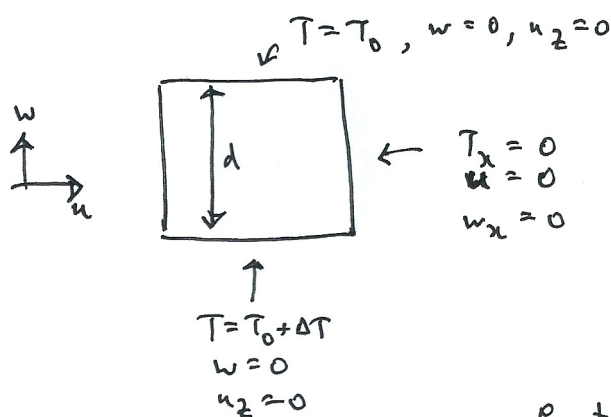


TF Lecture 5 : convection

(17)

- mantle convection
- clouds, thermals
- Earth's core

Bénard convection



stress free boundary conditions
(e.g. for mantle)

$$T_x = 0$$

$$u_x = 0$$

$$w_x = 0$$

$$\rho_f + \nabla \cdot (\rho \underline{u}) = 0$$

$$\rho [\underline{u}_t + (\underline{u} \cdot \nabla) \underline{u}] = -\nabla p - \rho \hat{k} + \mu \nabla^2 \underline{u}$$

ρ density
 c_p specific heat
 k thermal conductivity

$$\rho c_p [T_t + \underline{u} \cdot \nabla T] = k \nabla^2 T$$

$$\rho = \rho_0 [1 - \alpha (T - T_0)]$$

Non-dimensionalise

$$\underline{u} \sim \frac{\kappa}{d} \quad \left[\kappa = \frac{k}{\rho c_p} : \text{thermal diffusivity} \right] \quad t \sim \frac{d^2}{\kappa} \quad \text{thermal time scale}$$

$$T - T_0 \sim \Delta T, \quad \underline{x} \sim d, \quad p \sim p_0 \Rightarrow p = 1 - B T, \quad B = \frac{\alpha \Delta T}{\rho_0 g d} \quad (\text{non-d})$$

$$\rho = [\rho_a + \rho_0 g (d - z)] \sim \frac{\mu \kappa}{d^2}$$

We make the Boussinesq approximation in which $B \rightarrow 0$

[or: ignore variations of density except in the buoyancy term]

This leads to (ex.)

$$\nabla \cdot \underline{u} = 0$$

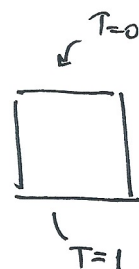
$$\frac{1}{Pr} [\underline{u}_t + (\underline{u} \cdot \nabla) \underline{u}] = -\nabla p + Ra T \underline{e}_z + \nabla^2 \underline{u}$$

$$T_t + \underline{u} \cdot \nabla T = \nabla^2 T$$

$$Pr = \frac{\mu}{\rho_0 \kappa} \quad (\text{Prandtl number}) \quad Ra = \frac{\alpha \rho_0 \Delta T d^3}{\mu \kappa}$$

Rayleigh number

(note $\alpha \propto \Delta T$ but $\neq 0$)



Conductive steady state

$$\underline{u} = 0, \quad T = 1 - z$$

Linear stability

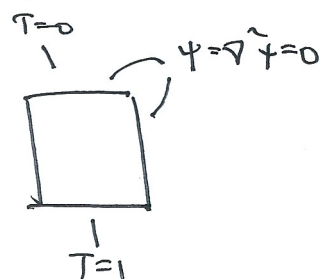
[2-D] Define a stream function via $\underline{u} = (-\psi_z, \psi_x)$

(ex.)
 $\Rightarrow$

$$\frac{1}{Pr} [\nabla^2 \psi_t + \psi_x \nabla^2 \psi_z - \psi_z \nabla^2 \psi_x] = Ra T_x + \nabla^4 \psi$$

$$T_t + \psi_x T_z - \psi_z T_x = \nabla^2 T$$

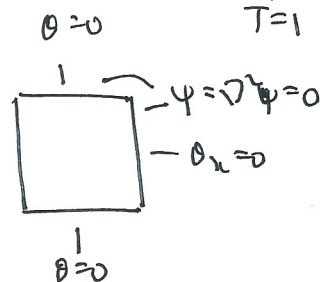
$$\boxed{\psi} \quad \psi > 0$$



Let $T = 1 - z + \theta$, linearise

$$\Rightarrow \frac{1}{Pr} \nabla^2 \psi_t = Ra \theta_x + \nabla^4 \psi$$

$$\theta_t - \psi_x = \nabla^2 \theta$$



Normal mode solutions

$$\psi = f(z) e^{\sigma t + i k x}, \quad \theta = g(z) e^{\sigma t + i k x}$$

$$\Rightarrow \partial_t \rightarrow \sigma, \quad \partial_x \rightarrow i k, \quad \nabla^2 \rightarrow \nabla^2 - k^2, \quad \nabla = \frac{d}{dz}$$

$$\Rightarrow \left. \begin{aligned} \frac{\sigma}{Pr} (\nabla^2 - k^2) f &= i k Ra g + (\nabla^2 - k^2)^2 f \\ \sigma g - i k f &= (\nabla^2 - k^2) g \end{aligned} \right\} \quad \left. \begin{aligned} f = f'' = 0 \\ g = 0 \quad \text{at } z = 0, 1 \end{aligned} \right\}$$

$$\Rightarrow \frac{\sigma}{Pr} (\nabla^2 - k^2) (\nabla^2 - k^2 - \sigma) f = k^2 Ra f + (\nabla^2 - k^2)^2 (\nabla^2 - k^2 - \sigma) f$$

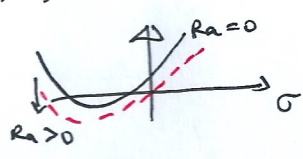
no shear
[f' = 0 at no slip]

The solutions are exponentially: for the particular case of stress free boundary conditions, we see by inspection that

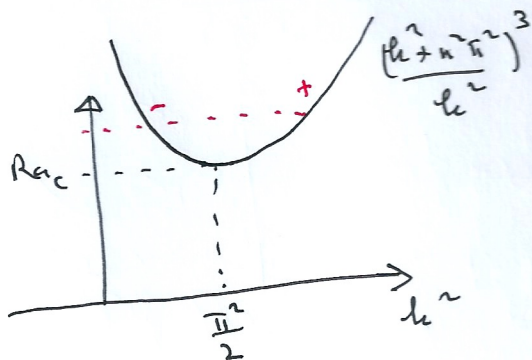
solutions are $f = \sin n\pi z$

and thus

$$\frac{\sigma}{Pr} K^2 (K^2 + \sigma) = k^2 Ra - K^4 (K^2 + \sigma), \quad K^2 = n^2 \pi^2 + k^2$$

$$\Rightarrow (\sigma + K^2) \left(\frac{\sigma K^2}{Pr} + K^4 \right) = k^2 Ra$$


σ is real and $\sigma > 0$ for $Ra > \frac{K^6}{k^2} = \frac{(k^2 + n^2 \pi^2)^3}{k^2}$



The minimum value is when

$$k = \frac{\pi}{\sqrt{2}} \quad \text{and} \quad Ra_c = \frac{27\pi^4}{4} \approx 657.5$$

For $Ra > Ra_c$, convection occurs for a range $k_- < k < k_+$.

Note: for no-slip on bottom, no stress on top, $Ra_c \approx 1101$
no-slip on both $Ra_c = 1708$

— requires numerical calculation (see Drazin and Reid
Hydrodynamic Stability CUP)

□

TF Lecture 6 : boundary layer theory

(20)

$Ra \gg 1$, $Pr = \infty$, steady, Boussinesq

$$\nabla \cdot \underline{u} \approx 0$$

$$0 = -\nabla p + \nabla^2 \underline{u} + Ra T \underline{e}_z$$

$$\underline{u} \cdot \nabla T = \nabla^2 T$$



For symmetry, take

$T = -\frac{1}{2}$ on top (slight change of non-d)
 $T = \frac{1}{2}$ on bottom

$Ra \gg 1 \Rightarrow \underline{u} \gg 1 \rightarrow$ boundary layers $\rightarrow$ plumes $\rightarrow$ vorticity $\rightarrow$ core flow

2-D, stream function

$\underline{u} = (-\psi_z, 0, \psi_x) \rightarrow \underline{\omega} = \text{curl } \underline{u} = (0, \omega, 0)$

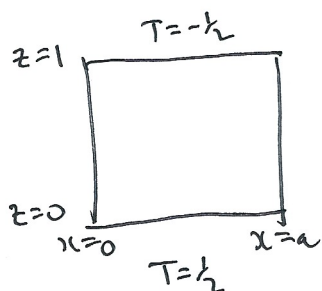
$$\Rightarrow \omega = -\nabla^2 \psi$$

$$\psi_x T_z - \psi_z T_x = \nabla^2 T$$

$$0 = -Ra T_x + \nabla^2 \omega$$

Rescale

$\psi \sim \omega \sim \frac{1}{\delta} z$, $\delta = \frac{1}{Ra^{1/3}}$ (for no stress h.c.s)



$$\Rightarrow \begin{aligned} \omega &= -\nabla^2 \psi \\ \psi_x T_z - \psi_z T_x &= \delta^2 \nabla^2 T \\ \nabla^2 \omega &= \frac{1}{\delta} T_x \end{aligned}$$

← !

$$\omega = -\nabla^2 \psi$$

$$\psi_x T_z - \psi_z T_x = \delta^2 \nabla^2 T$$

$$\nabla^2 \omega = \frac{1}{\delta} T_x$$

Core flow

$$\delta \downarrow 0 \quad T = 0 \quad \text{to all orders}$$

$$[T \approx T(\psi),$$

$$\nabla \cdot T \underline{u} = \delta^2 \nabla^2 T$$



$$\int_C T u_n ds = \delta^2 \int_C \frac{\partial T}{\partial n} ds$$

$$\approx \delta^2 T'(\psi) \int \frac{\partial \psi}{\partial n} ds$$

[Prandtl-Batchelor theorem]

$$\psi = 0$$

$$\omega = \omega_p$$

on sides

$$\left\{ \begin{array}{l} \nabla^2 \omega = 0 \quad (!) \\ \nabla^2 \psi = 0 \end{array} \right.$$

divided by sidewall stress



Plumes

e.g. at $x=0$:

$$\psi = \delta \bar{\Psi}, \quad x = \delta X$$

$$\Rightarrow \bar{\Psi}_{xx} \approx 0 \Rightarrow \bar{\Psi} \approx w_p(z) X$$

(w_p is core velocity up at boundary)

$$\omega_{xx} \approx T_x \quad (\rightarrow \omega_x = T)$$

$$\Rightarrow \omega \approx \int_0^X T dX$$

$$\text{And } \bar{\Psi}_x T_z - \bar{\Psi}_z T_x \approx T_{xx} \Rightarrow \int_0^\infty T d\bar{\Psi} \left[= \int_0^\infty T w_p(z) dX \right] = C$$

constant (ex.)

- using $T_x = 0$ at $X=0$ also

so core value

$$\omega_p = \int_0^\infty T dX = -\psi_{xx}|_{x \rightarrow 0+} \quad [\text{core}]$$

$$\& \omega_p w_p = \int_0^\infty T d\bar{\Psi} = C$$

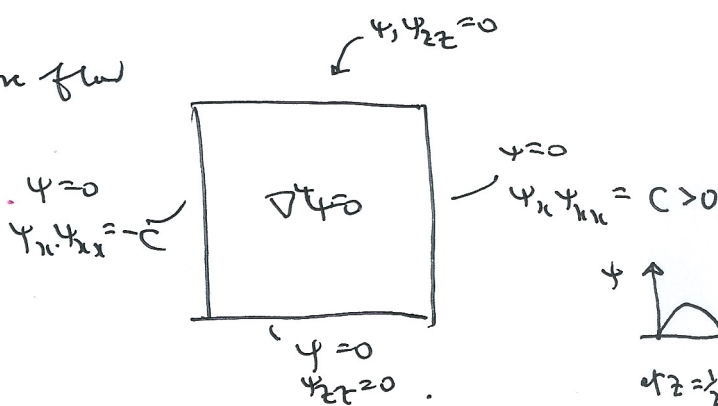
$$\Rightarrow \text{b.c. for core flow is } \psi_{xx} \psi_{xx} = -C$$

$$x=0$$

$$x=a$$

(by symmetry)

so core flow



$$\Rightarrow \psi = \sqrt{C} \hat{\psi}$$

parameter independent

$\hat{\psi}$ is canonical solution

What is C ? - upper and lower thermal boundary layers

e.g. at $z=1$ (top)

$$\omega = \delta \Omega, \quad \psi = \delta \Psi, \quad z = 1 - \delta z$$

$$\Rightarrow \Psi_{zz} \approx 0 \Rightarrow \Psi = u_s(x)z \quad (u_s > 0)$$

$$[\Omega_{zz} = T_x]$$

$$\Psi_z T_x - \Psi_x T_z = T_{zz}$$

Variables (ex.) $x, z \rightarrow x, \Psi \Rightarrow \partial_x \rightarrow \partial_x + \Psi_x \partial_\Psi, \quad \partial_z \rightarrow \Psi_z \partial_\Psi$

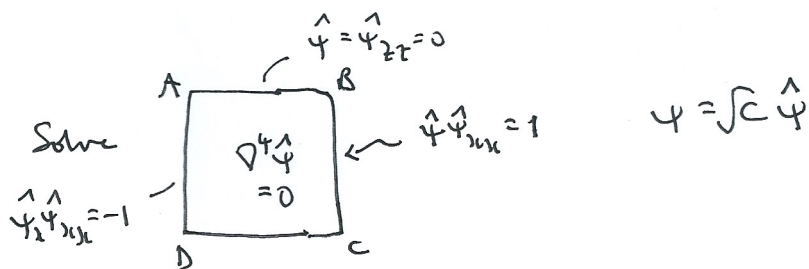
$$\Rightarrow T_x = \frac{\partial}{\partial \Psi} \left[u_s \frac{\partial T}{\partial \Psi} \right] \quad \text{with } u_s = u_s(x)$$

$$[\text{Similar transformation in } \Psi \Rightarrow T_z = \frac{\partial}{\partial \Psi} \left[\omega \frac{\partial T}{\partial \Psi} \right]]$$

with boundary conditions $T = -\frac{1}{2}$ at $z=0, \quad T \rightarrow 0$ at $z \rightarrow \infty$

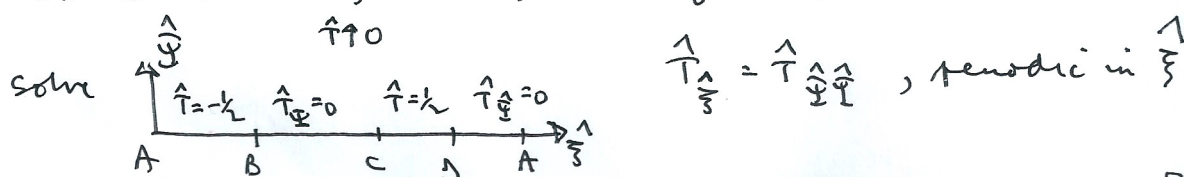
Note: canonical $u_s = C^{1/2} \hat{u}_s$, define $\Psi = C^{1/4} \hat{\Psi}, \quad \xi = \int_0^x \hat{u}_s dx$

Summary



define peripheral velocity $(= \frac{\partial \Psi}{\partial n} \big|_{n=0}, \text{ inward normal}) \quad U(s) \quad s = \text{arc length}$

so $U = \sqrt{C} \hat{U}(s)$, then put $\xi = \int_0^s \hat{U}(s) ds, \quad \Psi = C^{1/4} \hat{\Psi}, \quad T(\xi, \Psi) = \hat{T}(\frac{\xi}{C^{1/4}}, \hat{\Psi})$



$$C \text{ is determined via } C = \int_0^\infty T \big|_A d\Psi = \int_0^\infty \hat{T} \big|_A d\hat{\Psi} C^{1/4} \Rightarrow C = \left[\int_0^\infty \hat{T} \big|_A d\hat{\Psi} \right]^{4/3}$$

$\hat{T}$ and $\hat{\Psi}$ need to be computed numerically.

Topic Lecture 7 Double diffusive convection

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This occurs when two quantities affect buoyancy, e.g. heat and salt

(e.g. in the oceans).

If c is concentration (of salt), then we take

$$\rho = \rho_0 [1 - \alpha(T - T_0) + \beta(c - c_0)] \quad \alpha, \beta > 0$$

$$\begin{cases} c_t + \underline{u} \cdot \underline{\nabla} c = D \nabla^2 c \end{cases} \quad D \text{ is diffusion coefficient}$$

The scaled equations (with $c - c_0 \sim \Delta c$) are (Boussinesq assumption) [ex.]

$$\underline{\nabla} \cdot \underline{u} = 0$$

$$\frac{1}{Pr} \left[\underline{u}_t + (\underline{u} \cdot \underline{\nabla}) \underline{u} \right] = -\underline{\nabla} p + Ra Th - Rs c_k + \nabla^2 \underline{u}$$

$$T_t + \underline{u} \cdot \underline{\nabla} T = \nabla^2 T$$

$$c_t + \underline{u} \cdot \underline{\nabla} c = \frac{1}{Le} \nabla^2 c$$

$$\text{Solental Rayleigh number } Rs = \frac{\beta \rho_0 \Delta c g d^3}{\mu \kappa} \quad \text{Lewis number } Le = \frac{\kappa}{D}$$

Note: $Rs > 0$ is stabilising; typically $Le \gg 1$ (for heat + salt)

Linear stability

We prescribe boundary conditions $c = T = 1$ at $z = 0$;
 $c = T = 0$ at $z = 1$

$\rightarrow$ steady state $c = 1 - z, T = 1 - z, \underline{u} = \underline{0}$

Linearise (2-D)

First, $\underline{u} = (-\psi_z, 0, \psi_x)$

ex. $\Rightarrow \frac{1}{Pr} [\nabla^2 \psi_t + \psi_x \nabla^2 \psi_z - \psi_z \nabla^2 \psi_x] = Ra T_x - Rs c_x + \nabla^4 \psi$

$$T_t + \psi_x T_z - \psi_z T_x = \nabla^2 T$$

$$c_t + \psi_x c_z - \psi_z c_x = \frac{1}{Le} \nabla^2 c$$

$$c = 1 - z + C$$

$$T = 1 - z + \theta$$

$$C, \theta, \psi \ll 1$$

$$\Rightarrow \frac{1}{Pr} \nabla^2 \psi_t \approx Ra \theta_x - Rs c_x + \nabla^4 \psi$$

$$\theta_t - \psi_x = \nabla^2 \theta$$

$$c_t - \psi_x = \frac{1}{Le} \nabla^2 c$$

$$C = \psi = \theta = 0 \text{ at } z = 0, 1, \text{ no stress } \psi_{zz} = 0 \text{ at } z = 0, 1$$

$\Rightarrow$ Solutions are $\psi = e^{ikx + \sigma t} \sin m\pi z$ $\leftarrow$ for b.c.s

$$\theta = B e^{ikx + \sigma t} \sin m\pi z$$

$$C = H e^{ikx + \sigma t} \sin m\pi z$$

$$\partial_t \rightarrow \sigma, \partial_x \rightarrow ik, \nabla^2 \rightarrow -K^2, K^2 = k^2 + m^2 \pi^2$$

$$\Rightarrow -\frac{\sigma K^2}{Pr} = ik Ra B - ik Rs H + K^4$$

$$(\sigma + K^2) B = ik, \left(\sigma + \frac{K^2}{Le}\right) H = ik$$

$$\Rightarrow -\frac{\sigma K^2}{Pr} = \frac{-k^2 Ra}{\sigma + K^2} + \frac{k^2 Rs}{\sigma + \frac{K^2}{Le}} + K^4$$

or (ex.) $(\sigma + K^2 Pr)(\sigma + K^2)\left(\sigma + \frac{K^2}{Le}\right) = k^2 Pr \left[\frac{\sigma(Ra - Rs)}{K^2} + \left(\frac{Ra}{Le} - Rs\right) \right]$

- a cubic

coefficients
are v.l.o.g.

This can be written as (ex.)

$$\sigma^3 + a\sigma^2 + b\sigma + c = 0$$

$$a = K^2 \left(P_r + 1 + \frac{1}{L_e} \right) > 0$$

$$b = K^4 \left(P_r + \frac{1}{L_e} + \frac{P_r}{L_e} \right) + \frac{L_e^2}{K^2} P_r (R_s - R_a)$$

$$c = \frac{K^6}{L_e} P_r + \frac{L_e^2}{K^2} P_r \left(R_s - \frac{R_a}{L_e} \right)$$

For $R_s > 0, R_a < 0$ (both stabilizing) as $R_s \rightarrow \infty, R_a \rightarrow -\infty, b, c \rightarrow \infty$

So approximately $\sigma^3 + b\sigma + c = -a\sigma^2 \Rightarrow \sigma \approx -\frac{b}{c} < 0$

$$\text{or } \sigma^2 + b = -\frac{(c + a\sigma^3)}{\sigma} \Rightarrow \sigma \approx \pm i\sqrt{b}$$

$$\text{so e.s. to eigen } \sigma - i\sqrt{b} = -\frac{(c + a\sigma^2)}{\sigma(\sigma + i\sqrt{b})}$$

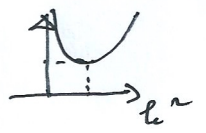
$$\Rightarrow \sigma \approx i\sqrt{b} - \frac{(c - ab)}{i\sqrt{b} \cdot 2i\sqrt{b}} = \frac{-(ab - c)}{2b} + i\sqrt{b}$$

so $\text{Re } \sigma < 0$ if $ab > c$... (ex) which is always true if $L_e > 1$

Now vary R_a, R_s : system loses stability if

$$\sigma = 0 \text{ (direct instability)} \Rightarrow c = 0 \Rightarrow R_a - L_e R_s = \frac{K^6}{L_e^2}$$

$$\Rightarrow \text{direct instability if } R_a - L_e R_s > R_c = \frac{27\pi^4}{4} \left(\min \frac{K^6}{L_e^2} \right)$$



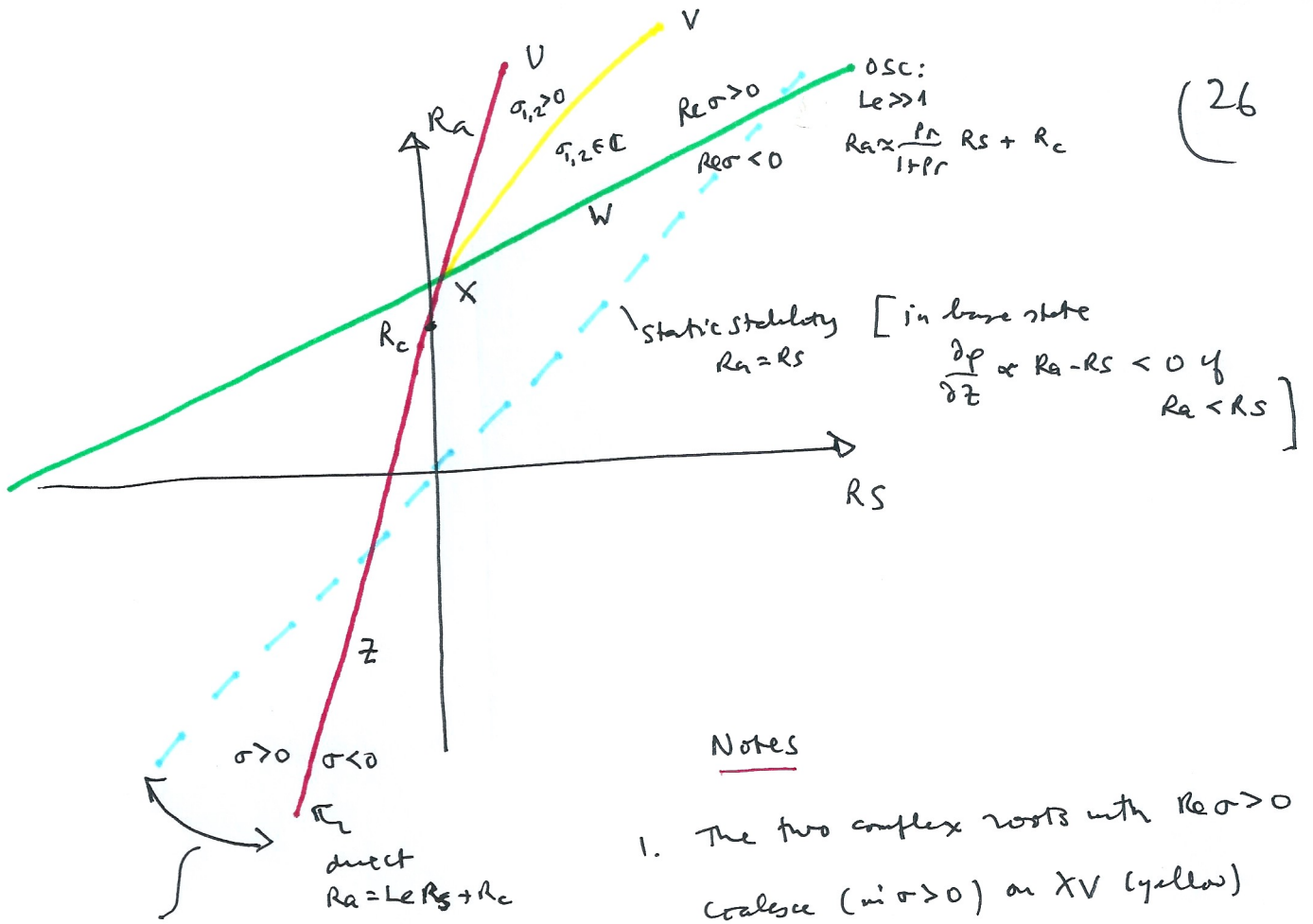
or oscillatory instability (Hopf) if

$$\sigma = \pm i\Omega \Rightarrow \sigma^3 + a\sigma^2 + b\sigma + c = (\sigma^2 + \Omega^2)(\sigma + \gamma) \quad (\gamma > 0)$$

$$= \sigma^3 + \gamma\sigma^2 + \Omega^2\sigma + \gamma\Omega^2$$

$$\Rightarrow \gamma = a > 0 \text{ and } \underline{cb = c}$$

$$\Rightarrow \text{oscillatory unstable if (ex.) } R_a > \frac{(P_r + \frac{1}{L_e}) R_s}{1 + P_r} + \frac{(1 + \frac{1}{L_e})(P_r + \frac{1}{L_e})}{P_r} R_c$$

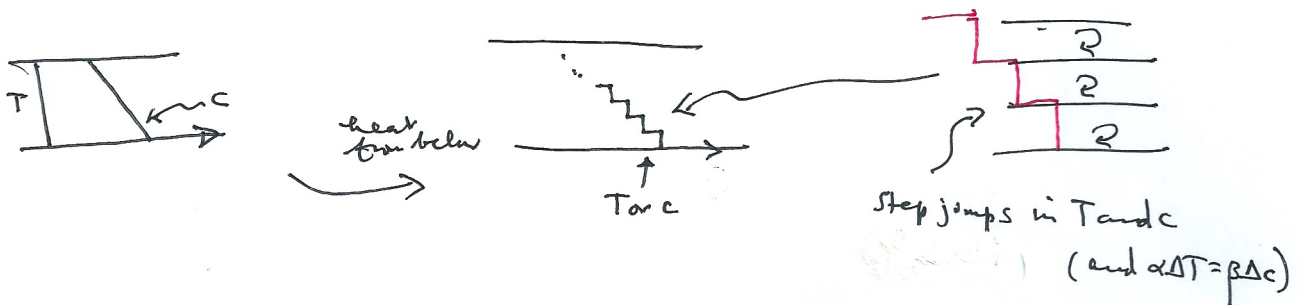


Notes

1. The two complex roots with $Re \sigma > 0$ coalesce (in $\sigma > 0$) at XV (yellow)
2. Oscillatory instability is not seen in practice
3. Salt fingers ($Le \gg 1$) occur at bottom left (hot salty above cold fresh) have been seen in the ocean
4. Application of prescribed concentrations does not happen in practice

fingers -
 high wave number
 - hot salty over cold fresh
 - oceans

5. Double diffusive convection promotes layered convection:
 heat a stable salt gradient $\Rightarrow$ transient layered convection cells

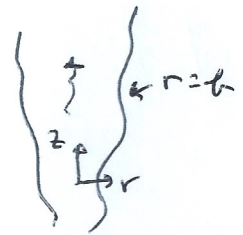
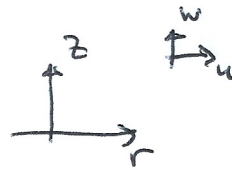


topics in fluids lecture 8: plumesPlumes

e.g. black smokers

chimneys

volcanoes

Assume cylindrical, turbulent

$$\text{mass} \quad (ru)_r + (rw)_z = 0$$

Assumes

Boussinesq approximation

$$\text{momentum} \quad uw_r + ww_z = -\frac{1}{\rho_0} p_r \left[+ \frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial u}{\partial r} \right\} \dots \right]$$

$$uw_r + ww_z = -\frac{1}{\rho_0} p_z - \frac{\rho g}{\rho_0} \left[+ \frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial w}{\partial r} \right\} \right]$$

$$\text{buoyancy} \quad u p_r + w p_z = \left[\frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial p}{\partial r} \right\} \right]$$

↑
via $p(T, c)$ etc.

↑
turbulent mixing

$\nu_T = \text{eddy diffusivity}$
 $\approx \epsilon_T w b$ for example
 $\epsilon_T \sim 10^{-2}$

Assume a background (ambient)
density $\rho_0(z)$

we suppose $p = p_0 - \Delta p$, $\Delta p \ll p_0$ ($\Rightarrow$ Boussinesq) $\Delta p > 0 \Rightarrow$ buoyant

Assume plume is thin $\rightarrow \frac{\partial p}{\partial r} \approx 0 \Rightarrow \frac{\partial p}{\partial z} \approx -\rho_0 g$ (as for ambient fluid)

$$\Rightarrow uw_r + ww_z = g' \equiv \frac{g \Delta p}{\rho_0} \quad \text{reduced gravity} \quad [+ \text{mixing}]$$

$$\text{And (ex.)} \quad N^2 \left(1 - \frac{\Delta p}{\rho_0}\right) w + u g'_r + w g'_z = \left[\frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial g'}{\partial r} \right\} \right]$$

 ≈ 1

Brunt-Väisälä frequency

$$N = \left(-\frac{g \rho'_0}{\rho_0} \right)^{1/2}$$

Full model is thus (with $\Delta p \ll p_0$)

$$(ru)_r + rw_z = 0$$

$$uw_r + ww_z = g' + \frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial w}{\partial r} \right\}$$

$$N^2 w + ug'_r + wg'_z = \frac{1}{r} \frac{\partial}{\partial r} \left\{ \nu_T r \frac{\partial g'}{\partial r} \right\}$$

Comments

1. The mixing terms are commonly ignored: this is ill-advised.
2. Entrainment at the flame edge occurs: $u = -u_e = 2\bar{w}$ at $r=b$

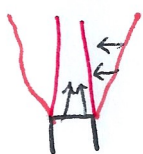
$$\bar{w} = \text{mean velocity} = \frac{1}{\pi b^2} \int_0^b 2\pi r w dr$$

3. Can define a stream function

$$ru = -\psi_z, \quad rw = \psi_r, \quad \psi = 0 \text{ at } r=0 \quad (\text{so } \psi > 0, r > 0)$$

4. Neglect mixing ($\nu_T = 0$)

$$\Rightarrow \text{hyperbolic system, } \dot{r} = u, \dot{z} = w, \dot{w} = g', \dot{g}' = -N^2 w$$



$\rightarrow$ characteristics:

$\Rightarrow$ mixing is necessary for a buoyant plume ($g' > 0$)
(and actually for a non-buoyant one too)

5. $N \neq 0$ provides a natural length scale

$$\left[N^2 w \sim wg'_z \Rightarrow z \sim \frac{g'}{N^2} \sim \frac{g \Delta p}{p_0 - g p_0'} \frac{p_0}{p_0'} = -\frac{\Delta p}{p_0'} \right]$$

If $N = 0$ (unstratified ^{ambient} fluid)

no natural length scale $\Rightarrow$ similarity solution

Unstratified ambient fluid - similarity solution

with $N=0$ define $\eta = \frac{r}{z}$ and the solution has the form $b = \beta z$, $w = B^{1/3} z^{-1/3} W(\eta)$,

$$g' = B^{2/3} z^{-5/3} G(\eta),$$

where W & G are like Gaussians. Here B is the buoyancy flux

$$B = 2\pi \int_0^b r w g' dr \quad (\text{which is conserved, and preserved})$$

Stratified fluid - an approximate solution

we construct moments as ~~for~~ follows:

$$Q = 2\pi \int_0^b r w dr \quad \text{volume flux}$$

$$M = 2\pi \int_0^b r w^2 dr \quad \text{momentum flux}$$

$$B = 2\pi \int_0^b r w g' dr \quad \text{buoyancy flux.}$$

Include mixing terms but they integrate to zero!take $w=0$
 $g'=0$ at $r=b$ (ex.)
 $\Rightarrow$

$$\frac{dQ}{dz} = 2\pi \alpha b \bar{w}$$

$$\frac{dM}{dz} = 2\pi \int_0^b r g' dr$$

$$\frac{dB}{dz} = -N^2 Q$$

$$\bar{w} = \frac{2}{b^2} \int_0^b r w dr = \frac{Q}{\pi b^2}$$

$$\begin{aligned} \text{or } Q &= \pi b^2 \bar{w} \\ M &= \pi b^2 \bar{w}^2 \\ B &= \pi b^2 \bar{w} g' \end{aligned}$$

Close

Assume top hat profiles



(30)

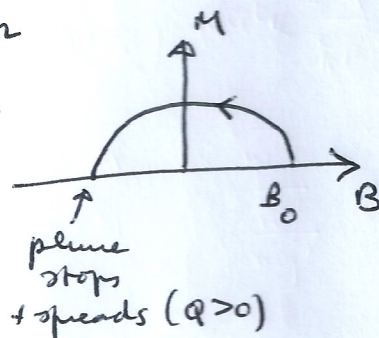
$$\text{so } \overline{w^2} = w^2, \quad \bar{w} = w, \quad \overline{wg'} = wg', \quad 2\bar{n} \int_0^b r g' dr = \bar{n} b^2 g'$$

$$\Rightarrow \begin{cases} B' = -N^2 Q \\ M' = \frac{BQ}{M} \\ Q' = 2\alpha \sqrt{\bar{n} M} \end{cases}$$

[Note: $N=0 \Rightarrow B$ constant
& similarity solution]

Assume N constant $B=B_0, M=Q=0$ at $z=0$

$$\Rightarrow \text{1st integral (B & M)} \quad \underline{B^2 + N^2 M^2 = B_0^2}$$



Define $\underline{B = B_0 \cos \theta}, \quad \underline{M = \frac{B_0}{N} \sin \theta}$

$\Rightarrow$ plume rises till $\theta = \pi$

(M eq) $\Rightarrow \theta' = \frac{N^2 Q}{B_0 \sin \theta} \quad \overset{(Q \text{ eq})}{Q' = 2\alpha \sqrt{\frac{\bar{n} B_0}{N}} \sin^{1/2} \theta}$



$$\Rightarrow \left[\frac{dQ}{d\theta} = \dots \right] \Rightarrow Q = \frac{2\alpha^{1/2} \pi^{1/4} B_0^{3/4}}{N^{5/4}} \left[\int_0^\theta \sin^{3/2} \phi d\phi \right]^{1/2} = Q(\theta)$$

$$\Rightarrow \theta' = \frac{N^2 Q(\theta)}{B_0 \sin \theta}, \quad \underline{z = \frac{B_0}{N^2} \int_0^\theta \frac{\sin \theta d\theta}{Q(\theta)}}$$

The rise height is $z_s = \frac{B_0}{N^2} \int_0^\pi \frac{\sin \theta d\theta}{Q(\theta)} \propto \frac{B_0^{1/4}}{N^{3/4}}$

- fits volcanic data!