

C5.11 Solutions

1. (a) $\mu \frac{\partial I}{\partial z} = -\rho \kappa (I - B)$ $\mu = \cos \theta \quad d\mu = -\sin \theta \, d\theta.$

$$I_+ = \int_0^{2\pi} \int_0^{\pi/2} I \sin \theta \, d\theta \, d\phi = 2\pi \int_0^1 I \, d\mu \quad (2)$$

$$I_- = \int_0^{2\pi} \int_{\pi/2}^\pi I \sin \theta \, d\theta \, d\phi = 2\pi \int_{-1}^0 I \, d\mu$$

Approximate $\int_0^1 \mu I \, d\mu \approx \frac{1}{2} I_+$ and $\int_{-1}^0 \mu I \, d\mu \approx -\frac{1}{2} I_-$.

Integrate radiative transfer equation $(\int_0^1 d\mu + \int_{-1}^0 d\mu)$

$$\Rightarrow \frac{1}{2} \frac{\partial I_+}{\partial z} = -\rho \kappa (I_+ - B) \quad \text{with } B = \frac{\sigma T^4}{\pi} \quad (3)$$

$$-\frac{1}{2} \frac{\partial I_-}{\partial z} = -\rho \kappa (I_- - B)$$

$\pi I_+ = \sigma T_s^4$ at $z=0$ is Stefan Boltzmann law for radiative emission from ground.
(T_s = surface temp) (3)

$I_- \rightarrow 0$ as $z \rightarrow \infty$ means no incoming longwave radiation from space

(b) $\frac{dI}{dz} = -\rho \kappa \quad \tau \rightarrow 0 \text{ as } z \rightarrow \infty \Rightarrow I = \int_z^\infty \rho \kappa \, dz$

$$\frac{1}{2} \frac{dI_+}{d\tau} = I_+ - \frac{\sigma T^4}{\pi} \quad \text{with } I_+ = \frac{\sigma T_s^4}{\pi} \text{ at } \tau = \tau_s = \int_0^\infty \rho \kappa \, dz.$$

$$\left(\frac{1}{2} \frac{dI_-}{d\tau} = I_- - \frac{\sigma T^4}{\pi} \right) \quad (3)$$

integrating factor $e^{-2\tau} \Rightarrow \frac{d}{d\tau} (I_+ e^{-2\tau}) = -\frac{2\sigma T^4}{\pi} e^{-2\tau}$

$$\text{so } I_+ e^{-2\tau} - \frac{\sigma T_s^4}{\pi} e^{-2\tau_s} = - \int_{\tau_s}^{\tau} \frac{2\sigma T^4}{\pi} e^{-2\tau'} \, d\tau' \quad N.$$

$$\Rightarrow \boxed{I_+ = \frac{\sigma T_s^4}{\pi} e^{-2(\tau_s - \tau)} + \int_{\tau}^{\tau_s} \frac{2\sigma T^4}{\pi} e^{-2(\tau' - \tau)} \, d\tau'} \quad (3)$$

$$\Rightarrow \boxed{\gamma = \frac{\pi I_+(0)}{\sigma T_s^4} = e^{-2\tau_s} + \int_0^{\tau_s} 2 \left(\frac{T}{T_s}\right)^4 e^{-2\tau'} \, d\tau'} \quad (1)$$

N.
(straightfrom

$$P c_p \frac{dT}{dz} - \frac{dp}{dz} = 0. \quad p = \rho R T$$

$$\Rightarrow \frac{dT}{dp} = - \frac{1}{\rho c_p} = \frac{RT}{c_p \rho M}$$

$$\Rightarrow \ln T = \frac{R}{c_p M} \ln p + \text{constant}$$

$$\frac{T}{T_s} = \left(\frac{p}{p_s} \right)^{\frac{R}{c_p M}} \quad (4)$$

d) If pressure hydrostatic law $\frac{dp}{dz} = -\rho g$ & $\frac{di}{dz} = -\rho \kappa$. $\Rightarrow \frac{dp}{di} = \frac{g}{\kappa}$ so p & i are linearly related.

$$p = \frac{g}{\kappa} i \quad (\text{since } p \text{ and } i \text{ both } 0 \text{ at } z \rightarrow \infty).$$

$$\Rightarrow \frac{T}{T_s} = \left(\frac{i}{i_s} \right)^{\frac{R}{c_p M}} \quad (2)$$

(3)
[If $i_s \ll 1$, then integral term in γ is small and $\gamma \approx e^{-2i_s} \approx 1$.]

N

If $i_s \gg 1$, then first term e^{-2i_s} is exponentially small, and integral is approximately

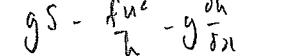
$$\gamma \approx \int_0^\infty 2 \left(\frac{i}{i_s} \right)^{\frac{4R}{c_p M}} e^{-2i} di \quad i \rightarrow \frac{1}{2} i$$

$$= \frac{1}{(2i_s)^{\frac{4R}{c_p M}}} \underbrace{\int_0^\infty \hat{i}^{\frac{4R}{c_p M}} e^{-\hat{i}} d\hat{i}}_{\Gamma \left(1 + \frac{4R}{c_p M} \right)} \quad (3), (4)$$

$$2. (a) \frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(hu) = i \quad \text{conservation of mass}$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = gS - \frac{f u^2}{h} - g \frac{\partial h}{\partial x}$$

centrifugal of momentum


 gravitational force
 turbulent drag.
 pressure force
 (hydrostatic pressure)

$(S = \beta g \rho_i)$

Negative values of r might represent seepage into the underlying bed or evaporation.

$$S = \frac{Q}{L} \cdot \frac{L}{h} = \frac{Q}{h}, \quad gS = \frac{f u^2}{h}$$

$$\Rightarrow \left(g \frac{S R_o L}{f} \right)^3 = [u]. \quad [L] = \frac{R_o L}{[u]}, \quad [t] = \frac{L}{[u]}.$$

$$\text{Then } \frac{\partial h}{\partial t} + \frac{\partial}{\partial t}(hu) = r$$

$$\delta = \frac{Ch}{SL}$$

$$\delta F^2 \left(\frac{\partial u}{\partial t}, u \frac{\partial u}{\partial x} \right) = 1 - \frac{u^2}{h} - \int \frac{\partial h}{\partial x} \\ F^2 = \frac{[u]^2}{g[h]}.$$

$$F^2 = \frac{[n]^2}{g[h]}.$$

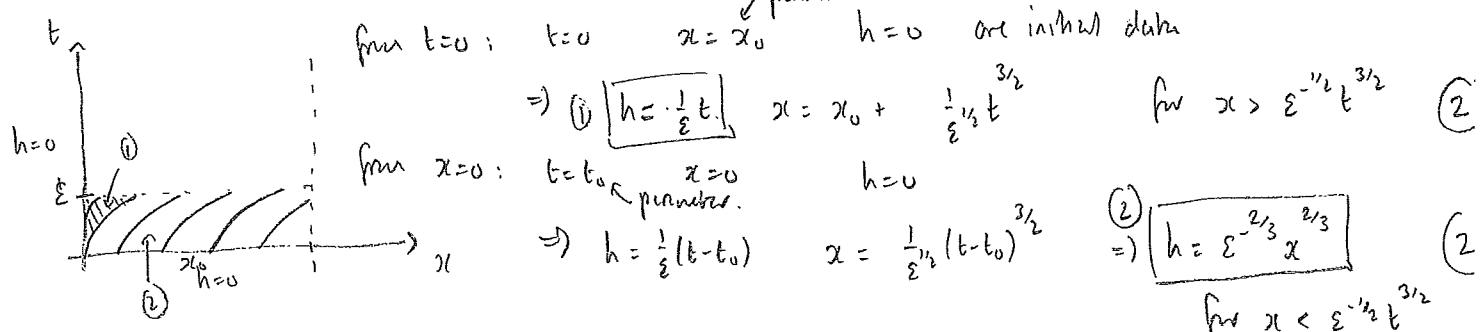
$$(b) \text{ If } f_{\text{ext}} = f_{\text{ext}}, \text{ second eqn} \Rightarrow v = h^{\frac{1}{2}}$$

$$\Rightarrow \frac{\partial h}{\partial t} + \frac{3}{2} h^{1/2} \frac{\partial h}{\partial x} = c$$

$b = 0$ at $t = 0$. ($x > 0$) Initial condition

$b = 0$ at $x = 0$ ($t > 0$). Boundary condition

(c) Octet : Characteristics have $i=1$ $i = \frac{3}{2} h^{1/2}$ $h = \frac{1}{\epsilon}$



$$\text{At } t = \varepsilon, h \begin{cases} 1 & x > \varepsilon \\ \left(\frac{x}{\varepsilon}\right)^{\frac{2}{2+\beta}} & x < \varepsilon. \end{cases}$$

$$t > \varepsilon \quad \text{Characteristics now} \quad t=1 \quad \dot{x} = \frac{3}{2} h^{1/2} \quad \dot{h} = -1.$$

from $x > \varepsilon$, how $t = \varepsilon$, $x = x_1$ \checkmark parameter. $h = 1$

$$\Rightarrow \boxed{(3) \quad h = 1 - t + \varepsilon} \quad x = x_1 + \left(1 - (1 - t + \varepsilon)^{3/2} \right). \quad \begin{array}{l} h \text{ reaches zero} \\ \text{when } t = 1 + \varepsilon. \end{array} \quad (2)$$

from $x < \varepsilon$, $t = \varepsilon$, $x = x_1$, $h = \left(\frac{x_1}{\varepsilon}\right)^{2/3}$

$$\Rightarrow \boxed{(4) \quad h = \left(\frac{x_1}{\varepsilon}\right)^{2/3} - t + \varepsilon \quad x = x_1 + \left(\frac{x_1}{\varepsilon} - \left(\left(\frac{x_1}{\varepsilon}\right)^{2/3} - t + \varepsilon \right)^{3/2} \right)} \quad (2)$$

$\hookrightarrow h \text{ reaches zero when } t = \varepsilon + \left(\frac{x_1}{\varepsilon}\right)^{2/3}. \quad (\text{for } \varepsilon < t < \varepsilon + 1)$

$$\text{so (eliminate } x_1) \quad x_1 = \varepsilon (t - \varepsilon)^{3/2}$$

$$\Rightarrow x = \varepsilon (t - \varepsilon)^{3/2} \left(1 + \frac{1}{\varepsilon} \right) \quad (\text{reaches } x=1 \text{ at } t = \varepsilon + (1+\varepsilon)^{3/2}) \quad (2)$$

\checkmark ii all from relation (3).

$$\text{At } x=1, \quad h = \begin{cases} \frac{t}{\varepsilon} & 0 < t < \varepsilon \\ 1 - t + \varepsilon & \varepsilon < t < 1 + \varepsilon - \varepsilon^{2/3} \\ ? & 1 + \varepsilon - \varepsilon^{2/3} < t < \varepsilon + (1+\varepsilon)^{2/3} \\ 0 & t > \varepsilon + (1+\varepsilon)^{2/3} \end{cases} \quad \text{so} \quad h = \begin{cases} 1 - t & 0 < t < 1 \\ 0 & t > 1 \end{cases} \quad \text{in limit } \varepsilon \rightarrow 0.$$

$$\Rightarrow \boxed{(Q) \quad h^{3/2} = \begin{cases} (1-t)^{3/2} & 0 < t < 1 \\ 0 & t > 1 \end{cases} \quad \text{known}} \quad (2)$$

$$3. (a) \quad 0 = -p_{x1} + \tau_2 \quad p = \tau = u \text{ at } z = s.$$

$$0 = -p_2 - pg.$$

$$u_2 = 2Az^n \quad u = Ce^m \text{ at } z = b.$$

$$\boxed{\frac{\partial h}{\partial t} + \frac{\partial q}{\partial x} = a}$$

$$q = \int_b^s u dz$$

(2)

$$\text{vertical motion} \Rightarrow p = pg(s-z).$$

$$\text{horizontal motion} \Rightarrow \tau = -pgs_{x1}(s-z) \rightarrow \tau_b = -pgs_{x1}h \quad h = s-b. \quad (4)$$

$$\text{flow law} \Rightarrow u = u_b + \int_b^s 2A(-pgs_{x1})^n (s-z)^n dz$$

$$\boxed{m=1} \quad = C(-pgs_{x1}h)^m + 2A \underbrace{(-pgs_{x1})^n}_{n+1} \left[h^{n+1} - (s-z)^{n+1} \right] \quad B.$$

$$\begin{aligned} q &= \int_b^s u dz = C(pg)^m h^{m+1} (-s_{x1})^m + \frac{2A(pg)^n}{n+1} \left(h^{n+2} - \frac{1}{n+2} h^{n+2} \right) \\ &= C(pg)^m h^{m+1} (-s_{x1})^m + \frac{2A(pg)^n}{n+2} (-s_{x1})^n h^{n+2} \end{aligned} \quad (4)$$

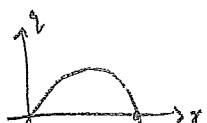
$$\Rightarrow \boxed{\frac{\partial h}{\partial t} + \frac{\partial}{\partial x} \left[C(pg)^m h^{m+1} (-s_{x1})^m + \frac{2A(pg)^n}{n+2} h^{n+2} (-s_{x1})^n \right] = a.}$$

$$\text{non-dimensionalize with } x \sim [x], \alpha \sim [a], \text{ chm. } [h] \text{ is flat} \quad \frac{C(pg)^m [h]^{2m+1}}{[x]^{m+1}} = [a].$$

$$\text{and } [t] \text{ is flat} \quad \frac{[h]}{[t]} = [\alpha],$$

$$\boxed{\alpha = \frac{2A(pg)^{n-m}}{(n+2)C} \frac{[h]^{2(n-m)}}{[x]^{(n-m)}}} \quad (2)$$

$$(b) \quad b=0, \quad a=1-x. \quad q = \int_0^x a = x - \frac{1}{2}x^2 \quad \text{so} \\ q=0 \text{ at } x=2 \Rightarrow \text{in flat extent is } 2.$$



(2)

$$\text{if } \alpha \ll 1, m=1 \quad q = -h^2 h_{x1} = -\frac{1}{3} (h^3)_{x1} \quad \text{so} \quad h^3 = \int_{x1}^2 3 \left(x - \frac{1}{2} x^2 \right) dx \quad (h=0 \text{ at } x=2)$$

$$\text{At } x=0; \quad h^3 = \left[\frac{3}{2}x^2 - \frac{1}{2}x^3 \right]_0^2 = 6 - 4 = 2 \Rightarrow h = 2^{\frac{1}{3}}$$

Max Thickness

(4)

(c) Archimedes \Rightarrow melted exerts upwards force equal to the weight of the amount displaced.

If $b=0$ in absence of ice, this force is $-\rho_m g b$. (per unit area).

This must balance weight of the ice. $\rho g h$, so we need $[-\rho_m b = \rho h]$ (2).

$$\text{Flux becomes } q = -h^2 S_x = -h^2(b+h)_x = -(1 - \frac{\rho}{\rho_m}) h^2 h_x.$$

$$\text{so now } \underbrace{(1 - \frac{\rho}{\rho_m}) h^3}_<1 = \int_0^2 3(x - \frac{1}{2}x^2) dx. \quad \text{i.e. } h \text{ is increased.} \quad (3)$$

$$\text{At } x=0 \quad (1 - \frac{\rho}{\rho_m}) h^3 = 2. \quad \Rightarrow \quad h = 2^{\frac{1}{3}} \left(1 - \frac{\rho}{\rho_m}\right)^{-\frac{1}{3}}$$

$$\text{If } \rho_m = 3\rho_{\text{melt}} \quad 1 - \frac{\rho}{\rho_m} \approx \frac{2}{3} \quad \text{so} \quad h \approx 2^{\frac{1}{3}} \left(\frac{2}{3}\right)^{-\frac{1}{3}} = 3^{\frac{1}{3}} \quad (2).$$