

c5-7 PS4 q1 answer.

(1

$$(\alpha p_s)_t + (\alpha p_s v)_z = \Gamma$$

$$[p_\ell(1-\alpha)]_t + [p_\ell(1-\alpha)u]_z = -\Gamma$$

$$p_s(v_t + uv_z) = -p_z - M$$

$$p_\ell(u_t + D_\ell u_z) = -p_z + M$$

If written in the form $A \underline{\psi}_t + B \underline{\psi}_z = \underline{c}$

For if $\underline{\psi}$ was scalar, the characteristics would be $\dot{z} = \frac{B}{A} = A^{-1}B$

& this generalises to systems:

Suppose $A^{-1}B \underline{w} = \lambda \underline{w}$

[actually here A is singular so we'd use $B^{-1}A \underline{\xi} = \mu \underline{\xi}$, $\mu = \frac{1}{\lambda}$]

& if $A^{-1}B$ is diagonalisable

$$A^{-1}B = P D P^{-1} \quad P = \text{diag}(\lambda_i)$$

Put $\underline{\psi} = P \underline{u}$

$$\Rightarrow A [P \underline{u}_t + P \underline{u}_z] + B [P \underline{u}_z + P \underline{u}_t] = \underline{c}$$

$$\times P^{-1}A^{-1} \Rightarrow \underline{u}_t + P^{-1}A^{-1}B P \underline{u}_z = P^{-1}A^{-1}[\underline{c} - \{AP_t + BP_z\}\underline{u}]$$

$$\Rightarrow \underline{u}_t + D \underline{u}_z = P^{-1}A^{-1}[\underline{c} - (AP_t + BP_z)\underline{u}]$$

$\Rightarrow$ characteristics are $\dot{z} = \lambda_i$

on which $\dot{u}_i = [P^{-1}A^{-1}\{\underline{c} - (AP_t + BP_z)\underline{u}\}]_i$

More generally, solve $\det(\lambda A - B) = 0$. Note RHS $\uparrow$ may contain derivatives of u_j also...

(i) p_s, p_e constant, $\frac{p_s}{p_e} = \delta \ll 1$

$$\text{Thus } \begin{aligned} \alpha_t + v\alpha_z + \alpha v_z &= \frac{r}{p_s} \\ -\alpha_t &= -u\alpha_z + (1-\alpha)v_z = -\frac{r}{p_e} \end{aligned}$$

$$p_s v_t + p_s v v_z + p_z = -M$$

$$p_e v_t + D_e p_e u v_z + p_z = M$$

Let write $\underline{y} = \begin{pmatrix} \alpha \\ u \\ v \\ p \end{pmatrix}$

$$\underbrace{\begin{pmatrix} 1 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 \\ 0 & 0 & p_s & 0 \\ 0 & p_e & 0 & 0 \end{pmatrix}}_A \underline{y}_t + \underbrace{\begin{pmatrix} v & 0 & \alpha & 0 \\ -u & (1-\alpha) & 0 & 0 \\ 0 & 0 & p_s v & 1 \\ 0 & D_e p_e u & 0 & 1 \end{pmatrix}}_B \underline{y}_z = \begin{pmatrix} r/p_s \\ -r/p_e \\ -M \\ M \end{pmatrix}$$

$\det(\lambda A - B)$

$$= \begin{vmatrix} \lambda - v & 0 & -\alpha & 0 \\ -(\lambda - u) & -(1-\alpha) & 0 & 0 \\ 0 & 0 & p_s(\lambda - v) & -1 \\ 0 & p_e(\lambda - D_e u) & 0 & -1 \end{vmatrix} = 0$$

This gives

$$(\lambda - v) \left[-(1-\alpha) p_g (\lambda - v)^{-1} \right] - \alpha \left[-(\lambda - u) p_\ell (\lambda - D_\ell u) \right] = 0$$

$$u \approx p_g (1-\alpha) (\lambda - v)^2 + p_\ell \alpha (\lambda - u) (\lambda - D_\ell u) = 0$$

with $\delta = \frac{p_g}{p_\ell} \ll 1$

$$\delta (1-\alpha) (\lambda - v)^2 + \alpha (\lambda - u) (\lambda - D_\ell u) = 0$$

$$(\lambda - u) (\lambda - D_\ell u) \approx - \frac{\delta (1-\alpha)}{\alpha} (\lambda - v)^2$$

Approximately $\lambda = u$ & $\lambda = D_\ell u$ are the (real) roots

↳ *corrects u to λ

$$\lambda - u = \frac{-\delta (1-\alpha) (\lambda - v)^2}{\alpha (\lambda - D_\ell u)}$$

$$\Rightarrow \lambda \approx u + \frac{\delta (1-\alpha) (u - v)^2}{\alpha (D_\ell - 1) u} \quad \text{etc.}$$

This only goes wrong if $D_\ell \sim \delta$.

(ii) Now suppose $\frac{dp_s}{dp} = \frac{1}{c_s^2}$, $\frac{dp_\ell}{dp} = \frac{1}{c_\ell^2}$

(c^s are sound speeds)

then equations are

$$\begin{aligned} p_g \alpha_t + \frac{\alpha}{c_g^2} p_t + p_g v \alpha_z + \gamma_g \alpha v_z + \frac{\alpha v}{c_g^2} p_z &= \Gamma \\ -p_\ell \alpha_t + \frac{(1-\alpha)}{c_\ell^2} p_t - \gamma_\ell u \alpha_z + p_\ell (1-\alpha) u_z + \frac{(1-\alpha)u}{c_\ell^2} p_z &= -\Gamma \end{aligned}$$

~ (define $\Pi_h = p_h c_h^2$)

$$\begin{aligned} \alpha_t + \frac{\alpha}{\Pi_g} p_t + v \alpha_z + \alpha v_z + \frac{\alpha v}{\Pi_g} p_z &= \frac{\Gamma}{p_g} \\ -\alpha_t + \frac{1-\alpha}{\Pi_\ell} p_t - u \alpha_z + (1-\alpha) u_z + \frac{(1-\alpha)u}{\Pi_\ell} p_z &= -\frac{\Gamma}{p_\ell} \end{aligned}$$

And $p_g v_t + p_g v v_z + p_z = -M$

$p_\ell u_t + p_\ell D_\ell u u_z + p_z = M$

The red terms are the additions, thus

$$A = \begin{pmatrix} 1 & 0 & 0 & \frac{\alpha}{\Pi_g} \\ -1 & 0 & 0 & \frac{(1-\alpha)u}{\Pi_\ell} \\ 0 & 0 & \gamma_g & 0 \\ 0 & p_\ell & 0 & 0 \end{pmatrix}, \quad B = \begin{pmatrix} v & 0 & \alpha & \frac{\alpha v}{\Pi_g} \\ -u & (1-\alpha) & 0 & \frac{(1-\alpha)u}{\Pi_\ell} \\ 0 & 0 & p_g v & 1 \\ 0 & D_\ell p_\ell u & 0 & 1 \end{pmatrix}$$

and thus

$$\det(\lambda A - B)$$

$$= \begin{vmatrix} \lambda - v & 0 & -\alpha & \frac{\alpha}{n_g}(\lambda - v) \\ -(\lambda - u) & -(1 - \alpha) & 0 & \frac{(1 - \alpha)}{n_e}(\lambda - u) \\ 0 & 0 & p_g(\lambda - v) & -1 \\ 0 & p_e(\lambda - \phi_e u) & 0 & -1 \end{vmatrix} = 0$$

$$\begin{aligned} \Rightarrow (\lambda - v) & \left[(1 - \alpha) p_g (\lambda - v) - \frac{(1 - \alpha)}{n_e} (\lambda - u) p_g p_e (\lambda - v) (\lambda - \phi_e u) \right] \\ & - \alpha \left[-(\lambda - u) p_e (\lambda - \phi_e u) \right] \\ & - \frac{\alpha}{n_g} (\lambda - v) \left[-(\lambda - u) \cdot -p_g p_e (\lambda - v) (\lambda - \phi_e u) \right] = 0 \end{aligned}$$

$$\text{i.e. } p_g (1 - \alpha) (\lambda - v)^2 + p_e \alpha (\lambda - u) (\lambda - \phi_e u)$$

$$- p_g p_e \left[\frac{1 - \alpha}{n_e} + \frac{\alpha}{n_g} \right] (\lambda - v)^2 (\lambda - u) (\lambda - \phi_e u) = 0$$

Previously, we had $\lambda \sim u$

Let's suppose $v \sim u$ and $c_g \sim c_d$

If $\lambda \sim u$ the new term is $\sim \left[\frac{p_3}{c_d^2}, \frac{p_1}{c_g^2} \right] u^4 \ll p_d u^2$

So two approximate roots are $\lambda = u, \partial_d u$ as before.

As the new term is negligible, the other two roots are large

$$\text{Approximately } p_d \propto (\lambda - u)(\lambda - \partial_d u) - \frac{\alpha p_d}{c_g^2} (\lambda - v)^2 (\lambda - u)(\lambda - \partial_d u) \approx 0$$

So the other two roots are

$$\underline{\lambda = v \pm c_g} \quad \text{for sound waves}$$

2, (a)



$$x_g = 1 \quad \text{if } \underline{x} \in G \quad (\text{gas phase})$$

$$0 \quad \text{if } \underline{x} \in L \quad (\text{liquid phase})$$

gas mass is $\frac{\partial \rho_g}{\partial t} + \nabla \cdot (\rho_g \underline{v}) = 0$

Let x_g & integrate over a cylindrical volume V

$$\Rightarrow \int_V \left[x_g \frac{\partial \rho_g}{\partial t} + x_g \nabla \cdot (\rho_g \underline{v}) \right] dV = 0$$

$$\Rightarrow \int_V \left[\frac{\partial}{\partial t} (x_g \rho_g) + \nabla \cdot \{ x_g \rho_g \underline{v} \} \right] dV$$

$$= \int_V \rho_g \left\{ \frac{\partial x_g}{\partial t} + \underline{v} \cdot \nabla x_g \right\} dV$$

Now x_g is a generalized function & defined via an arbitrary test function ϕ

$$\int \phi \left[\frac{\partial x_g}{\partial t} + \underline{v} \cdot \nabla x_g \right] dV dt$$

$$= - \int x_g \left[\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \underline{v}) \right] dV dt$$

$$= - \int_{-\infty}^{\infty} dt \int_G \left[\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \underline{v}) \right] dV dt$$

$$= - \int_{-\infty}^{\infty} dt \frac{1}{dt} \int_G \phi dV \quad \text{via Reynolds' transport theorem (as } G \text{ is material)}$$

$$= - \left[\int_G \phi dV \right]_{-\infty}^{\infty} = 0 \quad (\phi \rightarrow 0 \text{ at } \infty)$$

$$\text{So } \frac{\partial}{\partial t} \int_A x_g \rho_g dA \delta z + \left[\int_A x_g \rho_g \underline{v} \cdot \underline{k} \right]_z^{z+\delta z} = 0$$

where we take $V = A \delta z$ & since $\underline{v} \cdot \underline{n} = 0$ on walls [the unit vector upwards]

Thus

$$\frac{\partial}{\partial t} \int_A x_g \rho_g dA + \frac{\partial}{\partial z} \int_A x_g \rho_g v dA = 0$$

where $v = \underline{v} \cdot \underline{k}$ is vertical velocity

Define $\alpha = \frac{1}{A} \int_A x_g dA$

$$\alpha \bar{\rho}_g = \frac{1}{A} \int_A x_g \rho_g dA$$

$$\alpha \bar{\rho}_g \bar{v} = \frac{1}{A} \int_A x_g \rho_g v dA$$

$$\Rightarrow (\alpha \bar{\rho}_g)_t + (\alpha \bar{\rho}_g \bar{v})_z = 0$$

Similarly for liquid $[(1-\alpha)\bar{\rho}_\ell]_t + [(1-\alpha)\bar{\rho}_\ell \bar{u}]_z = 0$ (by symmetry)

$$(1-\alpha)\bar{\rho}_\ell = \frac{1}{A} \int_A x_\ell \rho_\ell dA$$

$$(1-\alpha)\bar{\rho}_\ell \bar{u} = \frac{1}{A} \int_A x_\ell \rho_\ell u dA \quad u = \underline{u} \cdot \underline{k} \quad x_\ell = 1 - x_g$$

(b) Drop the bars, ρ_g, ρ_ℓ constant

mass eqs $\rightarrow$

$$\begin{aligned} \alpha_t + (\alpha v)_z &= 0 \\ -(1-\alpha)_t + [(1-\alpha)u]_z &= 0 \end{aligned}$$

$\Rightarrow$ momentum $\rho_g \alpha (v_t + uv_z) = -\alpha p_z - \frac{F_{gl}}{A}$

$$\rho_\ell (1-\alpha) (u_t + uu_z) + \rho_\ell (D_\ell - 1) \{ (1-\alpha)u^2 \}_z = -(1-\alpha) p_z + \frac{F_{gl} - F_{lw}}{A}$$

$\hookrightarrow F_{gl} = 2\bar{n}R\sqrt{\alpha} \rho_g \gamma_{sl} |v-u|(v-u), F_{lw} = 2\bar{n}R \rho_\ell \gamma_{lw} |u|u$

$z=0, \alpha=\alpha_0, v=v_0, u=u_0, p=p_0$

Non-dimensionalise

$$z \sim \frac{R}{b_{gl}} \quad t \sim \frac{R}{b_{gl} \varepsilon \alpha_0 v_0}, \quad \alpha = 1 - B\beta, \quad u \sim \varepsilon \alpha_0 v_0, \quad v \sim \alpha_0 v_0,$$

$$p - p_a \sim p_g \alpha_0^2 v_0^2$$

So non-d. ulev conditions are

$$1 - B\beta = \alpha_0, \quad \varepsilon \alpha_0 v_0 u = u_0, \quad \alpha_0 v_0 v = v_0, \quad p_a + p_g \alpha_0^2 v_0^2 p = p_0$$

we get $\frac{b_{gl} \varepsilon \alpha_0 v_0}{R} \cdot -B\beta_t +$

$$\frac{\alpha_0 v_0 b_{gl}}{R} [(1 - B\beta)v]_z = 0$$

$$\Rightarrow -\varepsilon B\beta_t + [(1 - B\beta)v]_z = 0$$

$$\frac{b_{gl} \varepsilon \alpha_0 v_0}{R} B\beta_t + \varepsilon \alpha_0 v_0 \frac{b_{gl}}{R} [B\beta u]_z = 0$$

$$\Rightarrow \beta_t + (\beta u)_z = 0$$

gas momentum

$$p_g (1 - B\beta) \left[\alpha_0 v_0 \frac{b_{gl} \varepsilon \alpha_0 v_0}{R} v_t + \alpha_0^2 v_0^2 \frac{b_{gl}}{R} v v_z \right]$$

$$= -(1 - B\beta) p_g \alpha_0^2 v_0^2 \frac{b_{gl}}{R} p_z - \frac{F_{gl}}{A}$$

now $F_{gl} = 2\pi R \alpha p_g b_{gl} (v - u)|v - u|$ so with $F_{gl} = 2\pi R p_g b_{gl} \alpha_0^2 v_0^2 \Phi_{gl}$

$$\Rightarrow \Phi_{gl} = (1 - B\beta)^k (v - \varepsilon u)|v - \varepsilon u|$$

gas momentum μ : $\div$ by $p_g \alpha_0^2 v_0^2 \frac{b_{sl}}{R}$ (note $A = \bar{n} R^2$) (10)

$$\Rightarrow (1 - B\beta)(\varepsilon v_t + v v_z) = - (1 - B\beta) p_z$$

$$- \frac{2 \bar{n} R p_g b_{sl} \alpha_0^2 v_0^2 R}{\bar{n} R^2} \frac{1}{p_g \alpha_0^2 v_0^2 b_{sl}} \bar{\Phi}_{sl}$$

$$\text{net } (1 - B\beta)(\varepsilon v_t + v v_z) = - (1 - B\beta) p_z - 2(1 - B\beta)^k (v - \varepsilon u) |v - \varepsilon u|$$

liquid momentum dimensional nm-1

$$F_{lw} = 2 \bar{n} R p_l b_{lw} u |u| = 2 \bar{n} R p_l b_{lw} \varepsilon^2 \alpha_0^2 v_0^2 u |u|$$

$$\text{so } \frac{F_{lw}}{A} = \frac{2 \bar{n} R p_l b_{lw}}{\bar{n} R^2} \left(\frac{p_g b_{sl}}{p_l b_{lw}} \right) \alpha_0^2 v_0^2 u |u|$$

$$= \frac{2}{R} p_g b_{sl} \alpha_0^2 v_0^2 u |u|$$

$$\text{so } p_l B\beta \left[\varepsilon \alpha_0 v_0 \frac{b_{sl}}{R} \varepsilon \alpha_0 v_0 u_t + \varepsilon^2 \alpha_0^2 v_0^2 \frac{b_{sl}}{R} u u_z \right]$$

$$+ p_l (D - 1) \left[B\beta \varepsilon^2 \alpha_0^2 v_0^2 \frac{b_{sl}}{R} u^2 \right]_z = - B\beta p_g \alpha_0^2 v_0^2 \frac{b_{sl}}{R} p_z$$

$$+ \frac{2}{R} p_g b_{sl} \alpha_0^2 v_0^2 (1 - B\beta)^k (v - \varepsilon u) |v - \varepsilon u| \leftarrow \frac{F_{sl}}{A}$$

$$- \frac{2}{R} p_g b_{sl} \alpha_0^2 v_0^2 |u| u \leftarrow \frac{F_{lw}}{A}$$

$$\div \log p_\ell \frac{\varepsilon^2 \alpha_0^2 v_0^2 b_{j\ell}}{R}$$

$$\Rightarrow B\beta(u_f + u_{fz}) + (D_\ell - 1) [B\beta u^z]_z$$

$$= -\frac{B p_j}{\varepsilon^2 p_\ell} \beta p_z + \frac{2}{R} \frac{p_j b_{j\ell} \alpha_0^2 v_0^2 \cdot R}{p_\ell \varepsilon^2 \alpha_0^2 v_0^2 b_{j\ell}} \times$$

$$[(1-\varepsilon\beta)^{k_z} (v-\varepsilon u)|v-\varepsilon u| - |u|u]$$

$$= -\frac{B p_j}{\varepsilon^2 p_\ell} \beta p_z + \frac{2 p_j}{\varepsilon^2 p_\ell} [(1-\varepsilon\beta)^{k_z} |v-\varepsilon u|(v-\varepsilon u) - |u|u]$$

$$\text{note } \varepsilon^2 = \frac{p_j}{p_\ell B}, \Rightarrow \frac{p_j}{p_\ell \varepsilon^2} = B$$

$$\begin{aligned} \text{so } B\beta(u_f + u_{fz}) + (D_\ell - 1) B(\beta u^z)_z &= -B^2 \beta p_z \\ &+ 2B[(1-\varepsilon\beta)^{k_z} |v-\varepsilon u|(v-\varepsilon u) - |u|u] \end{aligned}$$

$$\Rightarrow \beta(u_f + u_{fz}) + (D_\ell - 1)(\beta u^z)_z = -B\beta p_z + 2[(1-\varepsilon\beta)^{k_z} |v-\varepsilon u|(v-\varepsilon u) - |u|u]$$

(c) Summary

$$-\varepsilon B \beta_t + [(1-B\beta)v]_z = 0$$

$$\beta_t + (\beta u)_z = 0$$

$$(1-B\beta)(\varepsilon v_t + v v_z) = -(1-B\beta)p_z - 2(1-B\beta)^{1/2} |v - \varepsilon u| (v - \varepsilon u)$$

$$\beta(u_t + u u_z) + (D_1 - 1)(\beta u)_z = -B\beta p_z + 2[(1-B\beta)^{1/2} |v - \varepsilon u| (v - \varepsilon u) - |u|u]$$

l.b.c's: $1-B\beta = \alpha_0$, $u = \frac{u_0}{\varepsilon \alpha_0 v_0}$, $v = \frac{1}{\alpha_0}$, $p = \frac{p_0 - p_a}{\rho_0 \alpha_0^2 v_0^2}$ at $z=0$

Now $D_1 - 1 \ll 1$, $B \ll 1$, $\varepsilon \ll 1$

$$\Rightarrow \text{define } \alpha_0 = 1 - B\beta_0 \quad u_0 = \varepsilon v_0 u^*, \quad \frac{p_0 - p_a}{\rho_0 v_0^2} = p^*$$

$$\Rightarrow \beta = \beta_0, \quad u \approx u^*, \quad v \approx 1, \quad p \approx p^* \text{ at } z=0.$$

△

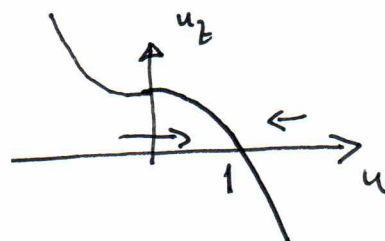
$$v_z = 0 \Rightarrow v \approx 1$$

$$\beta_t + (\beta u)_z = 0$$

$$0 \approx -p_z - 2v^2 \Rightarrow p \approx p^* - 2z$$

$$\beta(u_t + u u_z) \approx 1 - |u|u$$

Steady state $\beta u = \beta_0 u^*$
 $\beta_0 u^* u_z = 1 - |u|u$



$$\text{If } u > 1 \quad \int_{u^*}^u \frac{du}{u^2 - 1} = -\frac{z}{\beta_0 u^*}$$

$$z = \beta_0 u^* \int_u^{u^*} \frac{du}{u^2 - 1} = \frac{\beta_0 u^*}{2} \int du \left(\frac{1}{u-1} - \frac{1}{u+1} \right) = \frac{\beta_0 u^*}{2} \ln \left[\frac{u-1}{u+1} \frac{u^*+1}{u^*-1} \right] \text{ etc}$$

3/ Energy equation is

$$\rho L + \frac{\rho_g}{\alpha} p_s (T_t + v T_z) + (1-\alpha) \rho_e c_{pe} (T_t + u T_z) - \{(\alpha p_s)_t + (\alpha p_s v)_z\} - [\{(1-\alpha) \rho_e\}_t + \{(1-\alpha) \rho_e u\}_z] = Q$$

$$\text{where } \Gamma = (\alpha p_s)_t + (\alpha p_s v)_z = -[\{(1-\alpha) \rho_e\}_t + \{(1-\alpha) \rho_e u\}_z]$$

Energy is thus

$$\rho L + \alpha p_s (h_{st} + v h_{sz}) + (1-\alpha) \rho_e (h_{et} + u h_{ez}) - \{(\alpha p_s)_t + (\alpha p_s v)_z\} - [\{(1-\alpha) \rho_e\}_t + \{(1-\alpha) \rho_e u\}_z] = Q$$

~~$$\text{Now subtract } \{(\alpha p_s)_t + (\alpha p_s v)_z\}$$~~

$$\text{viz } \Gamma (h_s - h_e) + \dots$$

$$\text{viz } h_s [(\alpha p_s)_t + (\alpha p_s v)_z] + \alpha p_s (h_{st} + v h_{sz}) + h_e [\{(1-\alpha) \rho_e\}_t + \{(1-\alpha) \rho_e u\}_z] + (1-\alpha) \rho_e (h_{et} + u h_{ez}) - \dots = Q$$

$$\text{viz } (\alpha p_s h_s)_t + (\alpha p_s v h_s)_z - \frac{\alpha}{\rho_s} (\alpha p_s)_t - (\alpha p_s v)_z + \{(1-\alpha) \rho_e h_e\}_t + \{(1-\alpha) \rho_e h_e u\}_z - \{(1-\alpha) \rho_e\}_t - \{(1-\alpha) \rho_e u\}_z = Q$$

$$\text{viz } \{\alpha (p_s h_s - p_s)\}_t + \{\alpha v (p_s h_s - p_s)\}_z + \{(1-\alpha) (\rho_e h_e - p_e)\}_t + \{(1-\alpha) (\rho_e h_e - p_e) u\}_z = Q$$

$$u \frac{\partial}{\partial z} (\alpha \rho_g e_g)_t + (\alpha \rho_g e_g v) \frac{\partial}{\partial z} \\ + \{ (1-\alpha) \rho_l e_l \}_t + \{ (1-\alpha) \rho_l e_l u \}_z = Q$$

$$p = \rho_l (1-\alpha) + \rho_g \alpha$$

$$T = (1-\alpha) T_l + \alpha T_g$$

$$\rho e = \alpha \rho_g e_g + (1-\alpha) \rho_l e_l$$

$$h = e + \frac{p}{\rho}$$

$$\Rightarrow \rho h = \rho e + p = \alpha \rho_g e_g + (1-\alpha) \rho_l e_l \\ + \alpha p_g + (1-\alpha) p_l \\ = \alpha \rho_g h_g + (1-\alpha) \rho_l h_l$$

Now suppose $u = v$ (homogeneous flow)

The energy equation is then

$$\{ \alpha \rho_g e_g + (1-\alpha) \rho_l e_l \}_t + [\{ \alpha \rho_g e_g + (1-\alpha) \rho_l e_l \} u]_z = Q$$

$$\text{i.e. } (\rho e)_t + (\rho e u)_z = Q$$

$$\hookrightarrow \rho_t + (\rho u)_z = 0 \quad \text{so} \quad \underline{\rho \frac{de}{dt} = Q}, \quad \frac{d}{dt} = \frac{\partial}{\partial t} + u \frac{\partial}{\partial z}$$

We have $h = e + \frac{p}{\rho}$. When $\alpha = 0$, $p = p_l$, $e = e_l$, $\rho = \rho_l$

$$\Rightarrow h = h_l$$

$$\text{Similarly } \alpha = 1 \quad h = h_g$$

So as $\alpha : 0 \rightarrow 1$ $\Delta h \approx h_g - h_f = L$

and $\Delta h = \Delta e + \frac{\Delta p}{\rho}$

$$\Delta\left(\frac{p}{\rho}\right) < \frac{\Delta p}{\rho_g}$$

so if $\Delta p \ll \rho_g L$ then $\Delta\left(\frac{p}{\rho}\right) \ll \Delta h$

$$\Rightarrow \underline{h \approx e}$$

In this case $\rho \frac{dh}{dt} \approx Q$

Now $p = p_e - \Delta p$

$$\Delta p = p_e - p_g$$

$$\Rightarrow \alpha = \frac{p_e - p}{\Delta p}$$

$$\hookrightarrow p h = \alpha p_g h_g + (1-\alpha) p_e h_e$$

$$= p_e h_e + \frac{(p_g h_g - p_e h_e)(p_e - p)}{\Delta p}$$

$$= \frac{p_e h_e (p_e - p_g) + (p_g h_g - p_e h_e) p_e - (p_g h_g - p_e h_e) p}{\Delta p}$$

$$\text{thus } h = \frac{p_e p_g L}{\Delta p \rho} - \frac{(p_g h_g - p_e h_e)}{\Delta p}$$

$$\text{thus } \rho \frac{dh}{dt} = \frac{p_e p_g L}{\Delta p} \cdot p \cdot \frac{-1}{p^2} \frac{dp}{dt} = \frac{p_e p_g L}{\Delta p} u_z = Q$$

(note $\frac{dp}{dt} = -\rho u_z$)

$$\Rightarrow \underline{u_z = \frac{(p_e - p_g) Q}{p_e p_g L}}$$

4/

$$\rho_f + u \rho_z = -u_z \rho$$

$$\rho(u_f + u u_z) = -p_z - \rho g - \frac{4\beta \rho_f u^2}{d}$$

$$\rho(h_f + u h_z) = Q$$

$$h \approx h^* + \frac{\rho_f h}{\rho} \quad (\text{if } \alpha > 0)$$

$$z=0 \quad h=h_0, \quad u=U(t)$$

$$z=r \quad h=h_{\text{set}}$$

$$\text{For } z < r, \quad p = p_f, \quad h_f + u h_z = \frac{Q}{\rho_f}, \quad u = U(t) \quad (\text{as } u_z = 0)$$

$$\text{characteristics} \quad \begin{aligned} \dot{z} &= U \\ \dot{h} &= \frac{Q}{\rho_f} \end{aligned}, \quad z=0, \quad t=\eta, \quad h=h_0$$

$$\Rightarrow h = \frac{Q}{\rho_f}(t-\eta) + h_0, \quad z = \int_{\eta}^t U(s) ds$$

$$\text{at } z=r(t), \quad h=h_{\text{set}} \Rightarrow \eta = t - \frac{\rho_f(h_{\text{set}} - h_0)}{Q} = t - \tau, \quad \tau = \frac{\rho_f(h_{\text{set}} - h_0)}{Q}$$

$$\text{thus } r = \int_{t-\tau}^t U(s) ds$$

In the single-phase region the pressure drop is

$$\begin{aligned} \Delta p_{\text{sp}} &= \int_0^r -p_z dz = \int_0^r \left[\rho_f \ddot{U} + \rho_f g + \frac{4\beta \rho_f U^2}{d} \right] dz \\ &= \left[\rho_f \ddot{U} + \rho_f g + \frac{4\beta \rho_f U^2}{d} \right] r \end{aligned}$$

(17)

Non-dimensionalise via

$$p \sim p_l, z, r \sim l, t \sim \tau, u, V \sim u_0 = \frac{l}{\tau}$$

(non-d)

$$\Rightarrow \Delta p_{sp} = [p_l u_0^2 \dot{U} + p_l g l + \frac{4 \beta l p_l u_0^2}{d} U^2] r$$

$$= [\Delta p_i \dot{U} + \Delta p_g + \Delta p_f U^2] r, \text{ also } r = \int_{t-1}^t u(s) ds$$

$$\Delta p_i = p_l u_0^2$$

$$\Delta p_g = p_l g l$$

$$\Delta p_f = \frac{4 \beta l p_l u_0^2}{d}$$

(all non-d)

For $z > r$

$$p_t + u p_z = -u_z p$$

$$\text{also (dimensional): } p \cdot p_3 L \cdot -\frac{1}{p^2} \frac{dp}{dz} = Q$$

$$\text{or } p_3 L u_z = Q$$

$$\left(\frac{dp}{dz} = -u_z p \right)$$

$$\text{non-d } u_z = \frac{Q}{p_3 L} \frac{l}{u_0} = \frac{Q \tau}{p_3 L} = \frac{p_l \Delta h}{p_3 L}, \Delta h = h_{set} - h_0$$

$$\text{Define } \varepsilon = \frac{p_3 L}{p_l \Delta h}$$

$$\text{then } u_z = \frac{1}{\varepsilon} \Rightarrow u = U \text{ at } z = r$$

$$\Rightarrow u = U + \frac{z-r}{\varepsilon}$$

(18)

The characteristics for p are thus (non-1)

$$\dot{z} = u = U + \frac{z-r}{\varepsilon}$$

$$\dot{p} = -\frac{1}{\varepsilon} p$$

$$\Delta \quad t=\eta, \quad z=r(\eta), \quad p=1$$

$$\text{giving } p = \exp[-(t-\eta)/\varepsilon] \quad \Rightarrow \quad \eta = t - \varepsilon \ln \frac{1}{p}$$

$$\dot{z} = U + \frac{z-r}{\varepsilon}$$

$$\dot{z} - \frac{z}{\varepsilon} = U - \frac{r}{\varepsilon}$$

$$(z e^{-t/\varepsilon})' = (U - \frac{r}{\varepsilon}) e^{-t/\varepsilon}$$

$$z e^{-t/\varepsilon} = r(\eta) e^{-\eta/\varepsilon} + \int_{\eta}^t \left\{ U(s) - \frac{r(s)}{\varepsilon} \right\} e^{-s/\varepsilon} ds$$

$$\text{viz } z = r(\eta) e^{\frac{t-\eta}{\varepsilon}} + \int_{\eta}^t \left\{ U(s) - \frac{r(s)}{\varepsilon} \right\} e^{\frac{t-s}{\varepsilon}} ds$$

$$\text{writing } s = t - \varepsilon \xi, \quad \eta = t - \varepsilon \ln \frac{1}{p}, \quad \text{note when } s = \eta, \quad \xi = \ln \frac{1}{p}$$

$$z = r(t - \varepsilon \ln \frac{1}{p}) \frac{1}{p} + \int_0^{\ln \frac{1}{p}} \{ \varepsilon U(t - \varepsilon \xi) - r(t - \varepsilon \xi) \} e^{\xi} d\xi$$

$$\text{Integrating by parts, } \int_0^{\ln \frac{1}{p}} r(t - \varepsilon \xi) e^{\xi} d\xi$$

$$= [e^{\xi} r(t - \varepsilon \xi)]_0^{\ln \frac{1}{p}} + \varepsilon \int_0^{\ln \frac{1}{p}} e^{\xi} r'(t - \varepsilon \xi) d\xi$$

$$= r(t - \varepsilon \ln \frac{1}{p}) \frac{1}{p} - r(t) + \varepsilon \int_0^{\ln \frac{1}{p}} e^{\xi} [U(t - \varepsilon \xi) - U_1(t - \varepsilon \xi)] d\xi$$

$$\{ U_1(t) = U(t-1) \}$$

thus

$$\begin{aligned}
 z &= r(t - \varepsilon \ln \frac{1}{\rho}) \cdot \frac{1}{\rho} + \int_0^{\ln \frac{1}{\rho}} \varepsilon U(t - \varepsilon \xi) e^{\xi} d\xi \\
 &\quad - \left[r(t - \varepsilon \ln \frac{1}{\rho}) \cdot \frac{1}{\rho} - r(t) + \varepsilon \int_0^{\ln \frac{1}{\rho}} e^{\xi} [U(t - \varepsilon \xi) - U_1(t - \varepsilon \xi)] d\xi \right] \\
 &= r(t) + \varepsilon \int_0^{\ln \frac{1}{\rho}} U_1(t - \varepsilon \xi) e^{\xi} d\xi
 \end{aligned}$$

In dimensional terms, the two-phase pressure drop is

$$\Delta p_{tp} = \int_r^z \left[(\rho u)_t + (\rho u^2)_z + \rho g + \frac{4\beta \rho}{d} u^2 \right] dz$$

& the LHS in dimensional terms $\Phi(\rho, u)$ is

$$\Delta p_i \underbrace{\int_r^z [(\rho u)_t + (\rho u^2)_z] dz}_{\Phi_i} + \Delta p_g \underbrace{\int_r^z \rho dz}_{\Phi_g} + \Delta p_f \underbrace{\int_r^z \rho u^2 dz}_{\Phi_f}$$

Steady state

$U = V$, $r = V$. We need $V < 1$ so there is a two-phase region!

We have in the two-phase region $u = V + \frac{z-V}{\varepsilon}$, & $\rho u = V$

Then $\Delta p = \Delta p_g + \Delta p_{tp}$

$$= (\Delta p_g + \Delta p_g V^2) V$$

$$+ \Delta p_i [V u]_r^1 + \Delta p_g \int_r^1 \frac{V dz}{u} + \Delta p_f \int_r^1 V u dz$$

$$\text{viz } \Delta p = (\Delta p_g + \Delta p_f v^2) v$$

$$+ \frac{\Delta p_i}{\varepsilon} v(1-v) + \Delta p_g v \varepsilon \ln \left[\frac{v + \frac{(1-v)}{\varepsilon}}{v} \right] + \Delta p_f v \left[v^2 + \frac{(1-v)^2}{2\varepsilon} \right]_v^1$$

$$\Rightarrow \Delta p = \frac{\Delta p_i}{\varepsilon} v(1-v) + \Delta p_g v \left[1 + \varepsilon \ln \left\{ \frac{v + \frac{1-v}{\varepsilon}}{v} \right\} \right] + \Delta p_f \left[v^2 + \frac{v(1-v)}{2\varepsilon} \right]$$

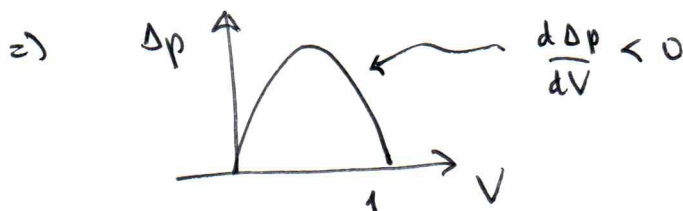
If v is close to 1

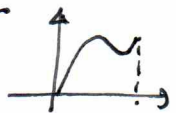
$$\text{then } \Delta p \approx \Delta p_g v + \Delta p_f v^2 + o(1-v) \quad \text{is increasing with } v$$

but for small ε

$$\Delta p \approx \frac{1}{\varepsilon} \left[\Delta p_i v(1-v) + \Delta p_f v(1-v)^2 \right]$$

$$= \frac{v(1-v)}{\varepsilon} \underbrace{[\Delta p_i + \Delta p_f (1-v)]}_{>0}$$



[compare i 

□

next, $\Delta p_i = \Delta p_g = 0$, so

$$\frac{\Delta p}{\Delta p_f} = \Pi, \text{ say,}$$

$$= U^2 r + \int_r^1 \rho u^2 dz$$

single
phase

two
phase

Linear stability

(2)

with

$$U = V + v, \quad r = r_0 + r_1, \quad u = u_0 + u_1, \quad p = p_0 + p_1$$

we have $r_0 = V, \quad u_0 = V + \frac{z-V}{\epsilon}, \quad p_0 = \frac{2}{\epsilon} \frac{V}{u_0} = \frac{V}{V + \frac{z-V}{\epsilon}}$

$$r = \int_{t-1}^t U(s) ds$$

$$\text{so } r_1 = \int_{t-1}^t v ds$$

$$u = U + \frac{z-r}{\epsilon} \Rightarrow u_1 = v - \frac{r_1}{\epsilon}$$

Note also $z = r(t) + \epsilon \int_0^{\frac{1}{p}} U_1(t-\epsilon \xi) e^{\xi} d\xi$

$$= r_0 + r_1 + \epsilon \int_0^{-\ln p_0 - \frac{p_1}{p_0}} \{V + v_1(t-\epsilon \xi)\} e^{\xi} d\xi$$

$\begin{aligned} \ln \frac{1}{p} &= -\ln p \\ &= -\ln(p_0 + p_1) \\ &= -\ln p_0 - \frac{p_1}{p_0} \dots \end{aligned}$

linearising

$$0 = r_1 + \epsilon \int_0^{\ln \frac{1}{p_0}} v_1(t-\epsilon \xi) e^{\xi} d\xi$$

$$-\frac{\epsilon p_1}{p_0} \frac{V}{p_0}$$

$$\Rightarrow p_1 \approx \frac{p_0^2}{V} \left[\frac{r_1}{\epsilon} + \int_0^{\ln \frac{1}{p_0}} v_1(t-\epsilon \xi) e^{\xi} d\xi \right]$$

$$= U^2 r + \int_0^1 \epsilon u^2 dz$$

Linearising the condition $\frac{\Delta p}{\Delta p_f} = \text{constant}$, we have

$$0 = V^2 r_1 + 2V^2 v - r_1 p_0 u_0^2 \Big|_{r_0} + \int_{r_0}^1 p_1 u_0^2 dz + \int_{r_0}^1 2p_0 u_0 u_1 dz$$

single phase

$$= V^2 r_1 + 2V^2 v - V^2 r_1 + \int_{r_0}^1 (p_1 u_0^2 + 2p_0 u_1) dz$$

$$\text{ii } 2V^2 v + \int_{r_0}^1 (p_1 u_0^2 + 2p_0 u_1) dz = 0$$

= p.

$$\text{Since } p_0 u_0 = V,$$

$$p_1 u_0^2 = V \left[\frac{\eta}{\varepsilon} + \int_0^{\frac{1}{p_0}} v_1(t - \varepsilon \xi) e^{\xi} d\xi \right]$$

$$\text{So } \begin{bmatrix} +V^2 \hat{r}_1 & -V^2 \hat{r}_1 \end{bmatrix} \\ 0 = 2V^2 v + \int_{r_0}^1 V \left[2u_1 + \frac{\eta}{\varepsilon} + \int_0^{\frac{1}{p_0}} v_1(t - \varepsilon \xi) e^{\xi} d\xi \right] dz$$

s.p.

$$\text{Now we put } v = e^{\sigma t};$$

$$\text{then } r_1 = \frac{1}{\sigma} (1 - e^{-\sigma}) e^{\sigma t}$$

$$u_1 = \left[1 - \frac{1}{\varepsilon \sigma} (1 - e^{-\sigma}) \right] e^{\sigma t}$$

$$\begin{aligned} \text{we have } \int_0^{\frac{1}{p_0}} v_1(t - \varepsilon \xi) e^{\xi} d\xi &= \int_0^{\frac{1}{p_0}} e^{\sigma(t - \varepsilon \xi)} e^{\xi} d\xi \\ &= e^{\sigma t} \int_0^{\frac{1}{p_0}} e^{(1 - \varepsilon \sigma) \xi} d\xi \times e^{-\sigma} \\ &= e^{\sigma t} \left[\frac{e^{-\sigma}}{1 - \varepsilon \sigma} \left\{ \frac{1}{p_0^{1 - \varepsilon \sigma}} - 1 \right\} \right] \\ &= \frac{e^{\sigma t - \sigma}}{1 - \varepsilon \sigma} \left[\left(1 + \frac{2 - V}{\varepsilon V} \right)^{1 - \varepsilon \sigma} - 1 \right], \end{aligned}$$

$$\begin{aligned} \text{so } \begin{bmatrix} +V^2 \hat{r}_1 & -V^2 \hat{r}_1 \end{bmatrix} \\ 2V^2 + \underbrace{V(1 - V) \left[2 \left\{ 1 - \frac{1}{\varepsilon \sigma} (1 - e^{-\sigma}) \right\} + \frac{1}{\varepsilon \sigma} (1 - e^{-\sigma}) \right]}_{2 - \frac{1}{\varepsilon \sigma} (1 - e^{-\sigma})} \\ + \frac{V e^{\sigma}}{1 - \varepsilon \sigma} \int_V^1 \left\{ \left(1 + \frac{2 - V}{\varepsilon V} \right)^{1 - \varepsilon \sigma} - 1 \right\} dz = 0 \end{aligned}$$

s.p.

viz

$$2V^2 \left[+ V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) - V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) \right]$$

single phase $0 < \sigma < \infty$

$$+ V(1-V) \left[2 - \frac{1}{\varepsilon \sigma} (1 - e^{-\sigma}) \right] + \frac{V e^{-\sigma}}{(1 - \varepsilon \sigma)} \left[\frac{\varepsilon V}{2 - \varepsilon \sigma} \left\{ \left(1 + \frac{1-V}{\varepsilon V} \right)^{2 - \varepsilon \sigma} - 1 \right\} - (1-V) \right] = 0$$

(*) only include the single-phase pressure drop:

$$\Rightarrow 2V^2 + V^2 \frac{1}{\sigma} (1 - e^{-\sigma}) = 0$$

$$\text{Then } \frac{1}{\sigma} (1 - e^{-\sigma}) + 2 = 0$$

$$\Rightarrow \underline{\sigma = -\frac{1}{2} (1 - e^{-\sigma})}$$

Suppose $\text{Re } \sigma > 0$: then $|e^{-\sigma}| < 1$, so $\text{Re}(1 - e^{-\sigma}) > 0$
 so $\text{Re } \sigma = -\frac{1}{2} \text{Re}(1 - e^{-\sigma}) < 0$ $\Rightarrow \text{Re } \sigma < 0$

(note $\sigma = 0$ is always a root: since $\frac{\Delta p}{\Delta p_f} = U^2(t) \int_{t-1}^t U(s) ds$)

this is associated with time translational invariance.)

Now as $\sigma \rightarrow \infty$ (LHS) we must have

$$e^{-\sigma} \rightarrow -\delta$$

$$\approx e^{\sigma} \rightarrow -\frac{1}{\delta}$$

$$\sigma \rightarrow \ln \frac{1}{\delta} + (2n+1)i\pi$$

is ill-posed for $\delta < 1$ (as then $\text{Re } \sigma > 0$ as $n \rightarrow \infty$)

(d) If we also include the inertial term in the angle phase region

$\Delta p_i \dot{U}$, then (c) is modified to

$$\frac{\Delta p_i}{\Delta p_f} \sigma + 2V^2 - \frac{V(1-V)}{\varepsilon} \frac{1}{\sigma} (1-e^{-\sigma}) + \frac{(1-V)^2}{2\varepsilon} e^{-\sigma} = 0$$

$$\Rightarrow V\sigma + \delta - \gamma \frac{1}{\sigma} (1-e^{-\sigma}) + e^{-\sigma} = 0, \quad V = \frac{2\varepsilon \Delta p_i}{(1-V)^2 \Delta p_f}$$

$$\Rightarrow \underline{V\sigma^2 + \sigma(\delta + e^{-\sigma}) - \gamma(1-e^{-\sigma}) = 0}$$

$$\underline{\delta = \frac{4\varepsilon V^2}{(1-V)^2}}$$

Now as $\sigma \rightarrow \infty$ we must have $\sigma(\delta + e^{-\sigma}) \gg \gamma(1-e^{-\sigma})$

So we must have

$$V\sigma^2 \approx -\sigma(\delta + e^{-\sigma})$$

$$\text{i.e. } \underline{V\sigma \approx -\delta - e^{-\sigma}}$$

LHS $\rightarrow \infty \Rightarrow e^{-\sigma} \rightarrow 0 \Rightarrow \text{Re } \sigma \rightarrow -\infty \Rightarrow \text{well-posed.}$

Instability Clearly as $V, \delta \rightarrow 0$ there is instability because of (b)

Therefore the steady state is unstable for sufficiently small V & δ , i.e. small enough ε .