_{a+\tau} e^{-\delta \tau - \gamma a}$$

$$t > \tau + a \quad (\text{so } \eta > 0)$$

(5) B/v

$$(c) \quad R = \int_0^A r \, da$$

$$\text{If } t > \tau + A \text{ then } R = \int_0^A F(t-a-\tau) e^{-\delta \tau - \gamma a} \, da$$

$$\text{we have } R = \int_0^A r_t \, da = \int_0^A (-\gamma r - r_a) \, da = -\gamma R + r|_{a=0} - r|_{a=A}$$

$$= -\gamma R + F_{\tau} e^{-\delta \tau} - F_{A+\tau} e^{-\delta \tau - \gamma A}$$

from solution above

(5) V

(1)

$$F = \frac{F_0 R_0^\lambda}{R^\lambda + R_0^\lambda}$$

Scale  $t \sim \tau, R \sim R_0$  define  $h(R) = \frac{1}{1+R^\lambda}$

so non-d  $F = F_0 h(R)$

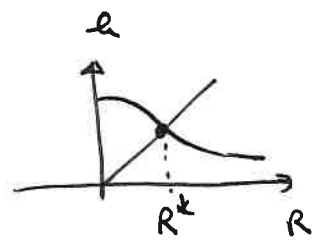
$$\Rightarrow \frac{R_0}{\tau} \dot{R} = -\gamma R_0 R + F_0 h(R_1) e^{-\delta t} - F_0 h(R_{1+\frac{\lambda}{\tau}}) e^{-\delta t - \gamma A}$$

$$\Rightarrow \dot{R} = -\gamma \tau R + \frac{\tau F_0 e^{-\delta t}}{R_0} h(R_1) - \frac{\tau F_0}{R_0} h(R_{1+\lambda}) e^{-\delta t - \gamma A}$$

or  $\dot{R} = \rho [a(R_1) - v h(R_{1+\lambda})] - \mu R$

with  $\lambda = \frac{A}{\tau}, \mu = \gamma \tau, \beta = \frac{\tau F_0 e^{-\delta t}}{R_0}, \frac{v}{\beta} = e^{-\gamma A}$

Steady state,  $\mu R = \beta(1-v)h(R)$



unique if  $v < 1$

(5) V/N

(e) If  $v \ll 1, \dot{R} \approx \beta h(R_1) - \mu R$

linearize  $R = R^* + r, \dot{r} = \beta h'(R^*) r - \mu r$

$$r = e^{\sigma t} \Rightarrow \sigma = \beta h'(R^*) e^{-\sigma} - \mu = -B - G e^{-\sigma}$$

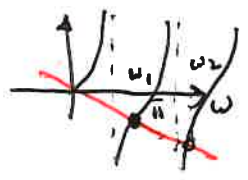
$$B = \mu, G = \beta |h'(R^*)|$$

Instability:  $G$  small:  $\text{Re } \sigma < 0$

instability at  $i\omega = -B - G e^{-i\omega}$

$$\begin{aligned} \omega &= G \sin \omega \Rightarrow \tan \omega = -\frac{\omega}{B} \\ B &= -G \cos \omega \end{aligned}$$

(5) V/N



unstable for  $G > \frac{\omega^2}{\sin \omega_2} \left( \frac{\omega_1}{\sin \omega_1} < 0 \right)$