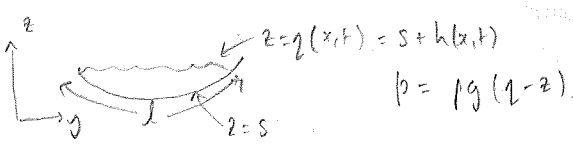
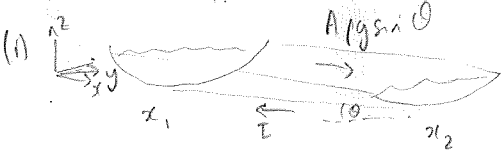


1. St Venant equations



Mass conservation $\frac{d}{dt} \int_{x_1}^{x_2} A dx = Q|_{x_1} - Q|_{x_2} = - \int_{x_1}^{x_2} \frac{\partial Q}{\partial x} dx$ where $Q = Au$ is volume flux.

Since x_1, x_2 are arbitrary, this implies $\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} = 0$ (A assuming continuity) (water is incompressible so volume is conserved)

Momentum conservation $\frac{d}{dt} \int_{x_1}^{x_2} \rho A u dx = \rho A u^2|_{x_1} - \rho A u^2|_{x_2} - \int_{x_1}^{x_2} \tau dx + \rho g A \sin \theta l + \bar{p} A|_{x_1} - \bar{p} A|_{x_2}$

momentum fluxes friction weight pressure forces.

$S = \sin \theta$

$$\int_{x_1}^{x_2} \frac{d}{dt} (\rho A u^2) - \tau l + \rho g A S - \frac{d}{dx} (\bar{p} A) dx$$

Since x_1, x_2 are arbitrary, $\frac{d}{dt} (\rho A u^2) + \frac{d}{dx} (\bar{p} A) = \rho g A S - \tau l$

Since $p = \rho g (z - z)$, $\bar{p} A = \int_A \rho g (z - z) dy dz$ $\frac{d}{dx} (\bar{p} A) = \int_A \rho g z_x dy dz = \rho g A z_x$, assuming z_x is independent of y . Also assume S flat, so $z_x = \bar{h}_x$, \bar{h} = average depth.

Using (1), dividing by ρA $\Rightarrow \frac{du}{dt} + u \frac{du}{dx} = g S - \frac{\tau l}{\rho A} - g \bar{h}_x$ (2)

Steady uniform flow would have $g S = \frac{\tau l}{\rho A}$, $\Rightarrow \tau = \rho g S R$ where $R = \frac{A}{l}$

If this has $u = R^{2/3} S^{1/2}$ then (eliminating S) $\tau = \frac{\rho g n^2 u^2}{R^{1/3}}$

For a triangular cross-section, $h = \frac{l}{2} \sin \beta$, $A = (\frac{l}{2})^2 \sin \beta \cos \beta = \frac{1}{8} l^2 \sin(2\beta)$ $\Rightarrow l = A^{1/2} (\frac{\sin 2\beta}{8})^{-1/2}$



$h = 2\bar{h}$ so $R = \frac{A}{l} = \frac{1}{8} l \sin 2\beta = (\frac{\sin 2\beta}{8})^{1/2} A^{1/2}$ and $\bar{h} = \frac{\sin \beta}{4} (\frac{\sin 2\beta}{8})^{-1/2} A^{1/2}$

Hence $\tau = \rho g n^2 (\frac{\sin 2\beta}{8})^{-1/6} \frac{u^2}{A^{1/6}}$ and $\bar{h} = (\frac{\tan \beta}{4})^{1/2} A^{1/2}$ $\frac{\tau l}{\rho A} = \frac{\tau}{\rho R} = \frac{g n^2}{R^{1/3}} u^2 = g n^2 (\frac{\sin 2\beta}{8})^{1/3} \frac{u^2}{A^{1/3}}$

Substituting into (2), we have $\frac{du}{dt} + u \frac{du}{dx} = g S - g n^2 (\frac{\sin 2\beta}{8})^{-2/3} \frac{u^2}{A^{2/3}} - g (\frac{\tan \beta}{4})^{1/2} \frac{d}{dx} (A^{1/2})$

(ii) Non-dimensionalization. $x \approx L \hat{x}$
 $A = [A] \hat{A}$
 $u = [u] \hat{u}$
 $t = [t] \hat{t}$

$$gS = g n^2 \left(\frac{\sin 2\beta}{r} \right)^{-2/3} \frac{[u]^2}{[A]^{2/3}} \quad \& \quad [A][u] = Q \rightarrow [u], [A]$$

$$[t] = \frac{L}{[u]} \rightarrow [t]$$

Solving for $[u] \Rightarrow SQ^{2/3} = n^2 \left(\frac{\sin 2\beta}{r} \right)^{-2/3} [u]^{8/3} \Rightarrow [u] = S^{3/4} Q^{1/4} \left(\frac{\sin 2\beta}{r} \right)^{1/4} n^{-3/4}$
 $[A] = Q^{3/4} S^{-3/8} \left(\frac{\sin 2\beta}{r} \right)^{-1/4} n^{3/4}$

Then non-dimensional equations are

$$\frac{\partial A}{\partial \hat{t}} + \frac{\partial}{\partial \hat{x}} (A \hat{u}) = 0$$

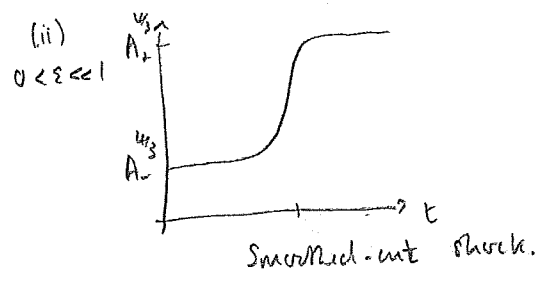
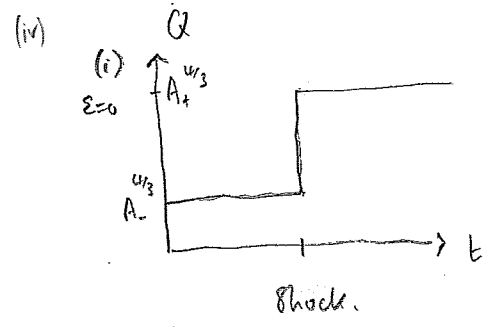
$$\varepsilon F^2 \left(\frac{\partial \hat{u}}{\partial \hat{t}} + \hat{u} \frac{\partial \hat{u}}{\partial \hat{x}} \right) = 1 - \frac{u^2}{A^{2/3}} - \varepsilon \frac{\partial}{\partial \hat{x}} (A^{1/2})$$

where $\varepsilon = \left(\frac{kn\beta}{4} \right)^{1/2} \frac{[A]^{1/2}}{L S} = \frac{[k]}{L S}$ and $F^2 = \frac{[u]^2}{g [k]}$ $([k] = \left(\frac{kn\beta}{4} \right)^{1/2} [A]^{1/2})$

(iii) - If $\varepsilon \ll 1$ and $F \ll 1$, leading order $A^{2/3} = u^2 \Rightarrow u \approx A^{1/3}$
 Then to next order in ε , $u^2 = A^{2/3} - \varepsilon A^{2/3} \frac{\partial}{\partial x} (A^{1/2}) = A^{2/3} - \frac{1}{2} \varepsilon A^{1/6} \frac{\partial A}{\partial x}$
 $\Rightarrow u = A^{1/3} \left(1 - \frac{\varepsilon}{2} A^{-1/2} \frac{\partial A}{\partial x} \right)^{1/2}$
 $\approx A^{1/3} \left(1 - \frac{\varepsilon}{4} A^{-1/2} \frac{\partial A}{\partial x} + \dots \right) \approx A^{1/3} - \frac{\varepsilon}{4} A^{-1/6} \frac{\partial A}{\partial x}$

so mass equation becomes $\frac{\partial A}{\partial \hat{t}} + \frac{\partial}{\partial \hat{x}} \left[A^{4/3} - \frac{\varepsilon}{4} A^{5/6} \frac{\partial A}{\partial \hat{x}} \right] = 0$

or $\frac{\partial A}{\partial \hat{t}} + \frac{4}{3} A^{1/3} \frac{\partial A}{\partial \hat{x}} = \frac{\varepsilon}{4} \frac{\partial}{\partial \hat{x}} \left(A^{5/6} \frac{\partial A}{\partial \hat{x}} \right)$



2. Surface waves

(i) As in previous question, and choosing $L = (h^3)/5$ so as to make $\epsilon = 1$, the equation for a triangular-shaped cross-section with Manning's law take the form

$$\frac{\partial A}{\partial t} + \frac{\partial (Au)}{\partial x} = 0$$

$$F^2 \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} \right) = 1 - \frac{u^2}{A^{2/3}} - \frac{1}{2A^{1/2}} \frac{\partial A}{\partial x}$$

$$F^2 = \frac{(u)^2}{g(h^3)}$$

Uniform steady state has $u^2 = A^{2/3}$ and of discharge is 1, $Au = 1$.

$$\Rightarrow u = A = 1$$

(ii) Perturbation $u = 1 + U$, $A = 1 + a$ with $U, a \ll 1$. Linearized equations

$$\frac{\partial a}{\partial t} + \frac{\partial a}{\partial x} + \frac{\partial U}{\partial x} = 0$$

$$F^2 \left(\frac{\partial U}{\partial t} + \frac{\partial U}{\partial x} \right) = -2U + \frac{2}{3}a - \frac{1}{2} \frac{\partial a}{\partial x}$$

$$\rightarrow \left(\frac{\partial}{\partial t} + \frac{\partial}{\partial x} \right) a = -\frac{\partial U}{\partial x}$$

$$\Rightarrow F^2 \left(\frac{\partial}{\partial t} + \frac{\partial}{\partial x} \right)^2 U = -2 \left(\frac{\partial}{\partial t} + \frac{\partial}{\partial x} \right) U - \frac{2}{3} \frac{\partial U}{\partial x} + \frac{1}{2} \frac{\partial^2 U}{\partial x^2}$$

Solution of form $U = e^{\frac{\sigma + ikx}{F^2}}$ here

$$\frac{F^2(\sigma + ik)^2}{F^4} = -\frac{2(\sigma + ik)}{F^2} - \frac{2}{3} \frac{ik}{F^2} - \frac{1}{2} \frac{k^2}{F^4}$$

$$\Rightarrow (\sigma + ik)^2 + 2(\sigma + ik) + \frac{2}{3} ik + \frac{1}{2} \frac{k^2}{F^2} = 0$$

$$\sigma + ik = -1 \pm \left(1 - \frac{2}{3} ik - \frac{k^2}{2F^2} \right)^{1/2}$$

$p + iq$

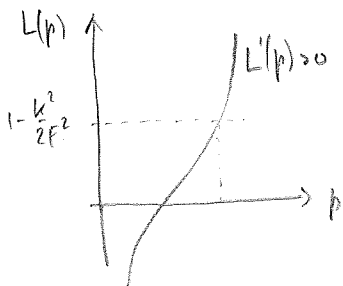
$$(p + iq)^2 = 1 - \frac{2}{3} ik - \frac{k^2}{2F^2} \quad (p > 0 \text{ w.d.o.g.})$$

$$\Rightarrow pq = -\frac{1}{3}k \rightarrow q = -\frac{k}{3p}$$

$$\Delta p^2 - q^2 = 1 - \frac{k^2}{2F^2} \rightarrow p^2 - \frac{k^2}{9p^2} = 1 - \frac{k^2}{2F^2}$$

"
L(p)

$$\Rightarrow \sigma = -1 \pm p - ik \left(1 \pm \frac{1}{3p} \right)$$



Velocity of perturbations is $\frac{-\sigma}{k} = 1 \pm \frac{1}{3p}$.

propagate up and downstream if $p < \frac{1}{3} \Leftrightarrow L(p) < L(\frac{1}{3})$
 $\Leftrightarrow 1 - \frac{k^2}{2F^2} < \frac{1}{9} = k^2$

$$\Leftrightarrow k^2 \left(\frac{1}{2F^2} - 1 \right) > \frac{8}{9}$$

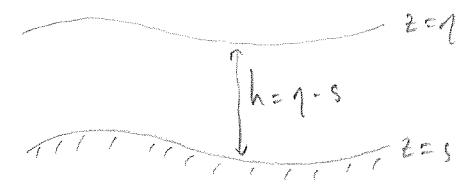
This occurs for at least some k , if $F^2 < \frac{1}{2}$. i.e. $F < \frac{1}{\sqrt{2}} = F_1$

Otherwise $p > \frac{1}{3}$ and all waves propagate downstream.

Instability occurs if $\sigma_R > 0 \Leftrightarrow p > 1 \Leftrightarrow L(p) > L(1)$
 $\Leftrightarrow 1 - \frac{k^2}{2F^2} > 1 - \frac{k^2}{9}$
 $\Leftrightarrow F^2 > \frac{9}{2}$

i.e. $F > \frac{3}{\sqrt{2}} = F_2$

3. Dunes and antidunes



(i) $\Sigma h_t + (hu)_x = 0$

Mass conservation

$F^2(\Sigma u_t + uu_x) = -\eta_x + \delta(1 - \frac{u^2}{h})$

Momentum conservation: (term on right: pressure gradient down slope gravity, friction)

$h(\Sigma c_t + uc_x) = E(u) - C = -S_E$

Suspended sediment conservation + Exner equation with erosion rate $E(u)$, deposition rate C (no bedload transport)

F is the Froude number - describes how fast the flow is.

δ represents ratio of advection timescale (for water) to bed evolution timescale.

δ represents importance of gravity and friction to force balance on the scale of a dune.

(ii) Steady state $u=h=c=1, s=0$ perturbed by writing $s=S, u=1+U, h=1+H, c=1+C,$

then with $\Sigma = 0, H+U=0$

$\rightarrow H = -U$

$F^2 U_x = -H_x - S_x + \delta(H - 2U)$

$(F^2 - 1)U_x + 3\delta U = -S_x$

$C_x = E'(1) + E'(1)U - C = -S_E$

$C_x = E'(1)U - C = -S_E$

Suppose $U = e^{\sigma t + ikx}, C = \hat{C} e^{\sigma t + ikx}, S = \hat{S} e^{\sigma t + ikx}$ then,

$ik \hat{C} = E'(1) - \hat{C}$

$\rightarrow \hat{C} = \frac{E'(1)}{1+ik}$

$ik(F^2 - 1) + 3\delta = -ik \hat{S}$

$\rightarrow -\hat{S} = \frac{ik(F^2 - 1) + 3\delta}{ik}$

$ik \hat{C} = -\sigma \hat{S}$

$\rightarrow \sigma = \frac{ik \hat{C}}{-\hat{S}} = \frac{E'(1) ik}{(1+ik)((F^2 - 1) - 3i\delta/k)}$

$= \frac{E'(1) ik(1-ik)((F^2 - 1) + 3i\delta/k)}{(1+k^2)[(F^2 - 1)^2 + 9\delta^2/k^2]}$

$= E'(1) \frac{\{(F^2 - 1)k^2 - 3\delta\} + ik\{(F^2 - 1) + 3\delta\}}{(1+k^2)[(F^2 - 1)^2 + 9\delta^2/k^2]}$

If $F > 1, \text{Re } \sigma > 0$ for $k^2 > \frac{3\delta}{F^2 - 1}$ is unstable. $-\text{Im } \frac{\sigma}{k} < 0$ in this case so waves move upstream. } \rightarrow corresponds to growth of antidunes

If $F < 1, \text{Re } \sigma < 0$ so system is stable.

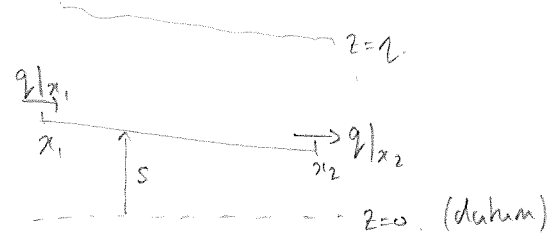
$-\text{Im } \frac{\sigma}{k}$ has sign depending on δ and F .

(iii) Note $\eta - 1 = H + S = (\frac{\hat{S}}{\hat{S}} - 1) e^{\sigma t + ikx}, \frac{\hat{S} - 1}{\hat{S}} = 1 + \frac{1}{(F^2 - 1) - 3i\delta/k} = 1 + \frac{(F^2 - 1) + \frac{3i\delta}{k}}{(F^2 - 1)^2 + \frac{9\delta^2}{k^2}}$

The argument of this factor gives the phase difference between surface and bed.

If $\frac{\delta}{k} \ll 1$, then $\frac{1}{F^2 - 1}$ so suggests in phase if $F > 1$, out of phase if $F < 1$. If $\frac{\delta}{k} \gg 1$ it is $1 + \frac{ik}{3\delta} + \dots$ so waves are in phase.

4. Eddy-viscosity model



(i) Consider a section of the bed between x_1 and x_2 .

$$\frac{\partial}{\partial t} \left(\int_{x_1}^{x_2} (1-\alpha) S dx \right) = q|_{x_1} - q|_{x_2} = - \int_{x_1}^{x_2} \frac{\partial q}{\partial x} dx$$

↑
rate of change of volume of sediments in the section.

Since x_1, x_2 are arbitrary,
$$(1-\alpha) \frac{\partial S}{\partial t} + \frac{\partial q}{\partial x} = 0$$

assume porosity α is constant.

If $q = q(t)$,
$$(1-\alpha) \frac{\partial S}{\partial t} + q'(t) \frac{\partial S}{\partial x} = 0$$

and if we scale $t \rightarrow [t]$ such that

$$[t] = \frac{(1-\alpha) [S] [x]}{[q]}$$

the equation becomes

↑ scales for $[S], [x], [q]$ all arbitrary at this stage.

$$\frac{\partial S}{\partial t} + q'(t) \frac{\partial S}{\partial x} = 0$$

(ii) Dimensionless shear stress model: $\tau = 1 - S + \int_0^{\infty} k(\xi) \frac{\partial S}{\partial x}(x-\xi, t) d\xi$ for $k(\xi) = \frac{1}{3} \xi^{1/3}$.

Perturb the steady state $S=0+S, \tau=1+T$, then

$$\frac{\partial S}{\partial t} + q'(1) \frac{\partial T}{\partial x} = 0, \quad T = -S + \int_0^{\infty} \frac{1}{3} \xi^{1/3} \frac{\partial S}{\partial x}(x-\xi, t) d\xi$$

Look for solutions of form $S = e^{\sigma t + ikx}, T = \hat{T} e^{\sigma t + ikx}$, then

$$\sigma = -ikq'(1)\hat{T}, \quad \hat{T} = -1 + ik \int_0^{\infty} \frac{1}{3} \xi^{1/3} e^{-ik\xi} d\xi = -1 + \frac{1}{2} \frac{\Gamma(2/3)}{\Gamma(1/3)} k^{1/3} \quad (\text{using hint})$$

$$\int_0^{\infty} \frac{1}{3} \xi^{1/3} e^{-ik\xi} d\xi = \int_{\Gamma} z^{-1/3} e^{-ikz} dz$$

$$= \int_{\Gamma} z^{-1/3} e^{-ikz} dz = \int_{\Gamma} z^{-1/3} e^{-ikz} dz + \int_{\Gamma} z^{-1/3} e^{-ikz} dz + \int_{\Gamma} z^{-1/3} e^{-ikz} dz + \int_{\Gamma} z^{-1/3} e^{-ikz} dz$$

$$= 0 + 0 + \left(-\frac{i}{k}\right)^{2/3} \int_0^{\infty} t^{-1/3} e^{-t} dt = 0$$

$$= \frac{e^{-i\pi/3}}{k^{2/3}} \Gamma\left(\frac{2}{3}\right)$$

(assuming $k > 0$).

So
$$\sigma = \frac{1}{2} \mu q'(1) \Gamma\left(\frac{2}{3}\right) k^{4/3} - ik q'(1) \left[\frac{\sqrt{3}}{2} \mu q'(1) \Gamma\left(\frac{2}{3}\right) k^{4/3} - 1 \right]$$

Perturbations are unstable ($\sigma_R > 0$) assuming $q'(1) > 0$. Perturbations travel downstream ($\frac{-\sigma_I}{k} > 0$) for large k and upstream for small k (long wavelength).