

Problem Sheet 2: Solutions

1. From the vertical component of the momentum equation (after applying the lubrication approximation) we have that

$$\frac{\partial p}{\partial z} = -\rho g$$

so that the pressure distribution within the drop is hydrostatic, i.e.

$$p = p_0 + \rho g [h(r, t) - z] \quad (1)$$

where we have neglected the pressure jump due to surface tension and p_0 is the constant atmospheric pressure.

The horizontal component of the momentum equation is, in the lubrication approximation,

$$\mu \frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial r} = \rho g \frac{\partial h}{\partial r}.$$

Integrating twice subject to $u(z = 0) = 0$ (no-slip) and $u_z(z = h) = 0$ (no stress) we find that

$$u = \frac{\rho g}{2\mu} z(z - 2h) \frac{\partial h}{\partial r},$$

and

$$\bar{u} = -\frac{\rho g}{3\mu} h^2 \frac{\partial h}{\partial r}.$$

At this point is acceptable to quote the general result that

$$\frac{\partial h}{\partial t} + \nabla \cdot \mathbf{q} = 0$$

where $\mathbf{q} = h\bar{u}\mathbf{e}_r$ is the fluid flux, though it would be reasonable to ask for this to be derived:

$$\begin{aligned} \frac{1}{r} \frac{\partial}{\partial r} \left(r \int_0^h u \, dz \right) &= \int_0^h \frac{1}{r} \frac{\partial}{\partial r} (ru) \, dz + h_r u(h) \\ &= - \int_0^h \frac{\partial w}{\partial z} \, dz + u(h) h_r && \text{[Using } \nabla \cdot \mathbf{u} = 0 \text{]} \\ &= -w(h) + w(0) + u(h) h_r \\ &= -[h_t + u(h) h_r] + u(h) h_r && \text{Using the k.b.c. and } w(0) = 0 \\ &= -h_t. \end{aligned}$$

Thus we have

$$h_t = \frac{\rho g}{3\mu} \frac{1}{r} \frac{\partial}{\partial r} \left(r h^3 \frac{\partial h}{\partial r} \right), \quad (2)$$

as desired.

We are told that the volume of the drop is a given constant V and so we must have

$$V = \int_0^{a(t)} 2\pi r h \, dr.$$

In scaling terms we may write volume conservation as $V \sim R^2 H$ where R is a typical radial scale and H a typical vertical scale at time T . In scaling terms the governing pde (2) reads

$$\frac{H}{T} \sim \frac{\rho g H^4}{\mu R^2}$$

from which we have

$$T \sim \frac{\mu}{\rho g} R^2 (H^{-3} \sim R^6/V^3).$$

Hence the typical radial scale R at time T must scale according to

$$R \sim \left(\frac{\rho g V^3}{\mu} T \right)^{1/8}$$

so that the radius $a(t)$ of the droplet must scale in the same way.

To progress further we non-dimensionalize lengths using $V^{1/3}$ and time using $\mu/\rho g V^{1/3}$ so that we wish to solve

$$h_t = \frac{1}{3r} \frac{\partial}{\partial r} \left(r h^3 \frac{\partial h}{\partial r} \right), \quad (3)$$

subject to the volume constraint

$$\int_0^{a(t)} r h \, dr = 1/(2\pi). \quad (4)$$

Based on the scalings discussed above it is natural to seek a similarity solution of the form $h(r, t) = t^{-1/4} \Theta(\eta)$ where $\eta = r t^{-1/8}$ and we expect the drop to occupy the region $0 \leq \eta \leq \eta_*$ where $\eta_* = a(t)/t^{1/8}$ is the position of the edge of the drop; i.e. $h(a(t), t) = 0$.

[*Note that it is better to use the above similarity ansatz than the alternative t/r^8 since we take more spatial derivatives than time derivatives. However, this alternative approach does work if one is sufficiently careful.*]

Substituting this similarity form into (3) we have

$$-\frac{1}{8}(2\Theta + \eta\Theta') = \frac{1}{3\eta} \frac{d}{d\eta} (\eta\Theta^3\Theta').$$

This may be integrated once to give

$$-\frac{3}{8}\eta^2\Theta = \eta\Theta^3\Theta'$$

where the constant of integration must vanish to ensure that the solution is well-behaved as $\eta \rightarrow 0$. A further integration gives

$$\Theta = \left(\frac{3}{4}\right)^{2/3} (\eta_*^2 - \eta^2)^{1/3}$$

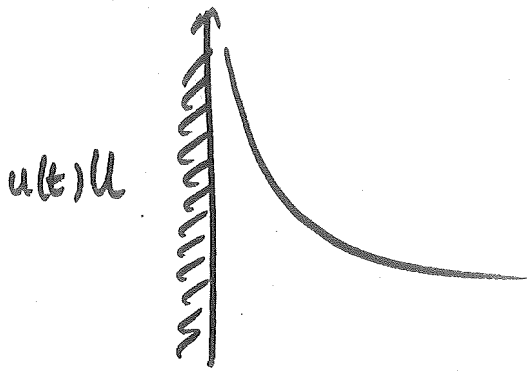
where we have applied the boundary condition that $\Theta(\eta_*) = 0$.

To determine the value of η_* we return to the similarity form of (4), which reads

$$\begin{aligned} \frac{1}{2\pi} &= \int_0^{\eta_*} \eta\Theta \, d\eta = \left(\frac{3}{4}\right)^{2/3} \int_0^{\eta_*} \eta(\eta_*^2 - \eta^2)^{1/3} \, d\eta \\ &= \left(\frac{3}{4}\right)^{2/3} \frac{3}{8}\eta_*^{8/3} \end{aligned}$$

from which we immediately have $\eta_* = (2^{10}/3^5\pi^3)^{1/8}$ and the result for $a(t)$ follows.

Q2



Lectures, Speed u

$$\bar{x} = x - t$$

$$\frac{\partial}{\partial t} = \frac{\partial}{\partial t} + \frac{\partial}{\partial x}$$

$$0 = h_t + h_z + \dots$$

Here Speed $u(t)$

$$\bar{x} = x - \int_0^t u(t') dt'$$

$$\frac{\partial}{\partial t} + u(t) \frac{\partial}{\partial x}$$

$$\rightarrow 0 = h_t + u(t) h_z + \frac{\partial}{\partial z} \left[\frac{h^3}{3a} (h_{zz} - \beta_0) \right]$$

Has scaled $\frac{\partial h_{\text{physical}}}{\partial t_{\text{physical}}}$ with $W = \frac{\delta U}{L} = \frac{HU}{L}$

But will scale with $\frac{H}{T_{\text{boundary}}}$, $T_{\text{boundary}} = \text{timescale boundary changes}$

$$\therefore \left(\frac{H}{T_{\text{boundary}}} \frac{1}{W} \right) \frac{\partial h}{\partial t} + \dots$$

$$= \frac{H|u(t)|}{H|u(t)|}$$

$T \rightarrow \infty$ as $u \rightarrow 0$

$$\frac{H}{T_b} \frac{L}{HU} = \underline{\underline{\left(\frac{L}{T_b u} \right)}}$$

Rescalings, as in notes

$$\lambda \frac{\partial \bar{h}}{\partial t} + u(t) \frac{\partial \bar{h}}{\partial \bar{z}} + \frac{\partial}{\partial \bar{z}} \left[\bar{h}^3 / 3 (\bar{h}_{\bar{z}\bar{z}\bar{z}} - B_0) \right] = 0$$

$\frac{L}{T_b u} \ll 1$ for u sufficiently small.

$$\therefore u(t) \bar{h}_{\bar{z}} + \frac{\partial}{\partial \bar{z}} \left(\bar{h}^3 / 3 \bar{h}_{\bar{z}\bar{z}\bar{z}} \right) = 0.$$

Proceeding...

$$u(t) \frac{\partial \tilde{h}}{\partial \tilde{z}} + \frac{\partial}{\partial \tilde{z}} \left(\frac{\tilde{h}^3}{3} \tilde{h}_{\tilde{z}\tilde{z}\tilde{z}} \right) = 0,$$

which integrates to give

$$u(t) \tilde{h} + \frac{\tilde{h}^3}{3} \tilde{h}_{\tilde{z}\tilde{z}\tilde{z}} = f(t).$$

As $\tilde{z} \rightarrow \infty$, we expect that $\tilde{h} \rightarrow \tilde{h}_0$, a constant and so

$$u(t) \tilde{h} + \frac{\tilde{h}^3}{3} \tilde{h}_{\tilde{z}\tilde{z}\tilde{z}} = u(t) \tilde{h}_0 \tag{6}$$

subject to $\tilde{h} \sim \tilde{z}^2 / \sqrt{2}$ as $\tilde{z} \rightarrow -\infty$.

Following the lecture notes, we let $\tilde{h} = \tilde{h}_0 g(\zeta)$, $\tilde{z} = z_* \zeta$ so that (6) becomes

$$g + \frac{\tilde{h}_0^3}{u(t) z_*^3} \frac{1}{3} g^3 g_{\zeta\zeta\zeta} = 1.$$

We choose $z_* = \tilde{h}_0 / u(t)^{1/3}$ so that we obtain the Landau-Levich equation

$$g + \frac{1}{3} g^3 g_{\zeta\zeta\zeta} = 1$$

with boundary conditions $g \rightarrow 1$ as $\zeta \rightarrow \infty$ and

$$g \sim \frac{\tilde{h}_0}{u(t)^{2/3}} \frac{\zeta^2}{\sqrt{2}}$$

as $\zeta \rightarrow -\infty$.

From the notes, we recall that the numerical solution of the Landau-Levich equation has $g \sim 0.67 \zeta^2$ as $\zeta \rightarrow -\infty$ and so we have

$$\frac{\tilde{h}_0}{\sqrt{2} u(t)^{2/3}} = 0.67$$

and so $\tilde{h}_0 \approx 0.95 u(t)^{2/3}$, as required.

3 We are given that

$$h_t + \left[\frac{h^3}{3Ca} (h_{xxx} - \text{Bo } h_x) \right]_x = 0.$$

Letting $h(x, t) = h_0 + \delta h_1(x, t)$ with h_0 constant we find that

$$0 = \delta \frac{\partial h_1}{\partial t} + \left[\frac{h_0^3 + 3\delta h_0^2 h_1}{3Ca} (\delta h_{1,xxx} - \delta \text{Bo } h_{1,x}) \right]_x + O(\delta^3).$$

Examining the $O(\delta)$ terms we immediately see that

$$0 = \frac{\partial h_1}{\partial t} + \frac{h_0^3}{3Ca} (h_{1,xxxx} - \text{Bo } h_{1,xx}),$$

as required.

Letting $h_1 = \Re[e^{\sigma t + ikx}]$ we have

$$\sigma = -\frac{h_0^3}{3Ca} [(ik)^4 - \text{Bo}(ik)^2] = -\frac{h_0^3}{3Ca} (k^4 + \text{Bo } k^2),$$

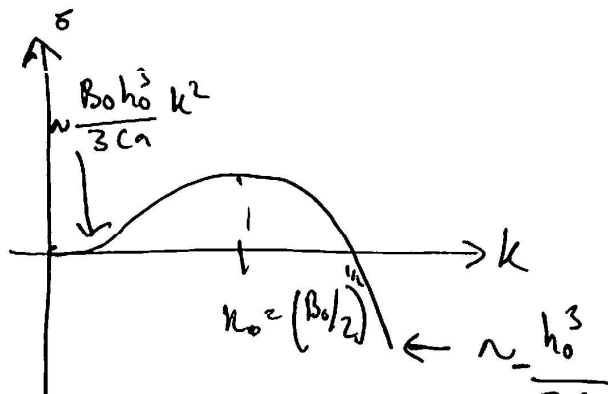
as required. Clearly $\sigma < 0$ for all $k \neq 0$; disturbances therefore decays with time and the film is stable to perturbations of any wavelength.

For $k = 0$, $\sigma = 0$ and so a uniform perturbation is neutrally stable — it neither grows nor decays.

When the film is beneath (rather than above) the plate, gravity acts in the opposite direction, $\text{Bo} \rightarrow -\text{Bo}$ and so we have

$$\sigma = -\frac{h_0^3}{3Ca} (k^4 - \text{Bo } k^2),$$

A sketch is shown below:



We see that the surface tension term ($-k^4$) is stabilising since it makes σ more negative, while gravity ($+\text{Bo } k^2$) is destabilising since it acts to increase σ .

The situation is unstable whenever $\sigma > 0$, i.e. for

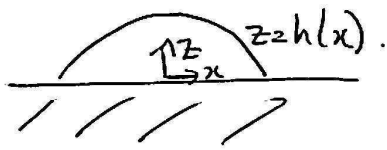
$$0 < k < \text{Bo}^{1/2}.$$

The maximally unstable mode is that for which σ is maximised. We have

$$\sigma'(k) = -\frac{h_0^3}{3\text{Ca}}(4k^3 - 2\text{Bo } k)$$

and so the maximally unstable wavelength is $\lambda = 2\pi/k_*$ where $k_* = (\text{Bo}/2)^{1/2}$.

Q4



The kinematic boundary condition is:

$$\frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x} = w - E \quad (1)$$

In deriving lubrication flow for droplets used length R timescale R/U and velocity scale U .

Using these scales here, we find:

$$\frac{\partial \tilde{h}}{\partial \tilde{t}} + \tilde{u} \frac{\partial \tilde{h}}{\partial \tilde{x}} = \tilde{w} - E/U$$

But U is thus far arbitrary, so we choose $U = E$

$$\Rightarrow \frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x} = w - 1 \quad \text{on } z = h(x).$$

(This is consistent with scalings used for lubrication theory but here $Ca = \frac{\mu E}{\gamma}$ specified).

In the fluid we have the dimensionless lubrication equations:

$$\frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial x}$$

$$0 = \frac{\partial p}{\partial z} \Rightarrow p = f(x) = -\frac{1}{Ca} \frac{\partial^2 h}{\partial x^2} \quad \text{on } z = h(x)$$

$$\Rightarrow p = -\frac{1}{Ca} \frac{\partial^2 h}{\partial x^2} \quad \text{everywhere.}$$

$$\therefore u = \frac{1}{2} \frac{\partial p}{\partial x} z(z-2h) \quad \left[\begin{array}{l} u = 0 \text{ on } z=0 \\ u_z = 0 \text{ on } z=h \end{array} \right]$$

$$\Rightarrow h\bar{u} = \frac{1}{2} \frac{\partial p}{\partial x} \left[\frac{1^3}{3} - h^3 \right] = -\frac{h^3}{3} \frac{\partial p}{\partial x} = \frac{h^3}{3Ca} \frac{\partial^3 h}{\partial x^3}$$

Now:

$$\begin{aligned}\frac{d}{dx} \int_0^h u dz &= h_x u(h) + \int_0^h \left(\frac{\partial u}{\partial x} z - \frac{\partial w}{\partial z} \right) dz \\ &= h_x u(h) - \left[w(h) = 1 + \frac{\partial h}{\partial t} + h_x u(h) \right] \\ &= -1 - \frac{\partial h}{\partial t}.\end{aligned}$$

$$\therefore \frac{\partial h}{\partial t} + \frac{\partial}{\partial x} (\bar{u} h) = -1$$

$$\text{i.e. } \frac{\partial h}{\partial t} + \frac{\partial}{\partial x} \left(\frac{h^3}{3Ca} \frac{\partial^3 h}{\partial x^3} \right) = -1. \quad (*)$$

$Ca \ll 1 \Rightarrow$ @ leading order:

$$\frac{d}{dx} \left(\frac{h_0^3}{3} \frac{\partial^3 h_0}{\partial x^3} \right) = 0 \Rightarrow \frac{\partial^3 h_0}{\partial x^3} = 0$$

$$\left[h_0^3 h_{0,xxx} = \text{const} = 0 \text{ as } h_0 = 0 \text{ at } x = \pm s \right]$$

$$\Rightarrow h_0 = k(t) (s^2 - x^2)$$

$$\text{To ensure } A(t) = \int_{-s}^s h_0 dx = k(t) \cdot \frac{4s^3}{3}$$

$$\Rightarrow k(t) = \frac{3}{4s^3} A(t).$$

Integrating the film eqn (*) we have:

$$\frac{d}{dt} \int_{-s}^s h dx = - \int_{-s}^s 1 dx = -2s$$

So, at leading order:

$$-2s = \frac{d}{dt} \int_{-s}^s h_0 dx = \frac{d}{dt} A \Rightarrow \dot{A} = -2s, \text{ as desired.}$$

Let $h = h_0 + Ca h_1 + Ca^2 h_2 + \dots$

and then calculate:

$$Ca \bar{u} = \frac{h^2}{3} h_{3x} = \frac{h_0^2 h_{0,3x}}{3} + Ca \left(\frac{h_0^2 h_{1,3x}}{3} + \frac{2h_0 h_1 h_{0,3x}}{3} \right) + \dots$$

$$= \bar{u}_0 + Ca \bar{u}_1 + \dots$$

Sub this into evolution equation (*):

$$-1 = \frac{\partial h_0}{\partial t} + \frac{Ca}{Ca} \frac{d}{dx} \left(h_0 \bar{u}_1 + h_1 \bar{u}_0 \right)$$

since $\bar{u}_0 = 0$

$$\Rightarrow h_0 \bar{u}_1 = - \int_0^x \left(1 + \frac{\partial h_0}{\partial t} \right) dx'$$

[$\because \bar{u}_1(x=0) = 0$
by symmetry]

$$= -x - \int_0^x -\frac{3}{2s^2} (s^2 - x'^2) dx'$$

$$= -x + \frac{3}{2s^2} \left(s^2 x - \frac{x^3}{3} \right)$$

$$= \frac{x}{2s^2} (s^2 - x^2)$$

$$\Rightarrow \bar{u}_1 = \frac{\frac{x}{2s^2} (s^2 - x^2)}{\frac{3A(k)}{4s^3} (s^2 - x^2)}$$

$$\bar{u} = \bar{u}_1 + Ca \bar{u}_2 + \dots$$

$$= \frac{2s}{3} \frac{x}{A(k)} + O(Ca)$$

as desired.

If gravity is present then we have:

$$\frac{1}{3} h^2 (h_{xxx} - B_0 h_x) = \bar{u}_0 + Ca \bar{u}_1 + \dots$$

The analysis above will be unchanged provided that

$$h_{xxx} - B_0 h_x \approx h_{xxx}$$

Now if we choose $L=S$ so that gradients of h_0 etc are all $O(1)$ then we require $B_0 \ll 1$

and hence: $\frac{\rho g S^2}{\gamma} \ll 1,$

5. We have the usual lubrication equation for the horizontal velocity, u , i.e.

$$\mu \frac{\partial^2 u}{\partial z^2} = \frac{\partial p}{\partial x}, \quad (7)$$

while at leading order the vertical component gives

$$\frac{\partial p}{\partial z} = -\rho g.$$

Integrating the latter and taking the pressure in the atmosphere to be 0, we have

$$p = \rho g [h(x, t) - z] - \gamma \frac{\partial^2 h}{\partial x^2}. \quad (8)$$

Integrating (7) we have that

$$u = \frac{1}{2\mu} \frac{\partial p}{\partial x} z^2 + Az + B$$

where A and B are constants to be determined from the boundary conditions problem:

- The condition of zero shear stress at the free surface gives

$$\left. \frac{\partial u}{\partial z} \right|_{z=h} = 0 \quad \implies \quad A = -\frac{1}{\mu} \frac{\partial p}{\partial x} h.$$

- The slip condition $u = \lambda u_z$ at $z = 0$ gives

$$B = \lambda A = -\frac{\lambda}{\mu} \frac{\partial p}{\partial x} h$$

and hence

$$u = -\frac{1}{\mu} \frac{\partial p}{\partial x} \left[\frac{1}{2} z^2 - zh - \lambda h \right].$$

Now

$$\begin{aligned} \bar{u} &= \frac{1}{h} \int_0^h u \, dz = \frac{1}{\mu h} \frac{\partial p}{\partial x} \left[\frac{1}{6} h^3 - \frac{1}{2} h^3 - \lambda h^2 \right]. \\ &= -\frac{1}{\mu} \frac{\partial p}{\partial x} \left[\frac{1}{3} h^2 + \lambda h \right]. \end{aligned}$$

From (8) we have that

$$\frac{\partial p}{\partial x} = \rho g \frac{\partial h}{\partial x} - \gamma \frac{\partial^3 h}{\partial x^3}$$

and so

$$\bar{u} = \frac{\gamma}{\mu} \left(\frac{\partial^3 h}{\partial x^3} - \ell_c^{-2} \frac{\partial h}{\partial x} \right) \left(\frac{1}{3} h^2 + \lambda h \right),$$

where $\ell_c^2 = \gamma/\rho g$, as usual.

The associated thin film equation is eqn (2.27) from the notes and so we have

$$0 = \frac{\partial h}{\partial t} + \frac{\gamma}{\mu} \frac{\partial}{\partial x} \left[\left(\frac{\partial^3 h}{\partial x^3} - \ell_c^{-2} \frac{\partial h}{\partial x} \right) \left(\frac{1}{3} h^3 + \lambda h^2 \right) \right]$$

[It is worth emphasizing again that the general statement of conservation of mass (having used the kinematic boundary condition) is of the form

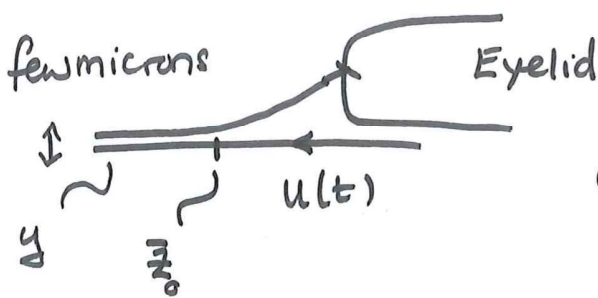
$$\frac{\partial h}{\partial t} + \nabla \cdot \mathbf{q} = 0,$$

since this comes up frequently in such problems.]

Q6 From Q2

$$\eta \frac{\partial \bar{h}}{\partial t} + u(t) \frac{\partial \bar{h}}{\partial \bar{z}} + \frac{\partial}{\partial \bar{z}} \left[\frac{\bar{h}^3}{3} (\bar{h} \bar{z} \bar{z} \bar{z} - \delta^2) \right] = 0$$

Dominant balance for thinnest possible film, A below as small as possible while there is still a balance



$$\text{Let } y = A(\bar{z} - \bar{z}_0), \quad A \ll 1$$

$$0 = \eta \frac{\partial \bar{h}}{\partial t} + u A \frac{\partial \bar{h}}{\partial y} + \frac{\partial}{\partial y} \left[\frac{\bar{h}^3}{3} (A^4 \bar{h} y y y - \delta^2 A) \right]$$

$A = \eta$, dominant balance

$$0 = \frac{\partial \bar{h}}{\partial t} + u(t) \frac{\partial \bar{h}}{\partial y}$$

As $y \rightarrow 0$, $\bar{h} \sim 0.95(u(t))^{2/3} \therefore$ Take $\bar{h}(y=0, t) = 0.95(u(t))^{2/3}$.

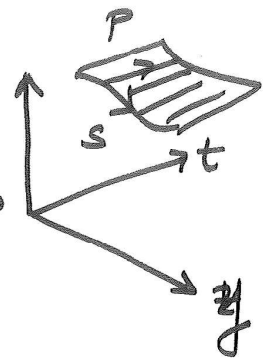
\therefore Noting $u(t) = e^{-t}$

$$e^t \frac{\partial \bar{h}}{\partial t} + \frac{\partial \bar{h}}{\partial y} = 0$$

$$h(0,t) = 0.95 e^{-2t/3}$$

Cauchy data, on $p=0$.

$$t=s, \quad y=0, \quad h(s) = 0.95 e^{-2s/3}$$



Characteristics

$$\frac{dt}{dp} = e^t$$

$$\frac{dy}{dp} = 1$$

$$\frac{dh}{dp} = 0$$

$$t(p=0) = s \quad \left| \quad y(p=0) = 0 \quad \right| \quad h(p=0) = 0.95 e^{-2s/3}$$

$$\therefore p = \int e^{-t} dt \quad \left| \quad y = p \quad \right| \quad h = 0.95 e^{-2s/3}$$

$$p = -e^{-t} + e^{-s}$$

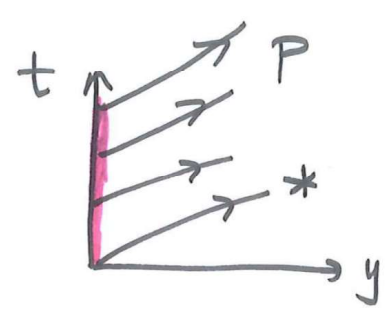
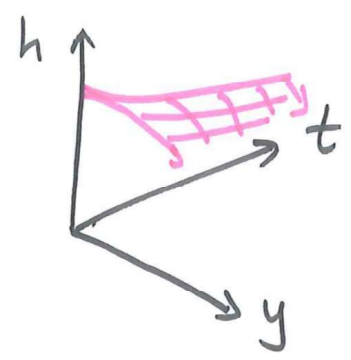
$$\therefore e^s = \frac{1}{p + e^{-t}} \quad \therefore e^{-2s/3} = (p + e^{-t})^{2/3}$$

$$= (y + e^{-t})^{2/3}$$

$y \rightarrow z$ to match question

$$\therefore h = (z + e^{-t})^{2/3} \cdot (0.95) \rightarrow 0.95 z^{2/3} \text{ as } t \rightarrow \infty$$

Constraint on z



Limiting characteristic (*) corresponds to $s=0$ above

$$\frac{dy}{dt} = e^{-t}, \quad y = A - e^{-t} \quad \text{with } y=0 \text{ when } t=0$$
$$\underline{\underline{y = 1 - e^{-t}}}$$

\therefore Range of $y \equiv z$ is $[0, 1)$.