

# Further Partial Differential Equations (2023)

## Problem Sheet 3

### 1. Asymptotic analysis of Stefan problems

- (a) Show that the transcendental relation (2.12) between  $\beta$  and  $St$  may be parameterized as

$$St = \sqrt{\pi}\xi e^{\xi^2} \operatorname{erf}(\xi), \quad \beta = \frac{2\sqrt{\xi}e^{-\xi^2/2}}{\pi^{1/4}\sqrt{\operatorname{erf}(\xi)}}, \quad (1)$$

where  $0 < \xi < \infty$ . By taking the limits  $\xi \rightarrow 0$  and  $\xi \rightarrow \infty$ , derive the asymptotic expressions (2.13).

**Solution**

Define  $\xi = \beta\sqrt{\text{St}}/2$ . Substituting into the transcendental equation (2.12) gives

$$\sqrt{\pi}\xi e^{\xi^2} \text{erf}(\xi) = \text{St}, \quad (2)$$

$$\beta = \frac{2\xi}{\text{St}} = \frac{2\sqrt{\xi}e^{-\xi^2/2}}{\pi^{1/4}\sqrt{\text{erf}(\xi)}}. \quad (3)$$

As  $\xi \rightarrow 0$ ,  $\text{erf}(\xi) \sim 2\xi/\sqrt{\pi}$  so  $\text{St} \sim 2\xi^2$  in (2) and  $\beta \rightarrow \sqrt{2}$  in (3).

As  $\xi \rightarrow \infty$ ,  $\text{erf} \rightarrow 1$ , so (2) and (3) give respectively

$$\text{St} \sim \sqrt{\pi}\xi e^{\xi^2}, \quad (4)$$

$$\beta \sim \frac{2}{\pi^{1/4}}\xi^{1/2}e^{-\xi^2/2}. \quad (5)$$

Equation (4) gives

$$\log\left(\frac{\text{St}}{\sqrt{\pi}}\right) \sim \xi^2 + \text{higher order logarithmic terms}, \quad (6)$$

and so

$$\beta \sim \frac{2}{\sqrt{\text{St}}}\sqrt{\log\left(\frac{\text{St}}{\sqrt{\pi}}\right)}. \quad (7)$$

## 2. Similarity solutions in the two-phase Stefan problem

Consider the two-phase Stefan problem (2.15) in the limit  $t \rightarrow 0$ . Show that the leading-order behaviour is given by

$$u(x, t) \sim \begin{cases} f(\eta) & 0 < \eta < \beta, \\ g(\eta) & \beta < \eta < \infty, \end{cases} \quad s(t) \sim \beta\sqrt{t}, \quad \eta = \frac{x}{\sqrt{t}},$$

where

$$g(\eta) = \theta \left( \frac{\operatorname{erfc}(\eta\sqrt{St}/2\sqrt{\kappa})}{\operatorname{erfc}(\beta\sqrt{St}/2\sqrt{\kappa})} - 1 \right), \quad f(\eta) = \left( 1 - \frac{\operatorname{erf}(\eta\sqrt{St}/2)}{\operatorname{erf}(\beta\sqrt{St}/2)} \right),$$

and  $\beta$  satisfies the transcendental equation

$$\frac{\beta\sqrt{\pi}}{2\sqrt{St}} = \frac{e^{-\beta^2 St/4}}{\operatorname{erf}(\beta\sqrt{St}/2)} - \frac{K\theta e^{-\beta^2 St/4\kappa}}{\sqrt{\kappa}\operatorname{erfc}(\beta\sqrt{St}/2\sqrt{\kappa})}.$$

**Solution**

Substitute in the similarity solution form given in the question. (Note that you can obtain the form of this similarity solution by using a scaling argument.) This transforms the problem to

$$f'' + \frac{\text{St}}{2}\eta f' = 0, \quad \eta < \beta, \quad (8)$$

$$g'' + \frac{\text{St}}{2\kappa}\eta g' = 0, \quad \eta > \beta, \quad (9)$$

$$f(0) = 1, \quad (10)$$

$$g \rightarrow -\theta \quad \text{as } \eta \rightarrow \infty, \quad (11)$$

$$f(\beta) = g(\beta) = 0, \quad (12)$$

$$Kg'(\beta) - f'(\beta) = \frac{\beta}{2}. \quad (13)$$

The solution follows straightforwardly from this.

### 3. Linear stability of a two-dimensional Stefan problem

Consider the linear stability of the free boundary problem depicted in Figure 2.2 in the limit  $St \rightarrow 0$ . Assume that the free boundary is moving at constant speed  $V$  under a constant temperature gradient  $-\lambda_{1,2}$  in each phase before being perturbed, so the solutions take the form

$$u_1(x, y, t) = -\lambda_1(x - Vt) + \tilde{u}_1(x, y, t), \quad u_2(x, y, t) = -\lambda_2(x - Vt) + \tilde{u}_2(x, y, t)$$

and the position of the free boundary is given by

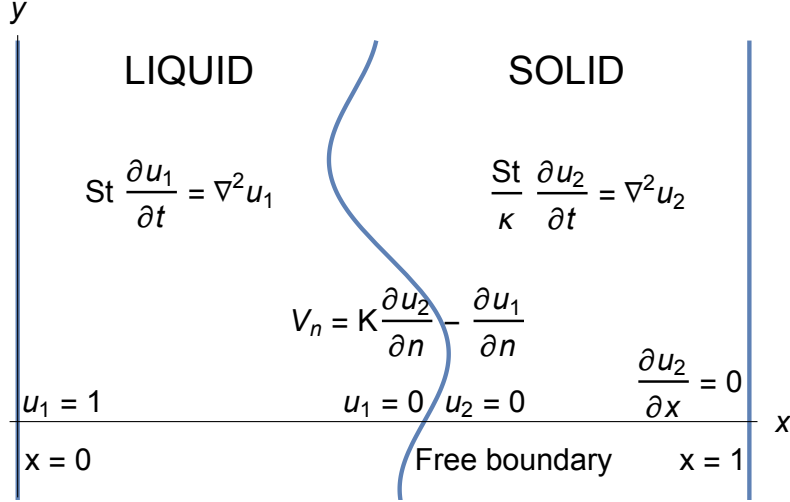
$$x = Vt + \xi(y, t).$$

By linearising the problem with respect to  $\tilde{u}_1$ ,  $\tilde{u}_2$  and  $\xi$ , show that perturbations with wavenumber  $k > 0$  and growth rate  $\sigma$  are possible provided

$$\frac{\sigma}{Vk} = -\frac{\lambda_1 + K\lambda_2}{\lambda_1 - K\lambda_2}.$$

### Solution

We consider the following problem with  $St \rightarrow 0$ :



We set

$$\begin{aligned} u_1 &= -\lambda_1(x - Vt) + \tilde{u}_1, \\ u_2 &= -\lambda_2(x - Vt) + \tilde{u}_2, \\ x &= Vt + \xi(y, t). \end{aligned}$$

If the free boundary is  $x = f(y, t)$  then the unit normal is

$$\mathbf{n} = \frac{\left(1, -\frac{\partial f}{\partial y}\right)}{\sqrt{1 + \left(\frac{\partial f}{\partial y}\right)^2}},$$

the normal derivative is

$$\frac{\partial u}{\partial n} = \frac{1}{\sqrt{1 + \left(\frac{\partial f}{\partial y}\right)^2}} \left(\frac{\partial u}{\partial x} - \frac{\partial f}{\partial y} \frac{\partial u}{\partial y}\right),$$

and the normal velocity is

$$V_n = \frac{\frac{\partial f}{\partial t}}{\sqrt{1 + \left(\frac{\partial f}{\partial y}\right)^2}}.$$

Now in our case,  $f = Vt + \xi(y, t)$ , so the free boundary conditions are

$$K \left(-\lambda_2 + \frac{\partial \tilde{u}_2}{\partial x} - \frac{\partial \xi}{\partial y} \frac{\partial \tilde{u}_2}{\partial y}\right) - \left(-\lambda_1 + \frac{\partial \tilde{u}_1}{\partial x} - \frac{\partial \xi}{\partial y} \frac{\partial \tilde{u}_1}{\partial y}\right) = V + \frac{\partial \xi}{\partial t}$$

on  $x = Vt + \xi(y, t)$ . Considering this at  $O(1)$  gives

$$-K\lambda_2 + \lambda_1 = V \quad \text{on } x = Vt$$

and at next order,

$$K \frac{\partial \tilde{u}_2}{\partial x} - \frac{\partial \tilde{u}_1}{\partial x} = \frac{\partial \xi}{\partial t} \quad \text{on } x = Vt.$$

Since  $u_1 = u_2 = 0$  on the interface, this gives

$$-\lambda_1 \xi + \tilde{u}_1 = -\lambda_2 \xi + \tilde{u}_2 = 0 \quad \text{on } x = Vt.$$

The leading-order equations for  $St \rightarrow 0$  are

$$\begin{aligned} \nabla^2 \tilde{u}_1 &= 0, & x < Vt, \\ \nabla^2 \tilde{u}_2 &= 0, & x > Vt, \end{aligned}$$

We no longer need to consider the conditions on  $x = 0$  and  $x = 1$  since we are now just performing a local analysis. Our only requirement is that the perturbations decay away so we seek solutions of the form

$$\begin{aligned} \tilde{u}_1 &= A \exp(\sigma t + iky + k(x - Vt)), \\ \tilde{u}_2 &= B \exp(\sigma t + iky - k(x - Vt)), \\ \xi &= C \exp(\sigma t + iky). \end{aligned}$$

These satisfy Laplace's equation and decay away from the interface. The interface conditions give

$$-Kk\lambda_1 - Bk\lambda_2 = \sigma$$

and

$$\begin{pmatrix} Kk & k & \sigma \\ 1 & 0 & -\lambda_1 \\ 0 & 1 & -\lambda_2 \end{pmatrix} \begin{pmatrix} A \\ B \\ C \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}.$$

Non-trivial solutions require the determinant of this matrix to be zero, which gives

$$\frac{\sigma}{kV} = -\frac{1}{V} (K\lambda_1 + \lambda_2) = -\frac{K\lambda_1 + \lambda_2}{\lambda_1 - K\lambda_2}$$

as required.

4. **OPTIONAL (will not be marked) A solid–liquid interface with a density change**

Consider the one-dimensional Stefan problem for melting of a solid considered in lectures. The full system behaviour may be described by equations expressing conservation of mass, momentum and total energy, which are given respectively by

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho v) = 0, \quad (14)$$

$$\frac{\partial}{\partial t} (\rho v) + \frac{\partial}{\partial x} (\rho v^2 + p) = 0, \quad (15)$$

$$\frac{\partial}{\partial t} \left( \rho h + \frac{1}{2} \rho v^2 \right) + \frac{\partial}{\partial x} \left( p v - k \frac{\partial T}{\partial x} + \rho \left( h + \frac{1}{2} v^2 \right) v \right) = 0, \quad (16)$$

where  $\rho$  is the density,  $v$  the velocity,  $p$  the pressure,  $T$  the temperature and

$$h = \begin{cases} c(T - T_m) + L & T > T_m \\ c(T - T_m) & T < T_m. \end{cases}$$

is the *enthalpy* of the system, which is the total energy per unit mass, including heat. Here,  $c$  is the specific heat and  $L$  the latent heat.

Suppose that liquid occupies a region  $0 \leq x \leq s(t)$  and solid occupies a region  $x > s(t)$ .

- (a) Show that when the density of the fluid and the solid are the same then  $v = 0$  and the temperature in the liquid and the solid is described by the one-dimensional heat equation

$$\frac{\partial}{\partial t} (\rho c T) - \frac{\partial}{\partial x} \left( k \frac{\partial T}{\partial x} \right) = 0. \quad (17)$$

- (b) Now suppose that the densities in the solid and the liquid phases are different. Integrate (14) over a domain  $x_1 < x < x_2$  that contains the interface (so  $x_1 < s(t)$  and  $x_2 > s(t)$ ). Divide the integral into  $x_1 \leq x \leq s(t)$  and  $s(t) \leq x \leq x_2$  and take the limit as  $x_1 \rightarrow s(t)^-$  and  $x_2 \rightarrow s(t)^+$  to show that the following jump condition is satisfied by the density:

$$[\rho]_-^+ \frac{ds}{dt} = [\rho v]_-^+. \quad (18)$$

- (c) By performing an identical process for (15) and (16) obtain the jump conditions

$$[\rho v]_-^+ \frac{ds}{dt} = [\rho v^2 + p]_-^+, \quad (19)$$

$$\left[ \rho h + \frac{1}{2} \rho v^2 \right]_-^+ \frac{ds}{dt} = \left[ p v - k \frac{\partial T}{\partial x} + \rho \left( h + \frac{1}{2} v^2 \right) v \right]_-^+. \quad (20)$$

- (d) Explain how these reduce to the Stefan condition presented in lectures when the solid and liquid densities are equal.



**Solution**

- (a) Substitution of constant  $\rho$  into (14) gives  $v$  as an arbitrary function of time. Since the liquid occupies the region  $0 \leq x \leq s(t)$ , the boundary  $x = 0$  is fixed and so  $v = 0$  here and hence  $v = 0$  everywhere. Substitution into (15) gives constant pressure gradient  $p$ . Substitution into (16) gives the required heat equation.
- (b) Equation (14) only applies provided the variables are continuous, and so does not hold across jumps. We thus consider the integrated conservative version,

$$\frac{d}{dt} \int_{x_1}^{x_2} \rho dx = [\rho v]_{x_1}^{x_2},$$

where  $x_1 < s(t) < x_2$ . We divide the integral into parts to the left and right of the jump,

$$\frac{d}{dt} \int_{x_1}^{s(t)} \rho dx + \int_{s(t)}^{x_2} \rho dx = [\rho v]_{x_1}^{x_2} \int_{x_1}^{s(t)} \frac{\partial \rho}{\partial t} dx + \rho|_{x_1} \frac{ds}{dt} + \int_{s(t)}^{x_2} \frac{\partial \rho}{\partial t} dx - \rho|_{x_2} \frac{ds}{dt} = [\rho v]_{x_1}^{x_2}$$

using Leibniz' rule. Then, taking the limit  $x_1 \rightarrow s(t)^-$  and  $x_2 \rightarrow s(t)^+$  and recognizing that

$$\lim_{x_1 \rightarrow s(t)^-} \int_{x_1}^{s(t)} \frac{\partial \rho}{\partial t} dx = 0, \quad \lim_{x_2 \rightarrow s(t)^+} \int_{s(t)}^{x_2} \frac{\partial \rho}{\partial t} dx = 0,$$

we obtain the required result,

$$[\rho]_-^+ \frac{ds}{dt} = [\rho v]_-^+.$$

- (c) This may be found easily by following the same steps as above.
- (d) When the solid and liquid densities are equal, (19) gives  $[p]_-^+ = 0$ , so the pressure is continuous across the interface, and

$$\rho L \frac{ds}{dt} = - \left[ k \frac{\partial T}{\partial x} \right]_-^+ \tag{21}$$

if we assume that the temperature is continuous across the interface. This is precisely the Stefan condition from the lectures.